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**Determination of VOC, Ethanol, and Acetaldehyde
Emissions from Commercial Bakeries**

Site 2 Test Report

Prepared for:

**Mr. Solomon Ricks
Emission Measurement Branch
U.S. Environmental Protection Agency
Research Triangle Park, NC 27711**

Prepared by:

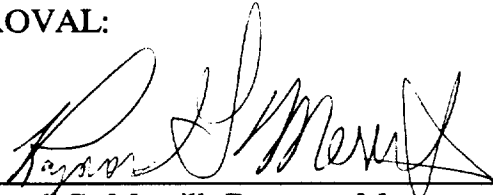
**Charles R. Parrish
Radian Corporation
P. O. Box 13000
Research Triangle Park, NC 27709**

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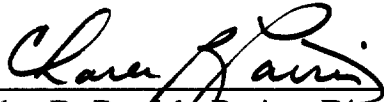
This report has been reviewed by the following Radian personnel and is a true representation of the results obtained from the sampling program conducted at four commercial bakeries on behalf of the U.S. Environmental Protection Agency. The testing was conducted from May through July, 1992, except where noted, sampling and analytical methods were performed in accordance with U.S. EPA reference procedures.

APPROVAL:




Raymond G. Merrill, Program Manager

9/29/92
Date



Charles R. Parrish, Project Director

9/30/92
Date



Susan Stamey-Hall, Peer Review

9/30/92
Date

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1.0

EXECUTIVE SUMMARY

Radian was contracted by The U.S. Environmental Protection Agency, Emissions Measurement Branch, to conduct Volatile Organic Compound (VOC) emissions testing at four commercial bakeries. This test report will present the results from the Site 2 test program. Tests were conducted on a variety of bakery ovens while baking different product types. The test procedures used were the U.S. EPA Stationary Source Testing Method 25A for VOCs and Method 18 for methane, ethanol and acetaldehyde determinations. Method 25A was used to quantify total hydrocarbons (THC). Method 18 was employed to quantify methane and two of the most prevalent VOC compounds (acetaldehyde and ethanol) in the bakery emission stream. Flow rates were measured using U.S. EPA Methods 1-4 and were used to calculate emission rates of the above gas stream components.

As a part of the test program, process conditions were monitored by a separate U.S. EPA contractor. Research Triangle Institute (RTI) monitored parameters such as product type, production rates, yeast concentration, proofing time and others. This report will only present the emissions data collected by Radian and will not include any process information. A separate report completed by RTI will incorporate the emission values presented in this report with the specific bakery process information.

Two sets of emission data were calculated. The first set presents VOC as ethanol emissions calculated using the Method 25A and Method 18 methane test results. (Ethanol concentrations typically made up over 98% of the total ethanol and acetaldehyde concentrations). The second data set presents emission rates of ethanol and acetaldehyde calculated from the Method 25A and the Method 18 ethanol and acetaldehyde test results.

VOC as ethanol emissions were determined by first averaging concentrations of THC over the respective test period. Non-methane hydrocarbon

concentrations were then determined by removing the methane concentration from the THC values. VOC as ethanol concentrations were determined by dividing the non-methane hydrocarbon concentration by the ethanol carbon equivalent correction factor (CECF). The CECF was empirically determined during and following the test program. The VOC as ethanol concentrations were then multiplied by the respective stack gas flow rates to determine VOC as ethanol emission rates.

Separate emissions rates of ethanol and acetaldehyde were calculated using both the Method 25A THC and Method 18 test results. The average ethanol-to-THC ratio was multiplied times the average THC concentration to determine an average ethanol concentration and formulate a larger averaging data base within the testing time period. Average acetaldehyde concentrations were calculated in the same manner. This procedure assumed that the proportion of ethanol to THC and acetaldehyde to THC remained constant throughout the test period. This assumption did not prove always to be true; however, concentrations determined in this manner were very similar to concentrations determined by averaging the Method 18 results alone. Results from both calculation methods are presented. Ethanol and acetaldehyde emission rates were then calculated by multiplying the average concentrations by the stack gas flow rates.

1.1 VOC as Ethanol Emissions

The Site 2 emissions ranged from 6.9 - 11.5 lbs/hr from Line 2, 17.8 lbs/hr from Line 1 and 40.9 lbs/hr from Line 3. A complete listing of all test results is given in Section 3.0 and in the attached Appendices.

1.2 Ethanol and Acetaldehyde Emissions

The Site 2 ethanol emissions ranged from 8.1 - 14.8 lbs/hr for Line 1 oven, 22.2 lbs/hr for the Line 2 oven, and 64.6 lbs/hr for the Line 3 oven. The corresponding

acetaldehyde rates were 0.24 - 0.42 lbs/hr for Line 1, 0.81 lbs/hr for Line 2, and 2.5 lbs/hr for Line 3.

1.3 Data Quality Assurance

The majority of reference method QA acceptance criteria were met during this test program. There were 10 days of testing using two THC monitoring systems . Method 25A daily calibration drift did not exceed the criterion of $\pm 3\%$ on any of the Site 2 test days. Over 150 Method 25A calibration error checks were performed during the test program. The majority of these calibration error checks met the Method 25A criterion of $\pm 5\%$ of the gas concentration. Method 25A sample bias checks, as well as O₂ leak checks were also completed.

Method 18 QA/QC procedures were also followed. Initial and final calibrations were performed. Calibrations for ethanol and acetaldehyde were all completed using 3 to 5 calibration points. Multi-point calibrations were also performed on methane for low concentrations on all of the test days (< 900 ppmC). On the second Site 2 test day, a single point calibration was used on higher methane values. This procedure was not expected to effect data quality.

Sample bias checks were routinely conducted on the Method 18 sampling system and the majority verified acceptable non-biased sampling. However, some checks revealed sample bias caused by the loss of heat in the heated sample tubing adjacent to the gas chromatograph (GC). These data points were invalid and testing was discontinued until the problem was remedied and a successful bias check had been completed. More is discussed on this matter in Section 6.0.

1.4 Recommendations for Further Work

Further work is recommended to further characterize bakery emissions and to improve the test method. Compounds other than ethanol and acetaldehyde were not

detected by the Method 18 analyses. However, trace (<10 ppmv) levels of other compounds may be present in the bakery stream and although these compounds would not be expected to increase VOC emission rates, it would be interesting to identify them.

Another area which could be further examined is the comparison of Method 18 GC results to the Method 25A THC results. It was expected that the concentration of THC detected by the Method 25A analyzer would exceed the concentrations of the three targeted VOC compounds. However, throughout this test program, a higher concentration of compounds was determined by the GC than by the THC monitor. Comparisons were made by first correcting concentrations of each compound determined from the GC analysis from parts per million by volume (ppmv) to ppmv as Carbon (ppmC). This was done using the previously mentioned CECF of 1.42 for ethanol, 1.23 for acetaldehyde, and 1 for methane. The sum of the three corrected GC concentrations were then divided by the THC concentration. Typically, comparisons resulted in values of 120-140% of GC vs THC values. This error may be a result of inaccuracy in the CECF as it was applied to the sample gas matrix. Matrix effects may have somehow lowered the THC response (CECF) for ethanol as compared to the ethanol response in a dry, nitrogen calibration gas. Further work examining this Method 18 and Method 25A results comparison could be examined.

2.0 INTRODUCTION

2.1 Overview

The U.S. Environmental Protection Agency (U.S. EPA) has been requested to develop an alternative control technique (ACT) guidance document for controlling Volatile Organic Carbon (VOC) emissions from commercial baking operations. Interest has also been expressed in recalculating the AP-42¹ emission factors for bakery VOC emissions. Ethanol (C_2H_5OH) is the primary pollutant emitted from commercial bakeries.² Ethanol along with Carbon Dioxide (CO_2) is produced during the yeast metabolic process. Previous test data from bakeries has also revealed the presence of acetaldehyde (CH_3CHO).² Therefore, in conjunction with the development of an ACT document and new AP-42 emission factors, the U.S. EPA has contracted Radian Corporation to perform emissions testing of several commercial bakeries in order to gather the necessary background emissions data. This report will present the results of the U.S. EPA Bakeries test program for Site 2.

The test procedures used were the U.S. EPA Stationary Source Testing Method 25A for VOCs and Method 18 for methane, ethanol and acetaldehyde determinations. Method 25A was used to quantify total hydrocarbons (THC). Method 18 was employed to quantify methane and two of the most prevalent VOC compounds (acetaldehyde and ethanol) in the bakery emission stream. By combining both procedures, the VOC emissions were fully characterized.

As a part of this data gathering phase, U.S. EPA contracted Research Triangle Institute (RTI) to monitor the baking process parameters during the emissions

¹Compilation of Air Pollutant Emission Factors, Section 6.13, U.S. EPA (1972).

²Background Documentation for AP-42, Section 6.13, Bakeries, PES for U.S. EPA (1972).

tests. Items such as dough mixing process, fermentation (proofing) time, yeast concentration, production rates and others were monitored. However, this report will only present emissions data, that will be used with the process and production rate data to develop emission factors that will be presented in a separate document.

2.2 Test Objectives

The objectives of this test program was to determine VOC emission rates as well as ethanol and acetaldehyde emission rates. The data could then be used to determine of which air pollution control techniques would be effective for the bakery industry. As discussed above, it was also desirable to correlate the emissions data with process data to update and/or verify the emission factors for commercial bakeries.

2.3 Test Methods

Because each oven had at least two stacks, concentrations of THC were continuously and simultaneously monitored on each stack using two THC continuous emissions monitoring systems (CEMS). The THC data was typically recorded on every 10 seconds a computer disk. The resulting THC data were then averaged over each period of time corresponding to a distinct segment of the process operation (i.e., 30 minute sandwich bread baking process). Methane, ethanol and acetaldehyde concentrations were measured semi-continuously using discrete analyses by a Gas Chromatograph/Flame Ionization Detector (GC/FID). One GC/FID analyzer was used for this test program. One analysis of methane, acetaldehyde, and ethanol could be completed every 10 minutes; therefore, a full oven characterization could be completed every 20 minutes (2 stacks per oven).

Method 25A and Method 18 required extracting a sample stream of the gas from the stack through a heated Teflon® tube. A portion of the sample was directed to a THC analyzer which quantified THC on a real-time basis by a Flame Ionization

Detector (FID). The THC analyzer processes unconditional gas samples; therefore, concentrations are characterized ppmv, on a wet basis. A portion of the remaining gas stream was directed to the Method 18 gas chromatograph. The GC column separated individual hydrocarbons which were quantified with the FID.

Gas flow rate was determined by using the U.S. EPA Method 2. This method called for measuring the velocity of the gas stream and by multiplying it by the stack cross-sectional area, a volumetric flow rate was determined. Method 2 also called for point location determination to be made by Method 1, CO₂ and O₂ concentrations by Method 3 and moisture content by Method 4.

2.4 Data Reduction

As previously discussed, two sets of emission data were calculated. The first set presents VOC as ethanol emissions calculated using the Method 25A and the Method 18 methane test results. The second data set presents emission rates of ethanol and acetaldehyde calculated from the Method 25A and the Method 18 ethanol and acetaldehyde test results. The data reduction methods used are summarized in the following paragraphs.

Method 25A requires THC data to be reported in units of parts per million as Carbon (ppmC). Preliminary THC concentrations in units of ppmv as the calibration compound (i.e., propane) are multiplied by that respective compound's carbon equivalent correction factor (CECF) to correct the units to ppmC. The CECF for methane, ethane and propane are 1, 2 and 3, respectively. For example, if the Method 25A monitor was calibrated with propane, all resulting concentrations would be multiplied by the propane CECF of 3 to correct the concentration from ppmv as propane to ppmC. The THC values can be converted to ppmv of the compound of interest if 1) the specific CECF is known, and 2) the compound proportion of THC is known. For this test program, the THC monitors were calibrated with methane which has a CECF of 1, so the resulting

THC data was already in units of ppmC. However, correcting the THC concentration to VOC as ethanol concentration did require dividing the average non-methane THC concentration by the ethanol CECF. This process assumed that the non-methane hydrocarbons were made up entirely of ethanol. The resulting VOC as ethanol concentrations were then multiplied by the stack gas flow rates in order to determine VOC as ethanol emission rates.

Ethanol and acetaldehyde emissions were also calculated. Average ethanol and acetaldehyde concentrations were calculated by averaging the multiple Method 18 analytical results. However, only three Method 18 data points (per compound) were typically acquired per hour. In order to increase the number of data points in a given time period, the continuous Method 25A data was also used. An average ethanol-to-THC proportion from the above three analyses was calculated and then multiplied by the average THC value to calculate an average ethanol concentration. This method assumes that the ethanol-to-THC proportion is constant throughout the test run. Acetaldehyde calculations were performed in the same manner.

All data reduction procedures are fully explained in Section 7.0

2.6 Report Organization

A summary of the test results is presented in Section 3, a description of typical Oven Configurations and Sampling Locations is given in Section 4, and Sampling and Analytical Procedures are discussed in Section 5. Quality Assurance (QA) is presented in Section 6, and Data Reduction Procedures in Section 7. All field data and supporting calculations are included in the Appendices.

3.0 EMISSIONS RESULTS SUMMARY

This section will present the final results for the U.S. EPA Bakery Site 2 emissions test program. All raw data and calculations are included in the Appendices.

3.1 Test Program Summary

Four test sites were tested using Method 25A for THC determinations and Method 18 for methane, ethane, ethanol and acetaldehyde concentrations determinations. One of the test objectives was to quantify the VOC emissions which represent only the photochemically reactive volatile organic compounds. Non-reactive compounds such as methane and ethane are subtracted from the THC concentrations for determining VOC concentrations. The VOC concentrations and emissions for this test report were calculated by assuming that all of the non-methane hydrocarbons detected by the Method 25A tests were comprised of ethanol. This was consistently observed at all four test sites as ethanol concentrations determined from the Method 18 analyses typically made up over 98% of the total ethanol and acetaldehyde concentrations (target VOCs).

In Section 3, two sets of emissions data are given. The first data set presents emissions of VOC as ethanol as discussed above. The VOC concentration as ethanol was calculated by dividing the non-methane hydrocarbon concentration in units of ppmC by the ethanol THC Carbon Equivalent Correction Factor. The CECF was determined by observing the response of the THC analyzer to known concentrations of ethanol. The second data set presents emissions of ethanol and acetaldehyde emissions determined from the Method 18 ethanol and acetaldehyde results and the THC results. Emissions were calculated by multiplying the respective stack gas concentrations by the stack gas flow rate by the methods discussed above. All calculations are shown in Section 7.0.

Methane concentrations were higher than expected during the test program which did not allow for the resolution of the ethane GC peak at three of the test sites. However, ethane concentrations were expected to be fairly low and so the error in determining VOC is expected to be minimal.

The emissions of both direct- and indirect-fired ovens were measured (see Section 4.1.2) while baking a variety of bakery products. Production rate is the most critical factor related to the quantity of bakery VOC emissions. However, as discussed in the previous section, no product information or process data will be given in this report. The general category of ovens tested will be identified, differentiating direct-fired from indirect-fired and bread from bun ovens.

Thirty test runs were conducted for a typical sample period of 1 hour. Some of the runs were shorter than an hour due to the stoppage of the product being baked. Emissions was measured from only a single product at one time. Time periods when the ovens were in transient conditions, either from start up/shut down occurrences or from product changes or gaps in the product feed, were not included in the reported data base. However, all of the field data is included in the Appendices.

A general description of the commercial baking process and bakery ovens along with the types of ovens tested at each test site is given in Section 4. A total of two or three stacks were tested simultaneously from each oven. The total oven emissions were calculated by totaling the emissions from each of the stacks. Emissions from comfort hood stacks (see Figure 4-1) were not originally intended to be tested. However, it was noticed during the Site 2 test program that these emissions represented a significant portion of the total oven emission rates and from that point on, comfort hood emissions were tested.

3.2 Site 2 Test Results

A small bun oven, a small bread oven and a larger bread oven were tested at Site 2. These ovens were identified as Lines 1, 2, and 3, respectively. The first two ovens were tested with the CEM trailer location; however, the trailer had to be moved to test the third oven (Bread, Line 3).

All of the ovens tested at Site 2 had comfort hoods which were exhausted by an axial fan roof ventilator. There was no duct work following the fan; therefore, the U.S. EPA Method 1 specifications were not met. Flow measurements had to be taken directly at or after the fan since the gas was vented to atmosphere (see Figure 4-6). Therefore, the resulting emission rates may have a higher degree of measurement error.

The oven on Line 1 predominantly bakes buns. There was a front and rear stack as well as a comfort hood vent. The comfort hood fan was not operating during the test and may not have operated for sometime. Gas flow was induced strictly by natural drafting of the hot gases at velocities of 50-300 fpm and at temperatures of approximately 150°F.

The Line 2 was an indirect-fired unit. The oven gases were vented from a stack located in the front of the oven with the burner stack in the rear. As with the Bun oven, there was a comfort hood which was vented by a axial fan roof ventilator. There was no gas ductwork following the fan; therefore, the flow measurement could not be made at a location in accordance with U.S. EPA Method 1 procedures. Flows were estimated using both velocity pressure measurements and hot-wire anemometer measurements.

The Line 3 bread oven was a direct-fired unit with two stacks located approximately 90 feet apart and a comfort hood. The front stack and comfort hood were alternately sampled using the same sample system and THC monitor.

3.2.1 Site 2 Test Log

Seven emissions test runs (Runs 6-12) were conducted on June 17 and 18, 1992. Runs 6 and 10 were conducted on the Line 2 Bread oven, Run 7 was conducted on the Line 1 Bun oven, Runs 8,9 and 11 were conducted on the Line 1 and 2 comfort hoods, and Run 12 was conducted on the Line 3 bread oven stack. Five of the seven test runs were conducted on two ovens. Table 3-1 presents a summary of the Site 2 sampling activities.

3.2.2 Site 2 VOC as Ethanol Emissions Test Results

Table 3-2 presents the VOC as ethanol test results. The table presents THC concentrations (including methane) as well as VOC concentrations derived by removing the methane concentrations from the THC values (ppmC/wet). Concentrations of VOCs are also given in ppmv as ethanol, calculated as discussed above. Emission rates from each stack are calculated from the VOC as ethanol concentrations. The total oven VOC emissions are then calculated by totaling the emissions from both vent stacks.

3.2.3 Site 2 Ethanol and Acetaldehyde Emission Test Results

Table 3-3 presents the emission rates of ethanol and acetaldehyde and concentrations determined in two ways. The first method reports the ethanol concentration determined by averaging the results of the Method 18 analyses. The second method multiplies the average ethanol-to-THC ratio by the average THC value to determine average ethanol concentrations. The second method assumes a constant ethanol-to-THC proportion and by using the continuous THC data base (THC values every minute), incorporates a much larger data base for averaging. Ethanol emissions are calculated from concentrations determined by both methods. However, the total oven emissions were determined from concentrations using the THC data. Acetaldehyde

Table 3-1

Site 2 Bakery VOC Emissions Test Log EPA Bakeries (1992)

Run	Date	Sampling Time	Oven & Product Designation	Number of GC injections	
				Front	Rear
6	6/17/92	11:33-13:00	Bread E	3	0
7	6/17/92	15:17-16:14	Bun F	4	3
8	6/17/92	16:22-16:26	Bun Comfort Hood Only	1	NA ^a
9	6/17/92	16:40-16:43	Bread Comfort Hood Only	0	NA
10	6/17/92	16:47-17:47	Bread G	3	4
11	6/17/92	18:36-18:44	Bun/Bread Comfort Hood Only	0	0
12	6/18/92	15:22-19:13	Bread H	5	10

^aNA = Runs 8 and 9 were conducted on a single stack (comfort hood) for each run.

**Table 3-2. VOC Emissions Assuming 100 % Ethanol
EPA Bakeries, Site 2 (1992)**

Run	Run 6			Run 7		Run 8		Run 9		Run 10	
	Front	Burner		Front	Rear	Comfort ^e		Comfort ^e		Front	Burner
THC Conc. (ppmC/wet)	1637.5	52.7		1724.3	1398.3	1157.5		120.9		669.8	48.8
Methane Concentrations											
Methane Conc. (ppmv/wet) ¹	3.8	NO GC		33.1	28.5	13.2		NO GC		13.2	13.2
Methane/THC Ratio	0.003	NO GC		0.019	0.019	0.011		NO GC		0.004	0.047
Methane Conc. (ppmC/wet) ²	4.913	0 ^d		32.762	26.568	12.733		0 ^d		2.679	2.294
VOC Emissions											
VOC Conc. (ppmC/wet) ³	1632.6	52.7		1691.5	1371.7	1144.8		120.9		667.1	46.5
VOC Conc. as Ethanol (ppmv/wet) ⁴	1149.7	37.1 ^d		1191.2	966.0	806.2		85.1 ^d		469.8	32.8
VOC Emission Rate as Ethanol (lb/hr) ⁴	7.73	0.20		6.96	8.71	2.16		3.19		3.16	0.17
Total VOC Emissions as Ethanol (lbs/hr) ⁴	11.489 ^b			17.750 ^c		2.156		3.195		6.894 ^b	

¹ Values calculated from average methane concentrations determined from multiple GC analyses.

-- Values calculated from average Methane to THC ratios (CH₄/THC) incorporating both GC and THC analyses:

² Methane Conc. = Avg (CH₄ / THC_i) * (Avg THC)

³ VOC Conc. = Avg (1 - CH₄ / THC_i) * (Avg THC)

⁴ VOC Conc. as Ethanol = (VOC Conc) / 1.42 VOC Emissions as Ethanol = (VOC Conc. as Ethanol) * Flow;
where 1.42 is the empirically derived carbon equivalent correction factor

^a Assumed value taken from similar location.

^b Incorporated average Line 2 C.H. emissions of 3.56 ethanol Runs 9 & 11

^c Incorporated average Line 1 C.H. emissions of 2.08 ethanol from Runs 8 & 11

^d GC analyses was not performed for this location therefore the VOC concentration was assumed to be 100 % of the THC conc.

^e Runs 8 & 9 were conducted on the Line 1 and Line 2 Comfort Hood stacks only.

Table 3-2. VOC Emissions Assuming 100 % Ethanol, (cont.)
EPA Bakeries, Site 2 (1992)

Run	Run 11A	Run 11B	Run 12		
Stack Location	L1 C.H. ^b	L2 C.H. ^b	Front	Comfort	Rear
THC Conc. (ppmC/wet)	1067.6	148.7	4114.2	638.9	2992.1
Methane Concentrations					
Methane Conc. (ppmv/wet) ¹	NO GC	NO GC	1193	NO GC	1776.5
Methane/THC Ratio	NO GC	NO GC	0.402	NO GC	0.542
Methane Conc. (ppmC/wet) ²	0 ^a	0 ^a	1653.9	0 ^a	1621.7
VOC Emissions					
VOC Conc. (ppmC/wet) ³	1068 ^a	148.7 ^a	2460.3	638.9 ^a	1370.4
VOC Conc. as Ethanol (ppmv/wet) ⁴	751.8	104.7	1732.6	449.9	965.1
VOC Emission Rate as Ethanol (lb/hr) ⁴	2.0	3.93	25.17	2.26	13.51
Total VOC Emissions as Ethanol (lbs/hr) ⁴	2.011	3.929	40.94		

¹ Values calculated from average methane concentrations determined from multiple GC analyses.

-- Values calculated from average Methane to THC ratios (CH₄/THC) incorporating both GC and THC analyses:

² Methane Conc. = Avg (CH₄ / THC_i) * (Avg THC)

³ VOC Conc. = Avg (1 - CH₄ / THC_i) * (Avg THC)

⁴ VOC Conc. as Ethanol = (VOC Conc) / 1.42 VOC Emissions as Ethanol = (VOC Conc. as Ethanol) * Flow;
where 1.42 is the empirically derived carbon equivalent correction factor

^a GC analyses was not performed for this location; therefore, the VOC concentration was assumed to be 100 % of the THC conc.

^b Tests were done on the Line 1 and line 2 Comfort Hood stacks.

**Table 3-3. Ethanol and Acetaldehyde Emissions Test Results
EPA Bakeries, Site 3 (1992)**

Run	Run 6			Run 7		Run 8 ^d		Run 9 ^d		Run 10	
	Front	Burner		Front	Rear	Comfort		Comfort		Front	Burner
THC Conc. (ppmC/wet)	1637.5	52.7		1724.3	1398.3	1157.5		120.9		669.8	48.8
Ethanol Emissions											
Ethanol Conc. (ppmv/wet) ¹	1286.7	NO GC		1462.5	1190	1041		NO GC		509	S
Ethanol Conc. (ppmv/wet) ²	1498.3	48.2		1446.7	1230.5	1026.7		107.2		505.7	36.8
Ethanol/THC Ratio	0.915	0.915 ^a		0.839	0.88	0.887		0.887 ^a		0.755	0.755 ^a
Ethanol Emission Rate (lb/hr) ¹	8.65	NO GC		8.55	10.73	2.78		NO GC		3.42	S
Ethanol Emission Rate (lb/hr) ²	10.08	0.26		8.46	11.09	2.75		4.02		3.40	0.20
Total Ethanol Emission Rate (lbs/hr) ²	14.819 ^b			22.187 ^c		2.746		4.024		8.083 ^b	
Acetaldehyde Emissions											
Acetaldehyde Conc. (ppmv/wet) ¹	39.10	NO GC		60.10	46.20	26.60		NO GC		16.00	5.36
Acetaldehyde Conc. (ppmv/wet) ²	46.51	1.50		59.49	47.40	26.28		2.74		15.94	5.22
Acetaldehyde/THC Ratio	0.028	0.028 ^a		0.035	0.034	0.023		0.023 ^a		0.024	0.107
Acetaldehyde Emission Rate (lb/hr) ¹	0.252	NO GC		0.336	0.398	0.068		NO GC		0.103	0.027
Acetaldehyde Emission Rate (lb/hr) ²	0.299	0.008		0.333	0.4	0.067		0.099		0.103	0.027
Total Acetaldehyde Emission Rate (lbs/hr) ²	0.417 ^b			0.806 ^c		0.067		0.099		0.239 ^b	

¹ Values calculated from average concentrations determined from multiple GC analyses.

² Values calculated from average Ethanol/THC and Acetaldehyde/THC ratios (ETOH/THC and AA/THC) incorporating both GC and THC analyses: ETOH Conc. = Avg (ETOH_i/THC_i) * (Avg THC); ETOH Emissions = (Avg ETOH Conc.) * Flow
AA Conc. = Avg (AA_i/THC_i) * (Avg THC); AA Emissions = (Avg AA Conc.) * Flow

^a Assumed value taken from similar location.

^b Incorporated average Line 2 C.H. emissions of 4.49 ethanol and 0.110 acetaldehyde from Runs 9 & 11

^c Incorporated average Line 1 C.H. emissions of 2.64 ethanol and 0.065 acetaldehyde from Runs 8 & 11

^d Comfort Hood flow rates for this site were estimated based on velocity pressures or hot wire anemometer velocity measurements. Measurement locations did not meet EPA 1 specifications.

S Suspect GC ethanol results.

**Table 3-3. Ethanol and Acetaldehyde Emissions Test Results (cont.)
EPA Bakeries, Site 2 (1992)**

Run	Run 11 ^b			Run 12		
	L1 C.H.	L2 C.H.	Front	Comfort	Rear	
THC Conc. (ppmC/wet)	1067.6	148.7	4114.2	638.9	2992.1	
Ethanol Emissions						
Ethanol Conc. (ppmv/wet) ¹	NO GC	NO GC	2777.5	NO GC	1651	
Ethanol Conc. (ppmv/wet) ²	947.0	131.9	2686.6	566.7	1621.7	
Ethanol/THC Ratio	0.887 ^a	0.887 ^a	0.653	0.887 ^a	0.542	
Ethanol Emission Rate (lb/hr) ¹	NO GC	NO GC	40.35	NO GC	23.11	
Ethanol Emission Rate (lb/hr) ²	2.53	4.95	39.03	2.85	22.70	
Total Ethanol Emission Rate (lbs/hr) ²	2.533	4.949		64.577		
Acetaldehyde Emissions						
Acetaldehyde Conc. (ppmv/wet) ¹	NO GC	NO GC	112.40	NO GC	71.80	
Acetaldehyde Conc. (ppmv/wet) ²	24.23	3.38	107.79	14.50	70.31	
Acetaldehyde/THC Ratio	0.023 ^a	0.023 ^a	0.026	0.023 ^a	0.024	
Acetaldehyde Emission Rate (lb/hr) ¹	NO GC	NO GC	1.562	NO GC	0.961	
Acetaldehyde Emission Rate (lb/hr) ²	0.062	0.121	1.498	0.070	0.941	
Total Acetaldehyde Emission Rate (lbs/hr) ²	0.062	0.121		2.509		

¹ Values calculated from average concentrations determined from multiple GC analyses.

² Values calculated from average Ethanol/THC and Acetaldehyde/THC ratios (ETOH/THC and AA/THC) incorporating both GC and THC analyses: ETOH Conc. = Avg (ETOH_i/THC_i) * (Avg THC); ETOH Emissions = (Avg ETOH Conc.) * Flow
AA Conc. = Avg (AA_i/THC_i) * (Avg THC); AA Emissions = (Avg AA Conc.) * Flow

^a Assumed value taken from similar location.

^b Comfort Hood flow rates for this site were estimated based on velocity pressures or hot wire anemometer velocity measurements. Measurement locations did not meet EPA 1 specifications.

values were calculated similarly. All data reduction procedures is given in Section 7.

3.2.4 Site 2 Method 25A and Method 18 Results

This section presents the results from the Method 18 analyses. The Method 25A THC concentrations are given for same time period that the GC injections were made. Typically, three injections were made during a test run at a specific sample location. The concentrations were then averaged. Some GC injections were made that did not fall into the test run time-frame. Results from these analyses are presented in the tables but are not included in the averages. Ethanol-to-THC and acetaldehyde-to-THC ratios were calculated for each injection as well. The ethanol and acetaldehyde values were not corrected to ppmC for this calculation; therefore, these values cannot be considered volumetric proportions of the THC stream. Their purpose was to be multiplied by the average THC value to calculate average methane, ethanol, and acetaldehyde concentrations. This allowed ethanol and acetaldehyde concentrations to be calculated without incorporating the additional methane analysis.

Finally, a comparison of the total concentration of the three target compounds detected by the GC was made with the THC values for each discrete injection. This parameter is not required by the reference method QA procedures, but it was originally thought to be an indication what proportion of THC the three target compounds represented. It was expected that the sum of the GC concentrations would be somewhat lower than the total THC concentration taking into account trace concentrations of organics in the gas stream that were not detected by the GC analyses. However, this comparison may not be sufficiently accurate. The average ratio is calculated as follows:

$$\left(\frac{\overline{\text{GC}}}{\overline{\text{THC}}} \right) = \frac{\sum_{i=1}^N \frac{\text{GC}_i}{\text{THC}_i}}{N} \times 100$$

where:

THC_i = THC concentrations determined from the Method 25A monitor at the same time as the GC injection (ppmC)

N = Number of GC injectors in the time period.

The units from the GC analyses have to be corrected to the same units as the THC concentrations (ppmC) as follows:

$$\text{GC}_i = \left(\frac{[\text{ETOH}]_i}{1.42} + \frac{[\text{AA}]_i}{1.23} + [\text{CH}_4]_i \right)$$

where:

$[\text{ETOH}]_i$ = Ethanol concentration determined from a single GC analysis (ppmv/wet)

1.42 = Ethanol THC Carbon Equivalent Correction Factor (empirically derived)

$[\text{AA}]_i$ = Acetaldehyde concentration determined from a single GC analysis (ppmv/wet)

1.23 = Acetaldehyde THC Carbon Equivalent Correction Factor (empirically derived)

$[\text{CH}_4]_i$ = Methane concentration determined from a single GC analysis (ppmv/wet).

NOTE: The methane CECF is 1.0.

The CECFs used for this test program were determined by challenging the THC analyzer with known, certified concentrations of ethanol and acetaldehyde and recording the response. For example, if a 200 ppmv ethanol gas standard responded as 300 ppmC THC, then the ethanol CECF was 1.5. The CECFs were determined over the entire range of concentrations observed during the test program. It is difficult to predict whether the THC analyzer responded to the ethanol in the bakery sample gas matrix the same (quantitatively) as to ethanol in a clean, dry calibration gas. Both sample gas moisture levels and O₂ levels were different than the calibration gas matrix (dry, N₂ balance). The unexpected high GC/THC ratios (> 100%) may have resulted from a variability in the actual sample CECF.

Tables 3-4 and 3-5 present the Method 25A and Method 18 analytical results from the oven stacks and burner stacks, respectively. The ethanol-to-THC proportions for the Line 1 and Line 2 oven front stacks were approximately 0.8-0.9.

The Method 25A and Method 18 results for Site 2 are presented graphically in Figures 3-1 through 3-7, respectively. Method 18 concentrations have been corrected to ppmC for these plots.

3.2.5 Stack Gas Flow Rates

Table 3-6 presents the stack gas flow rates determined for the Site 2 oven stacks. Flows were not corrected to a dry basis since Method 25A and 18 concentrations were determined on a wet basis and emissions calculations required both flows and concentrations be consistently on the same basis (wet or dry). Moisture content values are included in the Appendix.

Table 3-4. Method 25A and Method 18 Emissions Tests Results, Front Stack, EPA Bakeries, Site 2 (1992).

FRONT/OVEN STACK										
RUN	TIME	METHOD 25A THC RESULTS ^a (ppmC/wet)	METHOD 18 GC RESULTS			GC/THC RATIO ^b (%)	THC PROPORTIONS ^c			
			ETHANOL (ppmv/wet)	METHANE ^d (ppmv/wet)	ACET- ALDEHYDE (ppmv/wet)		ETH/THC RATIO	CH4/THC RATIO	AA/THC RATIO	
6	11:32:49	1042.9	1062	0.00/0.83		37.8	149.223	1.018	0.002	0.036
6	11:45:49	1647.3	1338	3.60/0.67		29.6	117.849	0.812	0.003	0.018
6	11:55:49	1594.4	1460	2.30/1.26		49.8	134.172	0.916	0.003	0.031
6	AVG	1637.5	1266.7	3.8		39.1	133.7	0.915	0.003	0.028
	12:06:49	1696.8	1201	6.5		7.86	101.462	0.708	0.000	0.005
7	15:17:30	1778.2	1490	4.82/17.1		62.5	125.506	0.838	0.022	0.035
7	15:35:54	1590.6	1300	3.54/12.4		53.2	121.951	0.817	0.018	0.033
7	15:54:54	1801.3	1530	4.72/19.0		65.1	127.428	0.849	0.024	0.036
7	16:13:54	1792.9	1530	4.75/8.80		59.5	126.507	0.853	0.012	0.033
7	AVG	1724.3	1482.5	33.1		60.1	125.3	0.839	0.019	0.034
8	16:24:34	1173.9	1041	1.80/5.70		26.6	129.835	0.887	0.011	0.023
8	AVG	1157.5	1041.0	13.2		26.6	129.8	0.887	0.011	0.023
10	16:56:39	681.0	550	2.28/0.21		17.1	118.173	0.808	0.004	0.025
10	17:15:09	646.2	532	2.34/0.20		17	120.564	0.823	0.004	0.026
10	17:34:09	701.2	445	2.54/0.00		14	92.9283	0.635	0.004	0.020
10	AVG	669.8	509.0	2.7		16.0	110.6	0.755	0.004	0.024

^a THC averages calculated from the full CEM data base (not just the above entries)

^b GC/THC RATIO = (ETH/1.42+AA/1.23+CH4)/THC * 100 where: 1.42 = Ethanol CECF
1.23 = Acetaldehyde CECF

^c THC proportions were calculated as: ETH/THC = ppmv ethanol/ppmC THC, CH4/THC = ppmv CH4/ ppmC THC,

^d Methane/Ethane Values are reported here. Averages are in units of ppmC. AA/THC = ppmv acetaldehyde/ ppmC THC

Table 3-4. Method 25A and Method 18 Emissions Tests Results (cont),
Front Stacks, EPA Bakeries, Site 2 (1992).

FRONT/OVEN STACK									
RUN	TIME	METHOD 25A THC RESULTS ^a (ppmC/wet)	METHOD 18 GC RESULTS			GC/THC RATIO ^b (%)	THC PROPORTIONS ^c		
			ETHANOL (ppmv/wet)	METHANE (ppmv/wet)	ACET- ALDEHYDE (ppmv/wet)		ETH/THC RATIO	CH4/THC RATIO	AA/THC RATIO
NA	16:21:55	813.4	2900	491	97.7	609.9	3.565	0.604	0.120
12	16:03:46	4250.1	3290	826	125	133.0	0.774	0.194	0.029
12	18:23:16	3907.5	2590	1411	91.4	133.1	0.663	0.361	0.023
12	18:42:16	4588.5	2390	1540	131	111.0	0.521	0.336	0.029
12	19:01:16	4320.7	2840	1330	102	127.0	0.657	0.308	-0.024
12	AVG	4114.2	2777.5	1193.0	105.5	126.0	1.352	0.402	0.049

^a THC averages calculated from the full CEM data base (not just the above entries)

^b GC/THC RATIO = (ETOH/1.42+AA/1.23+CH4)/THC * 100 where: 1.42 = Ethanol CECF
1.23 = Acetaldehyde CECF

^c THC proportions were calculated as: ETH/THC = ppmv ethanol/ppmC THC, CH4/THC = ppmv CH4/ ppmC THC,
AA/THC = ppmv acetaldehyde/ ppmC THC

Table 3-5. Method 25A and Method 18 Emissions Tests Results, Rear Stack, EPA Bakeries, Site 2 (1992).

REAR/BURNER STACK										
RUN	TIME	METHOD 25A THC RESULTS ^a (ppmC/wet)	METHOD 18 GC RESULTS			GC/THC RATIO ^b (%)		THC PROPORTIONS ^c		
			ETHANOL (ppmv/wet)	METHANE ^d (ppmv/wet)	ACET- ALDEHYDE (ppmv/wet)			ETH/THC RATIO	CH4/THC RATIO	AA/THC RATIO
7	15:27:54	1763.4	1200.0	3.76/13.9 ^d		50.1	101.918	0.834	0.018	0.035
7	15:45:54	1475.7	1250.0	4.10/14.8		49.9	126.723	0.847	0.023	0.034
7	16:03:54	1166.1	1120.0	2.57/8.80		38.5	142.170	0.960	0.017	0.033
7	AVG	1396.3	1190.0	28.5		46.2	123.6	0.860	0.019	0.034
10	16:48:09	56.3	85.7	2.02/.53		4.63	231.935	1.523	0.055	0.082
10	17:06:09	57.2	195.0	3.85/ND		7.24	499.841	3.410	0.067	0.127
10	17:24:39	38.0	97.8	2.54/ND		4.6	380.360	2.574	0.067	0.121
10	17:44:09	51.8	115.0	1.96/0.59		4.96	333.332	2.222	0.061	0.096
10	AVG	384.0	123.4	3.2		5.4	361.4	2.432	0.062	0.106

^a THC averages calculated from the full CEM data base (not just the above entries)

^b GC/THC RATIO = (ETOH/1.42+AA/1.23+CH4)/THC * 100 where: 1.42 = Ethanol CECF
1.23 = Acetaldehyde CECF

^c THC proportions were calculated as: ETH/THC = ppmv ethanol/ppmC THC, CH4/THC = ppmv CH4/ ppmC THC,

^d Methane/Ethane values reported here. Averages in units ppmC.

AA/THC = ppmv acetaldehyde/ ppmC THC

ND = Not detected

Table 3-5. Method 25A and Method 18 Emissions Tests Results (cont), Rear Stacks, EPA Bakeries, Site 2 (1992).

REAR/BURNER STACK									
RUN	TIME	METHOD 25A THC RESULTS ^a (ppmC/wet)	METHOD 18 GC RESULTS			GC/THC RATIO ^b (%)	THC PROPORTIONS ^c		
			ETHANOL (ppmv/wet)	METHANE (ppmv/wet)	ACET- ALDEHYDE (ppmv/wet)		ETH/THC RATIO	CH4/THC RATIO	AA/THC RATIO
12	15:54	3146.6	1710.0	1980.0	78.4	143.2	0.543	0.629	0.025
12	16:12:46	3105.4	1750.0	1550.0	82.0	133.2	0.564	0.499	0.026
12	16:30:46	2944.3	1820.0	1970.0	78.2	158.0	0.618	0.669	0.027
12	16:49:16	2900.5	1580.0	185.0	19.0	84.5	0.545	0.064	0.007
12	17:22:46	3040.4	1220.0	1990.0	72.3	125.4	0.401	0.655	0.024
12	17:52:46	2974.9	1390.0	2050.0	74.3	138.3	0.467	0.689	0.025
12	18:04:16	2798.2	1480.0	2030.0	66.7	150.6	0.509	0.698	0.023
12	18:33:16	2934.0	1660.0	1960.0	76.9	150.4	0.566	0.668	0.026
12	18:51:46	3177.2	1850.0	1940.0	83.4	147.0	0.582	0.611	0.026
12	19:10:16	3259.6	2050.0	2110.0	86.4	157.3	0.629	0.647	0.027
12	AVG	2992.1	1651.0	1776.5	71.8	138.6	0.542	0.583	0.024

^a THC averages calculated from the full CEM data base (not just the above entries)

^b GC/THC RATIO = (ETOH/1.42+AA/1.23+CH4)/THC * 100 where: 1.42 = Ethanol CECF

1.23 = Acetaldehyde CECF

^c THC proportions were calculated as: ETH/THC = ppmv ethanol/ppmC THC, CH4/THC = ppmv CH4/ ppmC THC,

AA/THC = ppmv acetaldehyde/ ppmC THC

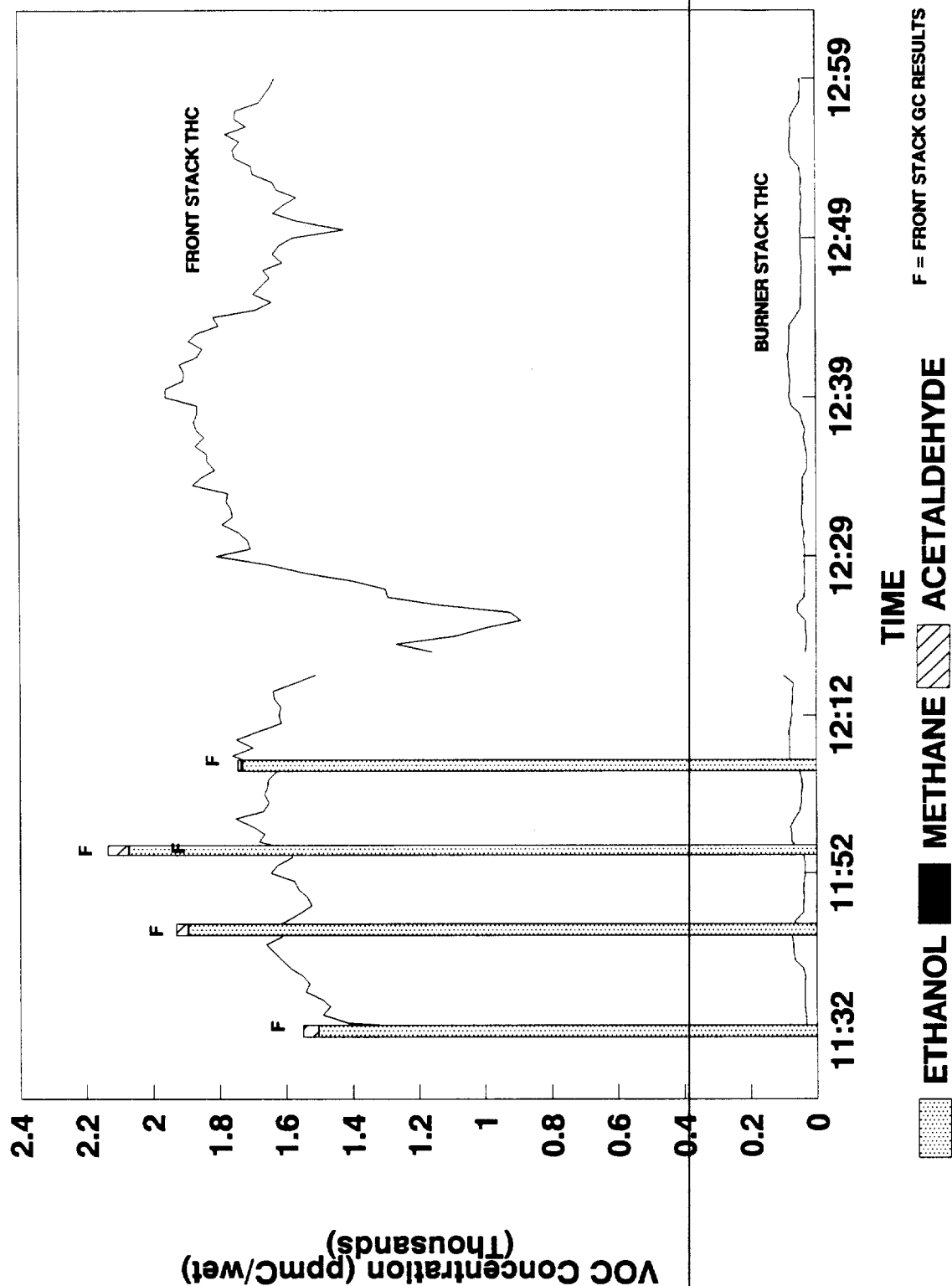


Figure 3-1. Run 6 Method 25A and Method 18 Results (adjusted to ppmC) .

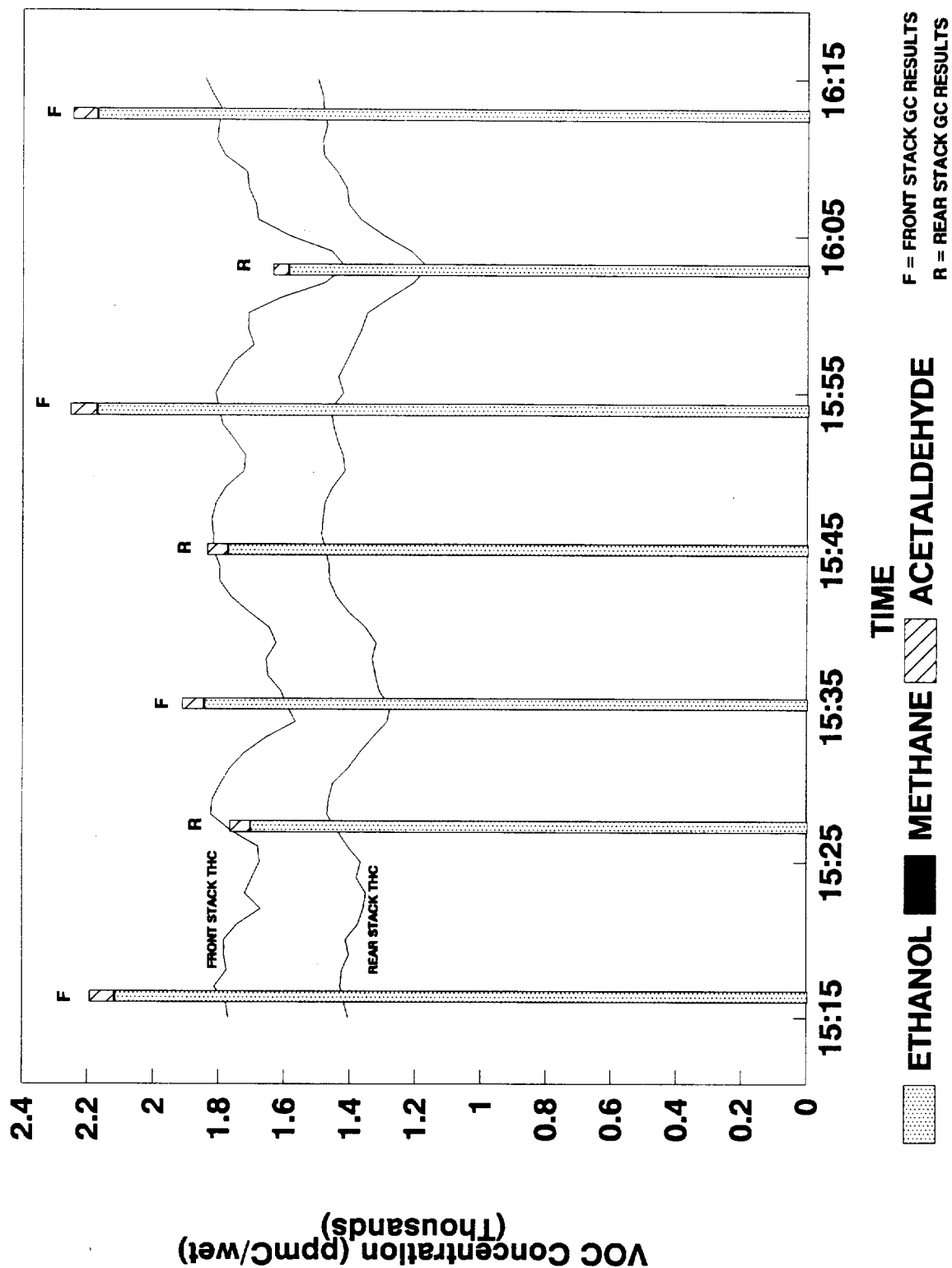


Figure 3-2. Run 7 Method 25A and Method 18 Results (adjusted to ppmC) .

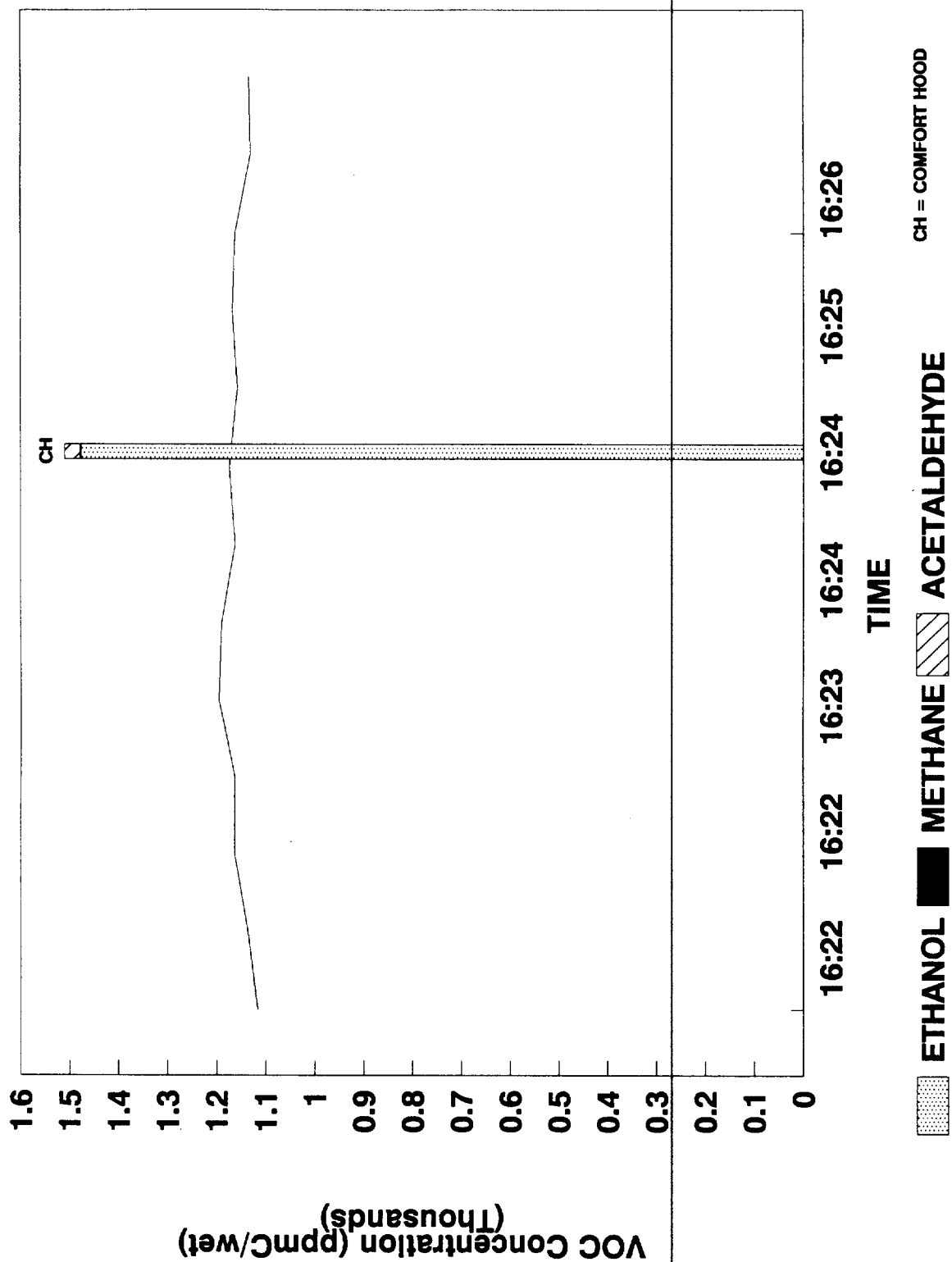


Figure 3-3. Run 8 Method 25A and Method 18 Results (adjusted to ppmC) .

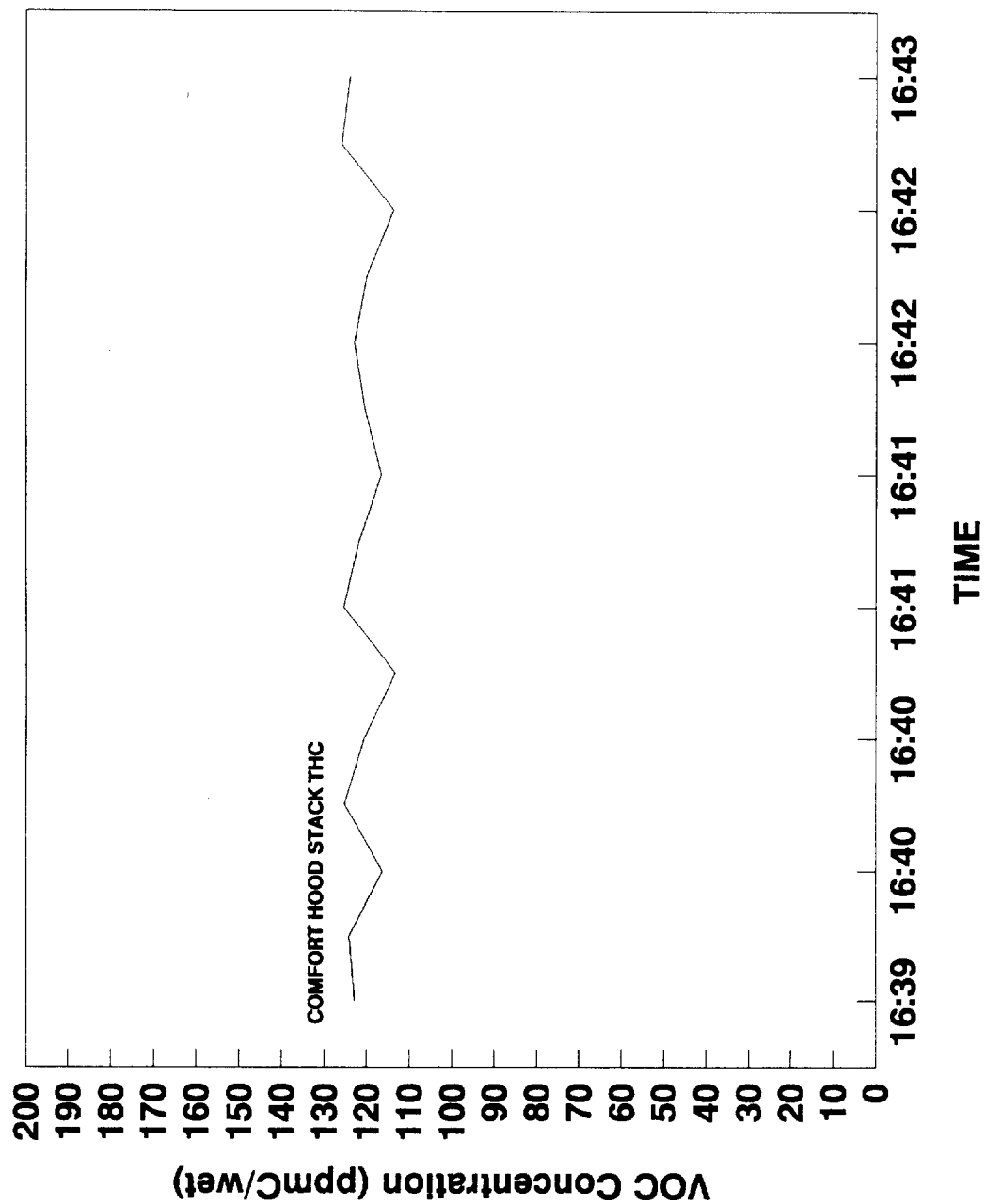


Figure 3-4. Run 8 Method 25A and Method 18 Results (adjusted to ppmC) .

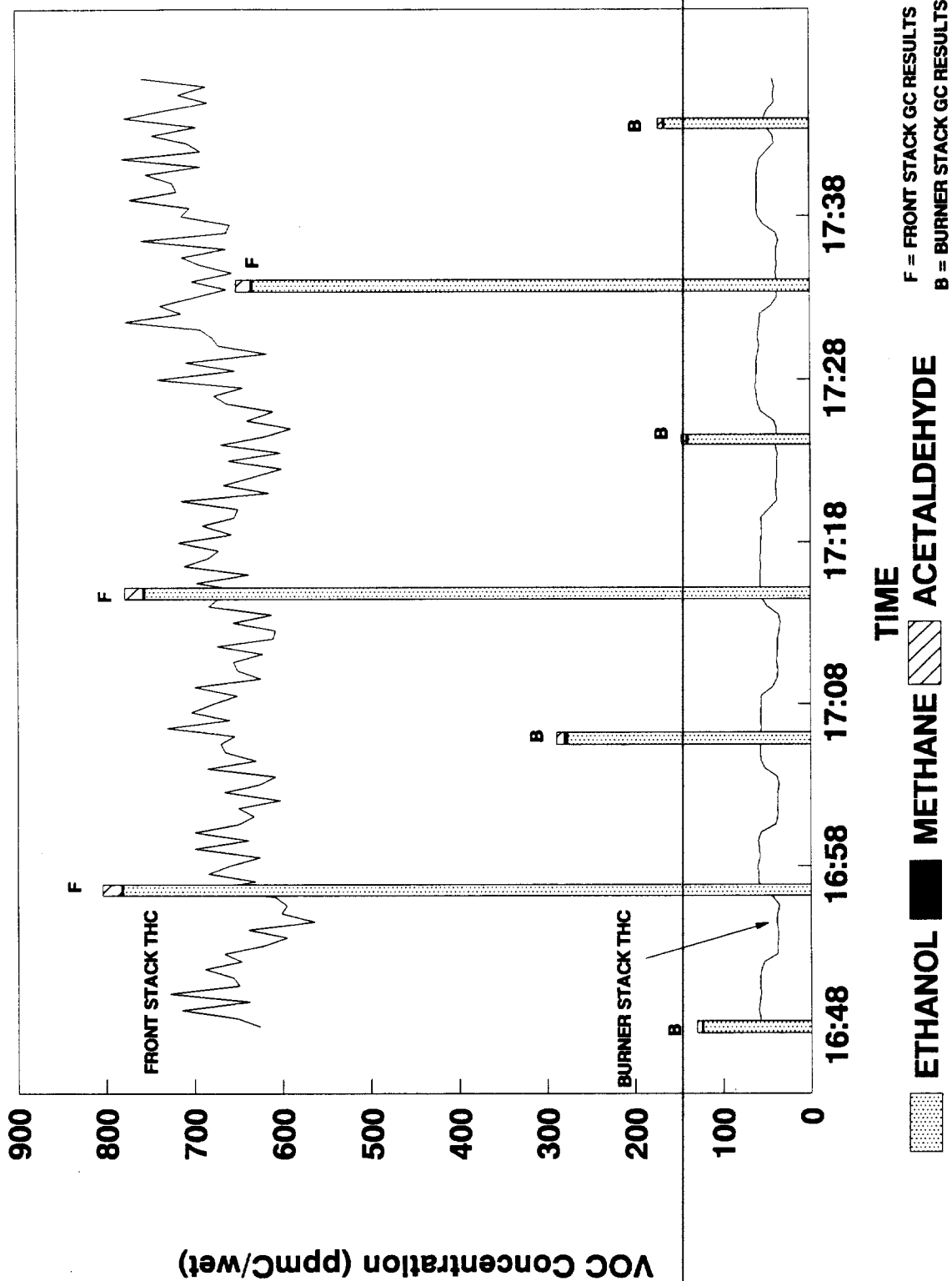


Figure 3-5. Run 10 Method 25A and Method 18 Results (adjusted to ppmC) .

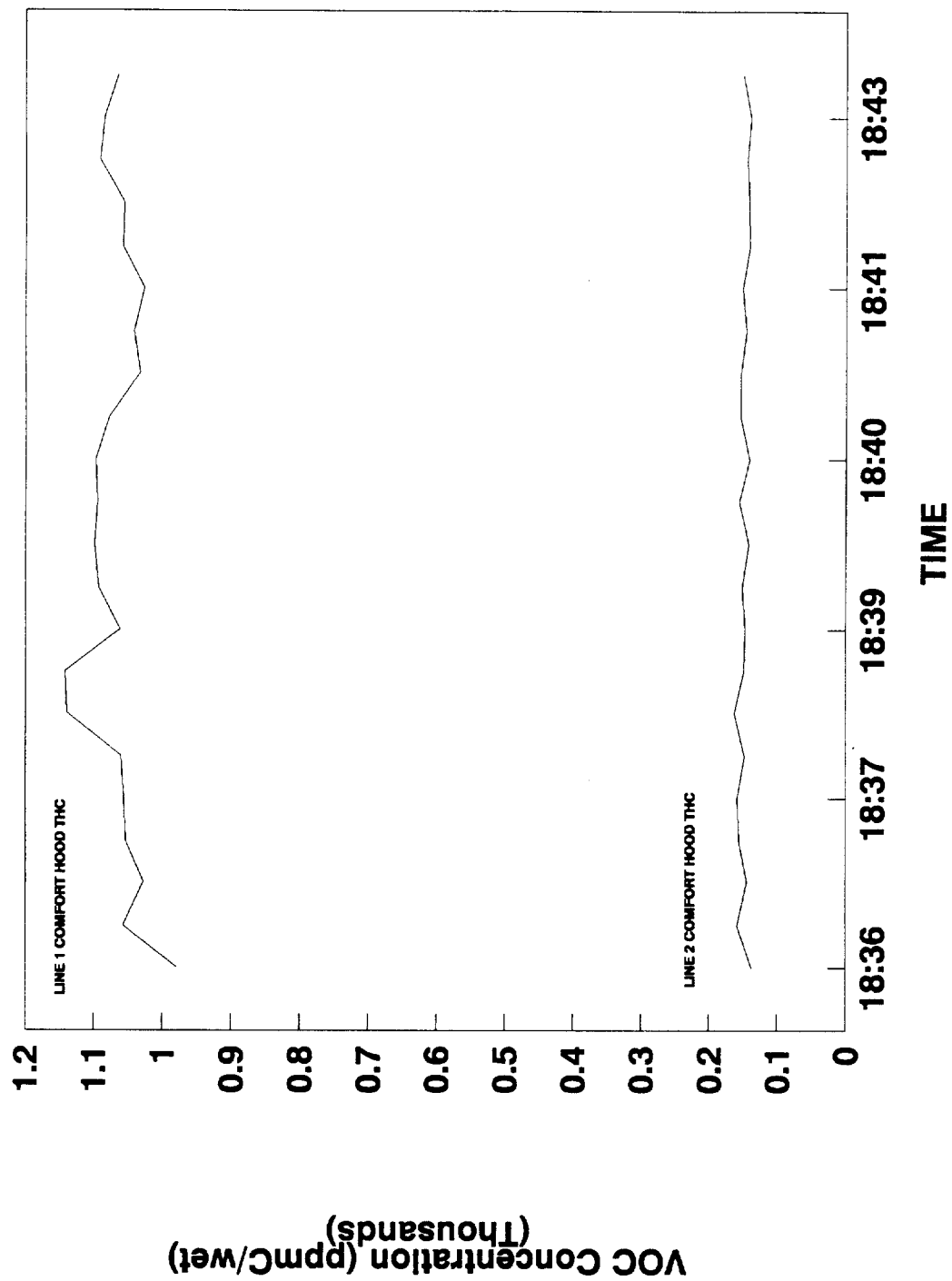


Figure 3-6. Run 11 Method 25A Results (adjusted to ppmC) .

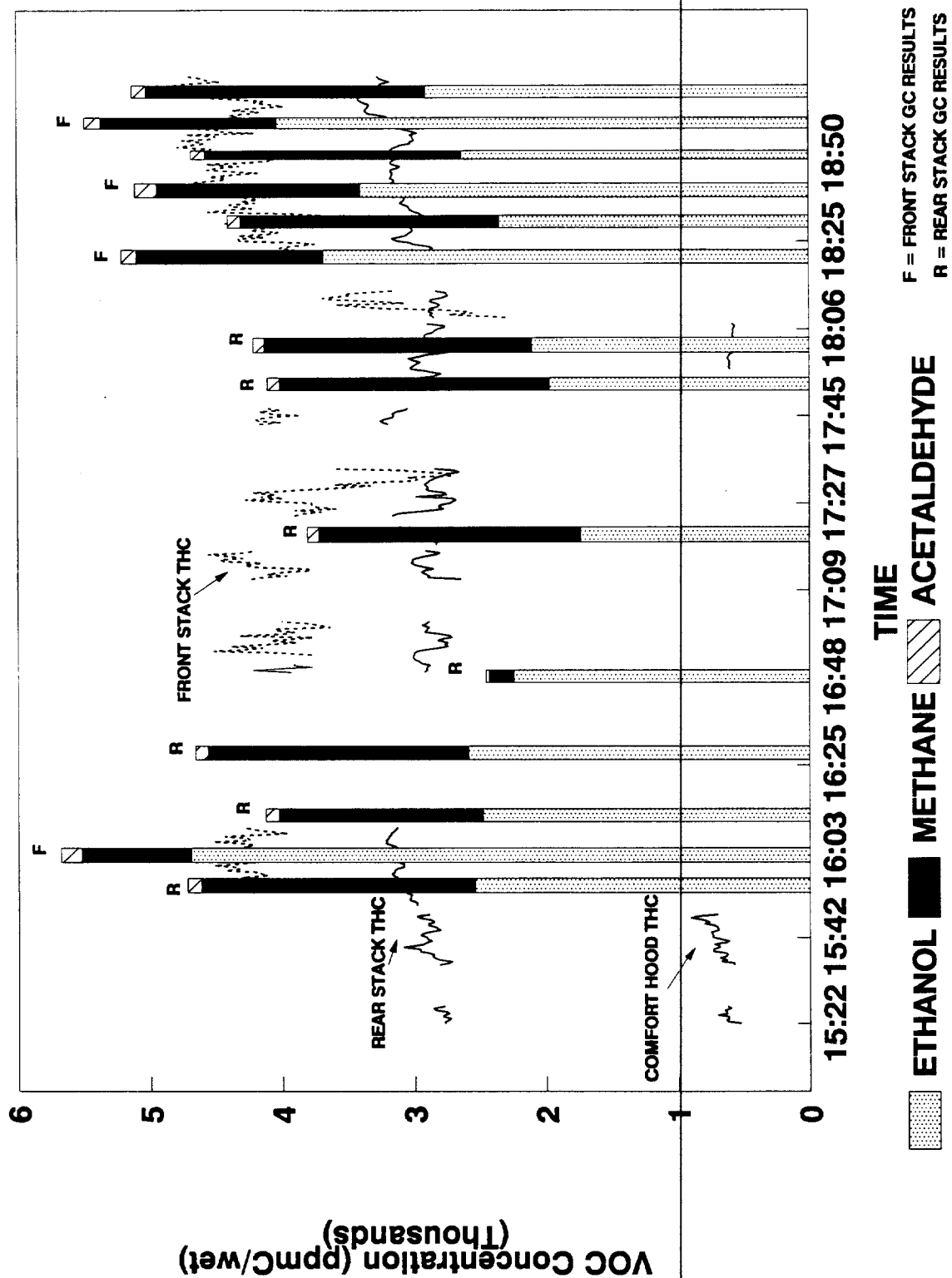


Figure 3-7. Run 12 Method 25A and Method 18 Results (adjusted to ppmC) .

**Table 3–6. Summary of Flue Gas Sampling Parameters
Site 2 (1992)**

Run Number	Location	Stack Gas Temperature (deg F)	Barometric Pressure (in. Hg)	Stack Gas Static Pressure (in H ₂ O)	Volumetric Flow Rate (acfm)	Volumetric Flow Rate (scfm)
Run 6	Front	230	30.21	–0.1	1,216	939
	Burner	316	30.21	–0.05	1,083	744
Run 7	Front	269	30.21	–0.1	1,116	811
	Rear	309	30.21	–0.2	1,816	1,251
Run 8	Comfort	207	30.21	0	467	371
Run 9	Comfort	108	30.21	0	5,585	5,242
Run 10	Front	230	30.21	–0.1	1,216	939
	Burner	316	30.21	–0.2	1,083	744
Run 11	L1 C.H.	207	30.21	0	467	371
	L2 C.H.	108	30.21	0	5,585	5,242
Run 12	Front	216	30.01	–0.25	2,593	2,013
	Comfort	100	30.01	0	742.45	702.12
	Rear	214	29.75	–0.15	2512.22	1,957

Table 3-7 presents the ethanol carbon equivalent correction factor (CECF) determination. As discussed before, the CECF is the relative response of the THC analyzer in units of ppmC to known concentrations of ethanol. The CECF was determined for both ethanol and acetaldehyde by observing the response of the THC analyzer in units of ppmC to known gas concentrations of the two target compounds. The observed response was divided by the known concentration to determine the CECF value. This was done both in the field and in the laboratory. Ethanol challenges were made in the field at only one concentration (typically 200 ppmv); therefore, it was decided to develop the ethanol CECF over a much wider range of concentrations that were encountered in the field. The CECF value used for this test program was determined in the laboratory using a wide range of ethanol concentration. The average CECF for ethanol was determined to be 1.42. The on-site ethanol QC challenges are presented in Section 6.0.

Table 3-8 presents the acetaldehyde CECF determination. This procedure was performed in the field with a single concentration of acetaldehyde. Only relatively low sample concentrations were observed during the test program (< 50 ppmv); therefore, extensive CECF development did not need to be completed. The acetaldehyde CECF used for this test program was 1.23.

**Table 2-7. In-House Ethanol Carbon Equivalent Corretion
Factor Determination. EPA BAkeries (1992)**

Ethanol QC Gas Conc. (ppmC)	Instrument Response (ppmC)	Carbon Equivalent Correction Factor
498	628	1.26
1000	1294	1.29
1470	2055	1.40
2000	2773	1.39
1470	2022	1.38
1470	2097	1.43
498	732	1.47
1000	1499	1.50
1470	2287	1.56
2000	2997	1.50
	AVG	1.42

**Table 2-8. Acetaldehyde Carbon Equivalent Correction
Factor Determination. EPA Bakeries (1992)**

Site	Test Day	Ethanol QC Gas Conc. (ppmC)	System 1		System 2	
			THC Instrument Response (ppmC)	Carbon Equivalent Correction Factor	THC Instrument Response (ppmC)	Carbon Equivalent Correction Factor
1	2	82.5	101.5	1.23	103.5	1.25
3	2	82.5	98.9	1.20	101	1.22
4	3	82.5	103.5	1.25	107	1.30
4	4	82.5	DOWN		100.5	1.22
			AVG	1.23	AVG	1.26

4.0 OVEN CONFIGURATIONS AND SAMPLING LOCATIONS

This section presents a general discussion of the oven stack locations, sampling port locations, and flow traverse point locations. Specific information is given for the Site 2 test program. The U.S. EPA Method 1 guidelines were used to determine the majority of test locations measuring gas flow rates. Method 25A and 18 samples were taken from the same port that the flow measurements were made. The sample point was located near the centroid of the duct (centrally located 10% area of the stack cross-section). All locations were at least 2 diameters upstream from the gas discharge to the atmosphere as required in Method 25A.

4.1 General Process Description

The following sections present a general description of the baking process and commercial baking ovens. It is not within the scope of this document to present detailed process information or production rates; therefore, these descriptions are only meant to familiarize the reader of the general principles and equipment used in the commercial baking industry.

4.1.1 Baking Process Description¹

Bread baking at large commercial bread bakeries is a highly-mechanized process consisting of high-speed production lines with ovens capable of baking 20,000 pounds or more of bread per hour. The process starts with the mixing of flour, water, sugar, and yeast to form dough, thereby initiating a long series of complex biochemical changes which ends in the oven where the bread is baked.

¹ Compilation of Air Pollutant Emission Factors (AP-42), Chapter 13.01, Bread Baking (Final Draft 1991)

There are four basic types of dough mixing processes: sponge dough, straight dough, brew, and continuous mix ("no-time"). These processes vary in the manner in which the various dough ingredients are mixed which determines the fermentation time available. Fermentation time can vary from 20 minutes or less for the continuous mix or "no-time" process, to 5 hours or more in the sponge dough process. The continuous mix or "no-time" process consists of mixing all of the dough ingredients at the same time; therefore, the fermentation time is minimized by using processing agents and higher temperatures. Sponge dough is formed when two-thirds of the flour, part of the water and the yeast are initially mixed and allowed to ferment before the remaining ingredients are added.

The baking process actually occurs in the oven which causes expansion of the loaf to final volume, crust formation, yeast and enzymatic activity inactivation, coagulation of dough proteins, partial gelatinization of starch, and reduction of loaf moisture. All of these processes are necessary to produce high quality, saleable bread products. To accomplish all of these product and process effects in the proper sequence, commercial bread ovens have between three and eight temperature gradient zones which are maintained in critical balance. Oven rise, which determines the final loaf volume and internal texture, occurs during the first 5-6 minutes of baking. Thermal degradation of the yeast occurs when the internal bread temperature reaches 140-145 °F which stops the fermentation process. Protein is denatured between 140-180 °F. At the end of the process, browning and crust color develop while ethanol and moisture are evaporated to cool the loaf and prevent the internal temperature from reaching the boiling point of water.²

²J. W. Stitley, Baking Technology, Oven Emissions and Control Devices, American Institute of Baking, Manhattan, KS (1986).

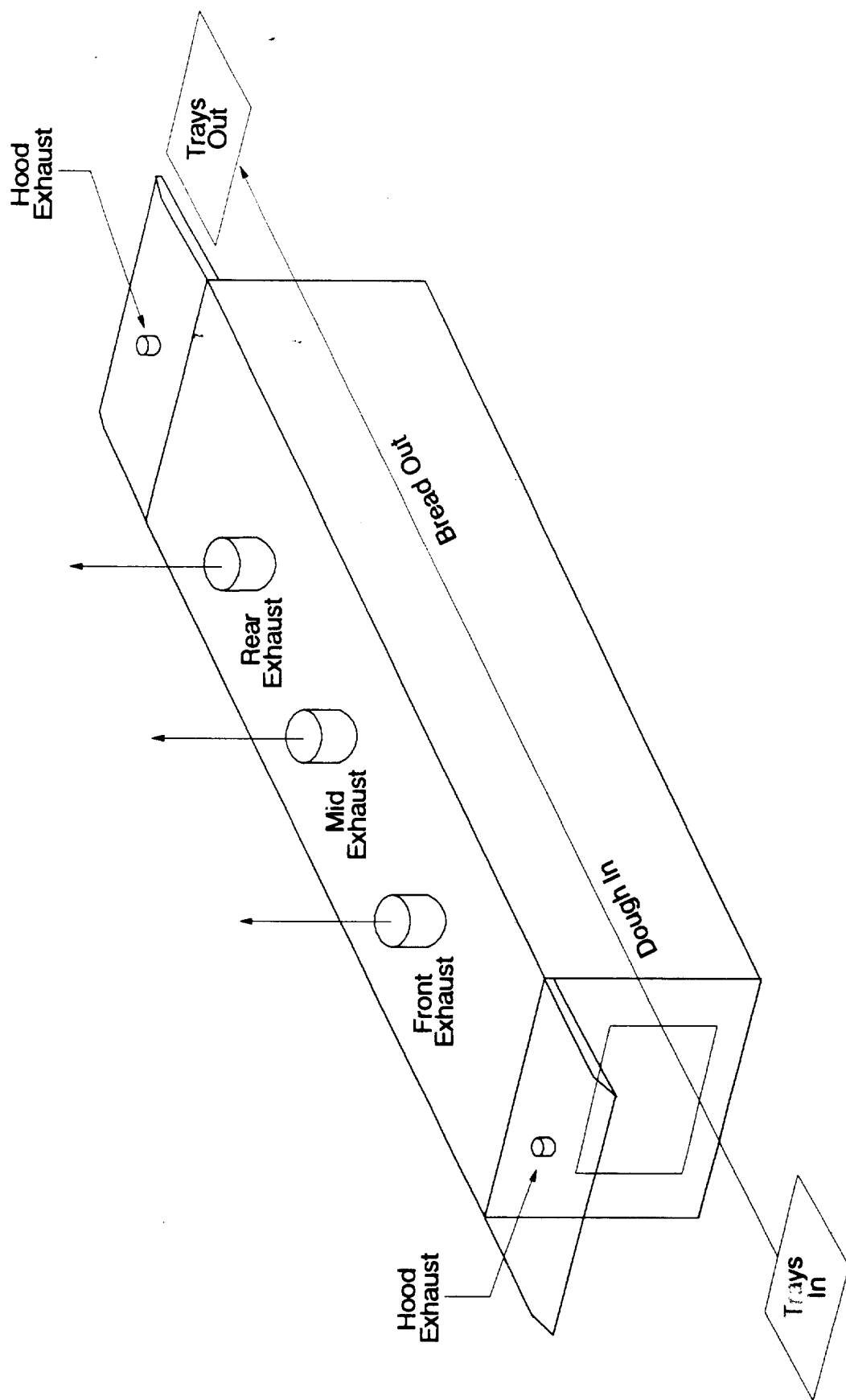
There are three fundamental oven types: tunnel, tray, and spiral. Tunnel ovens, as shown in Figure 4-1 are long horizontal ovens where dough enters at one end and is conveyed to the opposite end where it exits as bread. Tray ovens as shown in Figure 4-2 are also horizontal; however, the dough enters the oven and exits on the same side after being conveyed the length of the oven. The tray is lowered to a second level and then conveyed to the exit near where it entered. In spiral ovens, dough enters at the top corner of the oven and is conveyed in a downward spiral to the bottom corner of the oven where it exits through an opening diagonally lower from where it entered the oven. No spiral ovens were tested during this test program. Tunnel and tray ovens typically contain three to five exhaust stacks with one stack typically used for purging the oven of natural gas during ignition and the remaining stacks used during normal baking operations. In contrast, spiral ovens usually contain just one stack which is used during both purging and normal operations.³

4.1.2 Oven Heating Systems⁴

Ovens may be divided into two general categories according to the manner in which they are heated, namely, direct-fired ovens and indirect-fired ovens. A third category makes use of semi-direct heating. In direct-fired ovens, the burners are located directly within the baking chamber and are usually ribbon type and burn natural gas. Modern ovens normally feature banks of ribbon burners located both above and below the baking surface, across the path of travel of the baking trays or oven band. Most such ovens are equipped with an external forced-air agitation system to augment the naturally formed convection currents within the baking chamber.

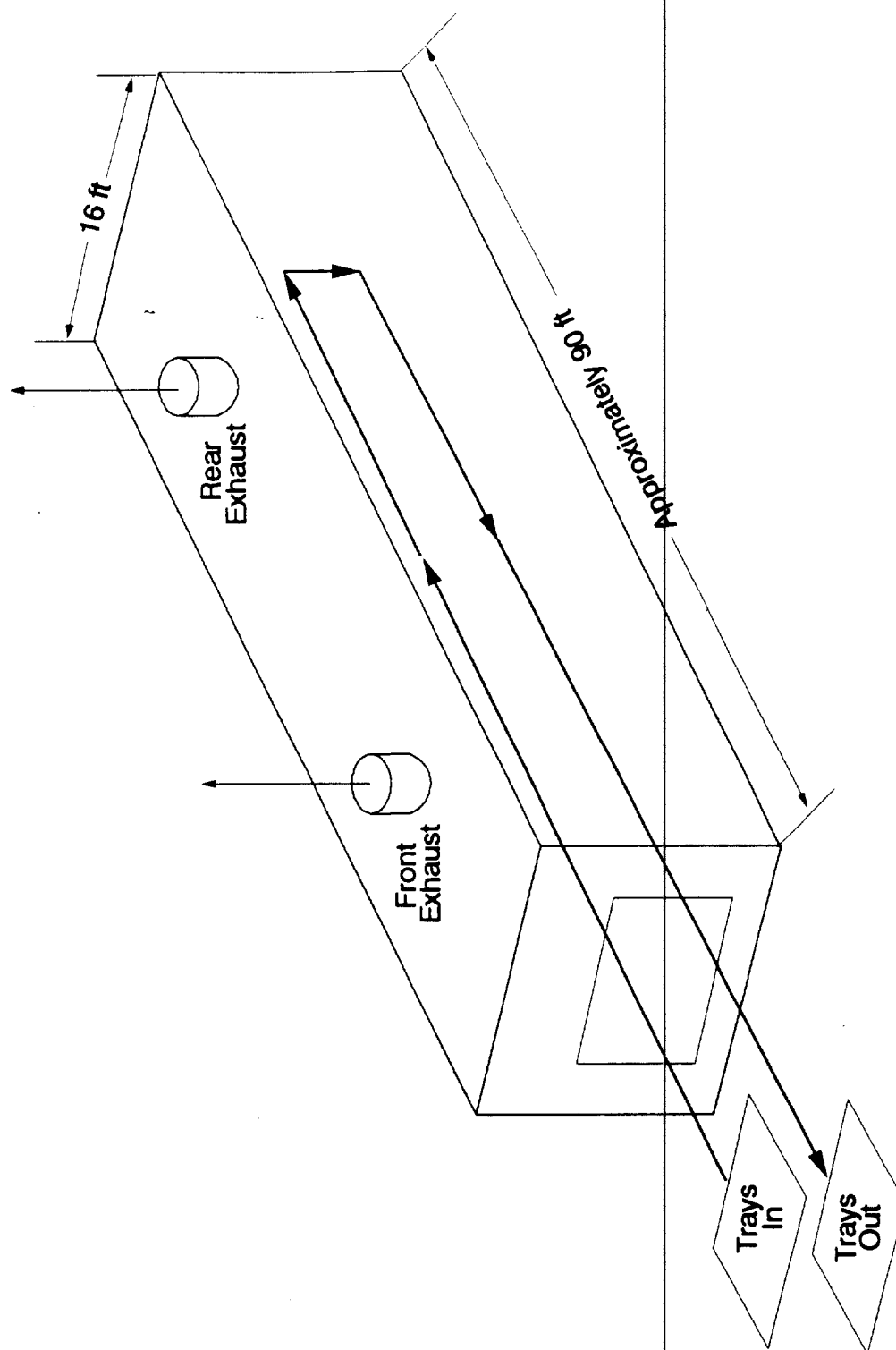
³BAAQMD Staff Report Supporting Adoption of Rule 8-42 (July 1988).

⁴ The Science of Baking, Lesson 26 Bakery Ovens, American Institute of Baking (no date)



4-4

Figure 4-1. Generalized Schematic of a "Tunnel" Type Baking Oven
EPA Bakeries (1992)



**Figure 4-2. Generalized Schematic of a "Tray" Type Baking Oven
EPA Bakeries (1992)**

In indirect-fired ovens, the combustion chamber is isolated from the baking chamber. The heat is transferred from the hot combustion gases to the baking chamber by means of flues or radiator tubes. In these ovens, the products of combustion do not enter the baking chamber and thus do not come into direct contact with the baking products. The heat is generated by single high-capacity burners (one burner for each oven zone) and radiant heat is supplied by the flues and radiators within the baking chambers. Forced air agitation systems and improved oven efficiency are a general feature of indirect-fired ovens.

Semi-direct fired ovens (which are also referred to as semi-indirect fired ovens) closely resemble indirect-fired ovens in their use of separate combustion chambers and of radiator tubes for the heat transfer. In their case, however, the radiator tubes have either thin slots or small holes that allow the hot combustion gases to enter the baking chamber. These gases create convection currents whose intensity can be controlled by means of baffles. Thus, semi-direct fired ovens combine the advantages of both convection and radiant heat transfers.

4.2 Test Program Overview

This section will present a general discussion of the oven types and sample locations from all four sites. However, specific information will only be presented for the Site 2 facility.

This test program involved measuring the emissions from both direct- and indirect-fired ovens. Some of the indirect fired units had their heat exchanger tubes drilled out to promote better heating efficiency. However, maintenance records were incomplete and plant personnel were uncertain whether this had been completed or not. In some instances, maintenance personnel stated that their indirect-fired ovens had not been drilled out and yet high concentrations of unburned methane (> 1000 ppmv) were detected in the stack gases. So a strict direct/ indirect firing classification was not always possible.

Another important facet of the test program was that during steady-state operation, the gas flow in some of the stacks would almost be completely shut off with a flow damper to prevent oven heat loss. The Method 25A and 18 tests would detect fairly high concentrations of THC (> 1000 ppmC) while flow rates would be minimal (< 100 cfm), resulting in fairly low emissions rates. The flow damper positions were always verified to ensure they were the same during both flow measurement tests and the Method 25A and 18 tests.

The majority of ovens tested had two stacks venting exhaust gases. If both stacks vented oven (baking) gases (i.e., direct-fired), they were referred to as the front stack and the rear stack depending on their respective location. Front stacks were located near the end of the oven where the bread dough entered, and the rear stacks were on the opposite end.

Indirect-fired ovens also typically had two stacks with one stack exhausting the oven gases and the other exhausting the burner gases. Gases from the burner stack were expected to be comprised mainly of unburned hydrocarbons (i.e. methane). However as previously mentioned, oven maintenance records were sometimes incomplete and what was expected to be purely a burner exhaust gas stream, was sometimes comprised of significant portions of gases from the baking processes (i.e. ethanol and acetaldehyde).

Three sites had a third stack (typically referred to as comfort hoods) venting the gases, which was either adjacent to the oven entrance or to the exit. (See Figure 4-1). Their purpose was to remove fugitive oven heat from worker areas. Gases were pulled from these locations through a ventilation hood configuration, typically spanning the width of the oven (10-15 feet) and 1 - 3 feet in length. Exhausts from the Site 2 comfort hoods were pulled through roof ventilator fans which had very little ductwork downstream of an axial fan. This made determining flow rates inaccurate since

measurement locations could not be located in accordance with the U.S. EPA Method guidelines.

The majority of stacks were small roof vent ducts with an inside diameter (ID) ranging from 12 to 16 inches. As shown in Figures 4-1 and 4-2, the stacks were typically arranged in a straight line (i.e., in line with the orientation of the oven). Most had rain caps installed over the opening which was typically 6-15 feet above the roof. All stacks were accessed from the roofs of the facilities and sample ports were located from 2-6 feet above the roof line. A 1.75 inch hole in the duct walls allowed for full insertion of the Method 25A and 18 sample probe. Two ports were located 90° apart at the same elevation. The sample port that was not being used was always capped off to prevent any ambient air from diluting the sample stream.

Approximately 100 to 150 feet of heated Teflon® tubing was used to transport the gas sample from the stack to the mobile continuous emissions monitoring (CEM) vehicle that was typically parked adjacent to the bakery wall. In cases where there were three stacks originating from the oven, one sampling probe/heat trace system would be alternated from the second and third stack.

A general description of sample locations for the Site 2 test program is presented according to the respective test site in the following section.

4.3 Site 2 Sample Locations

A small bun oven, a small bread oven and a large bread oven were tested at the Site 2. These ovens were also identified as Lines 1 through 3, respectively. Line 1 and 2 ovens were tested with the CEM trailer parked in the same parking location. The trailer had to be moved to test the third oven (Line 3).

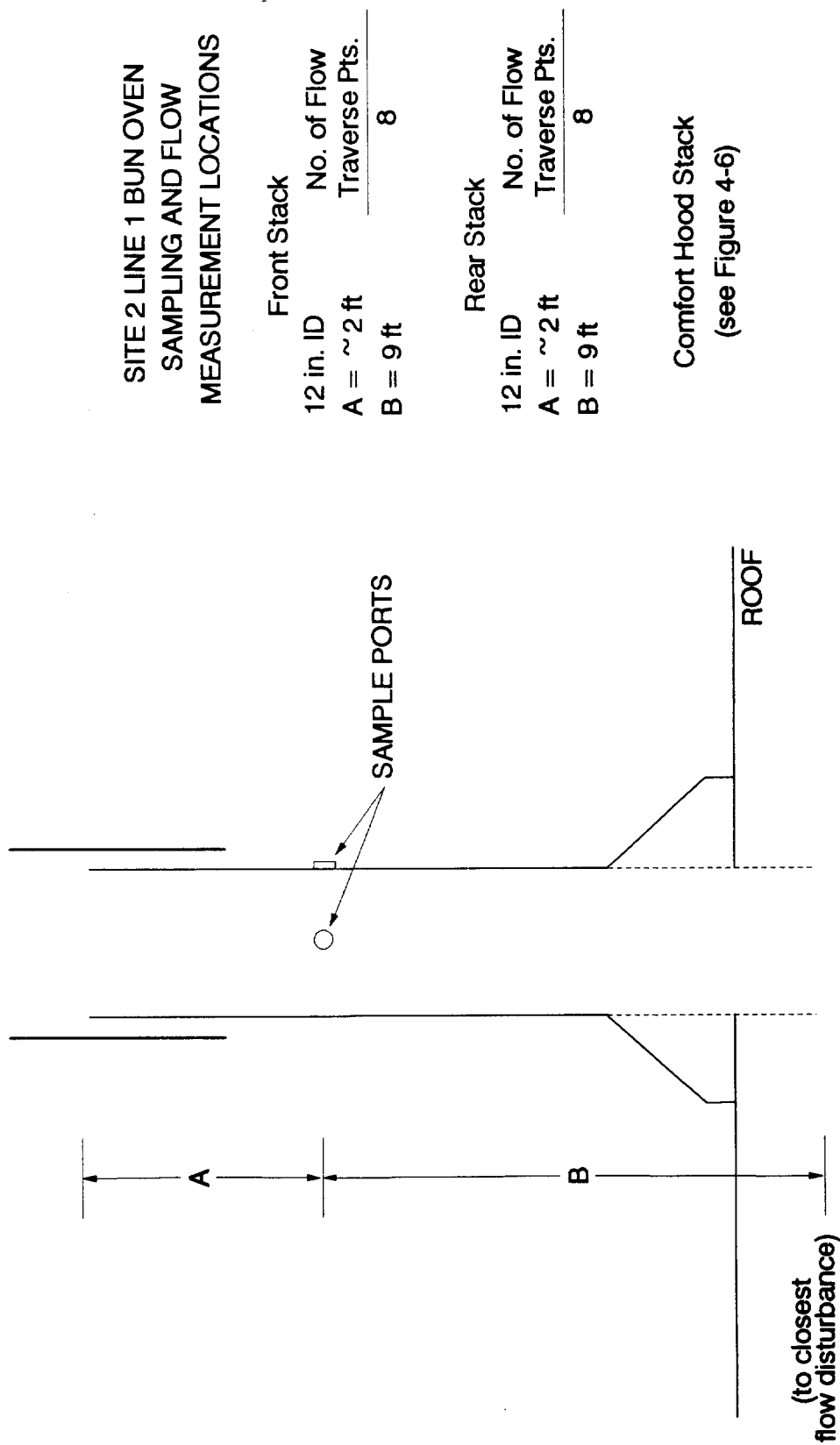
The oven on Line 1 had two stacks and a comfort hood; however, neither stack had a rain cap. The sampling locations are shown in Figure 4-3. The front stack and comfort hood were sampled alternately using a 150-foot length of heat-traced sample line. The location of the rear stack necessitated a 200 foot length. Both the front and rear stacks had a 12-inch ID. Ports were located approximately 9-feet (9 diameters) downstream and 2-feet (2 diameters) upstream of the nearest flow disturbances. Flow was measured at 8 traverse points.

All of the comfort hoods at Site 2 were exhausted by axial fan roof ventilator (Dayton Model 3C276-A). There was no ductwork following the fan; therefore, U.S. EPA Method 1 specifications were not met. Flow measurements had to be taken directly after the fan as it was exhausted to atmosphere. The general configuration is shown in Figure 4-4. Six traverse points were located as shown.

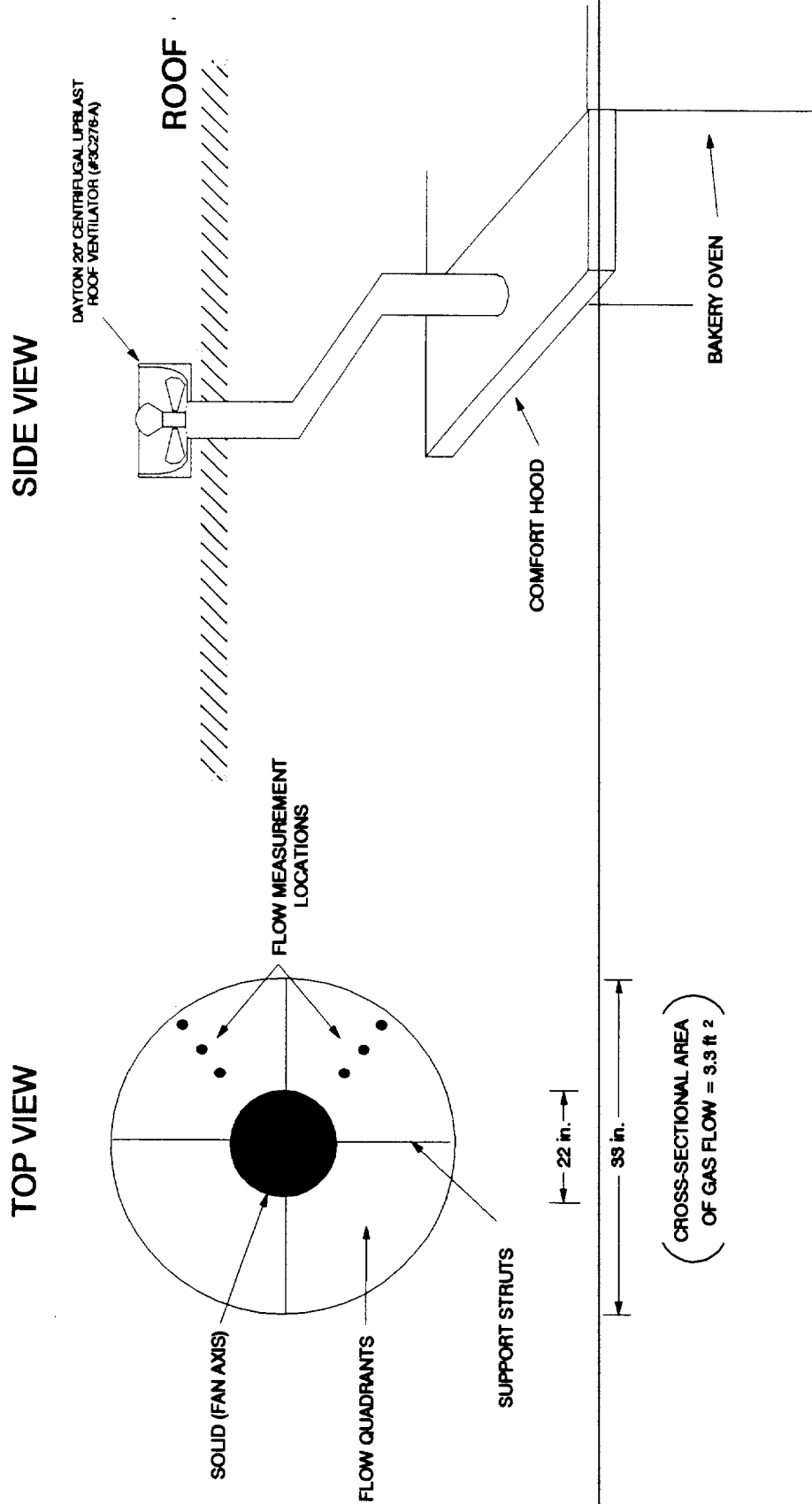
The comfort hood fan on Line 1 was not operating during the test and had evidently not operated for some time. Gas flow was induced by strictly natural drafting of the hot gases at velocities of 50-300 fpm and at temperatures of 150°F.

The Line 2 was an indirect-fired unit and the oven gases were vented from a stack located in the front of the oven and the burner stack was located in the rear. As with the Bun oven, there was a comfort hood that was vented by a axial fan roof ventilator. There was no gas duct work following the fan; therefore, the flow measurement could not be made at a location in accordance with the U.S. EPA Method 1 procedures. Flows were estimated by both velocity pressure measurements and hot-wire anemometer measurements.

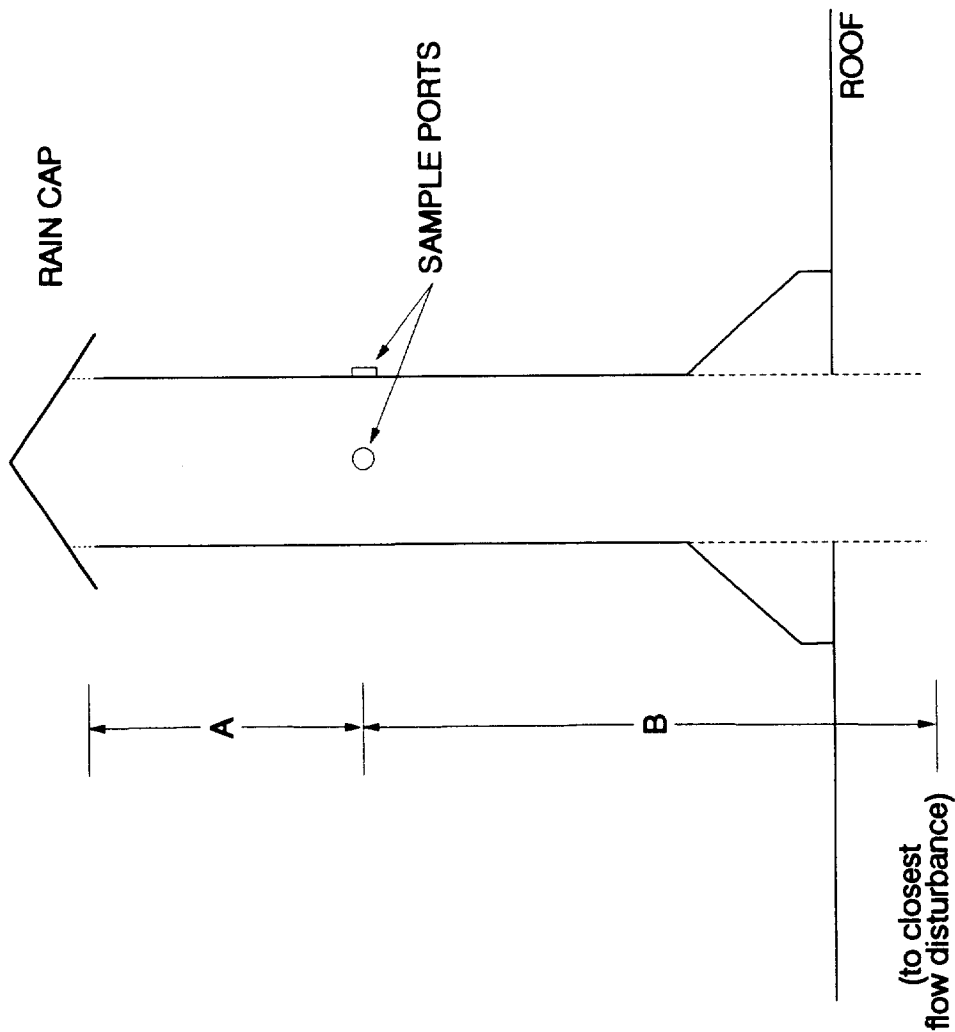
The sampling locations on Line 2 are shown in Figure 4-5. The oven (front) stack was 11.5-inch ID with a rain cap. Ports were located 5.5-feet (5.7 diameters) downstream and 1.0-feet (1.0 diameters) upstream of the nearest flow disturbances. Flow was measured at 16 traverse points.



**FIGURE 4-3. SITE 2 LINE 1 BUN OVEN STACK CONFIGURATION
EPA BAKERIES (1992)**



**FIGURE 4-4. GENERAL SCHEMATIC OF THE SITE 2 COMFORT HOOD EXHAUST FANS
EPA BAKERIES (1992)**



**SITE 2 LINE 2 BREAD OVEN
SAMPLING AND FLOW
MEASUREMENT LOCATIONS**

Front Stack	
11.5 in. ID	No. of Flow
A = ~1 ft	Traverse Pts.
B = ~5.5 ft	16

Rear Stack (Burner)*	
16 in. ID	No. of Flow
A = 2 ft	Traverse Pts.
B = 4 ft	16

* Rear stack did not have rain cap.

Comfort Hood Stack
(see Figure 4-6)

**FIGURE 4-5. SITE 2 LINE 2 BREAD OVEN STACK CONFIGURATION
EPA BAKERIES (1992)**

The burner stack on Line 2 had a 16-inch ID without a rain cap. Ports were located approximately 4-feet (3.0 diameters) downstream and 2-feet (1.5 diameters) upstream of the nearest flow disturbances. Flow was measured at 16 traverse points.

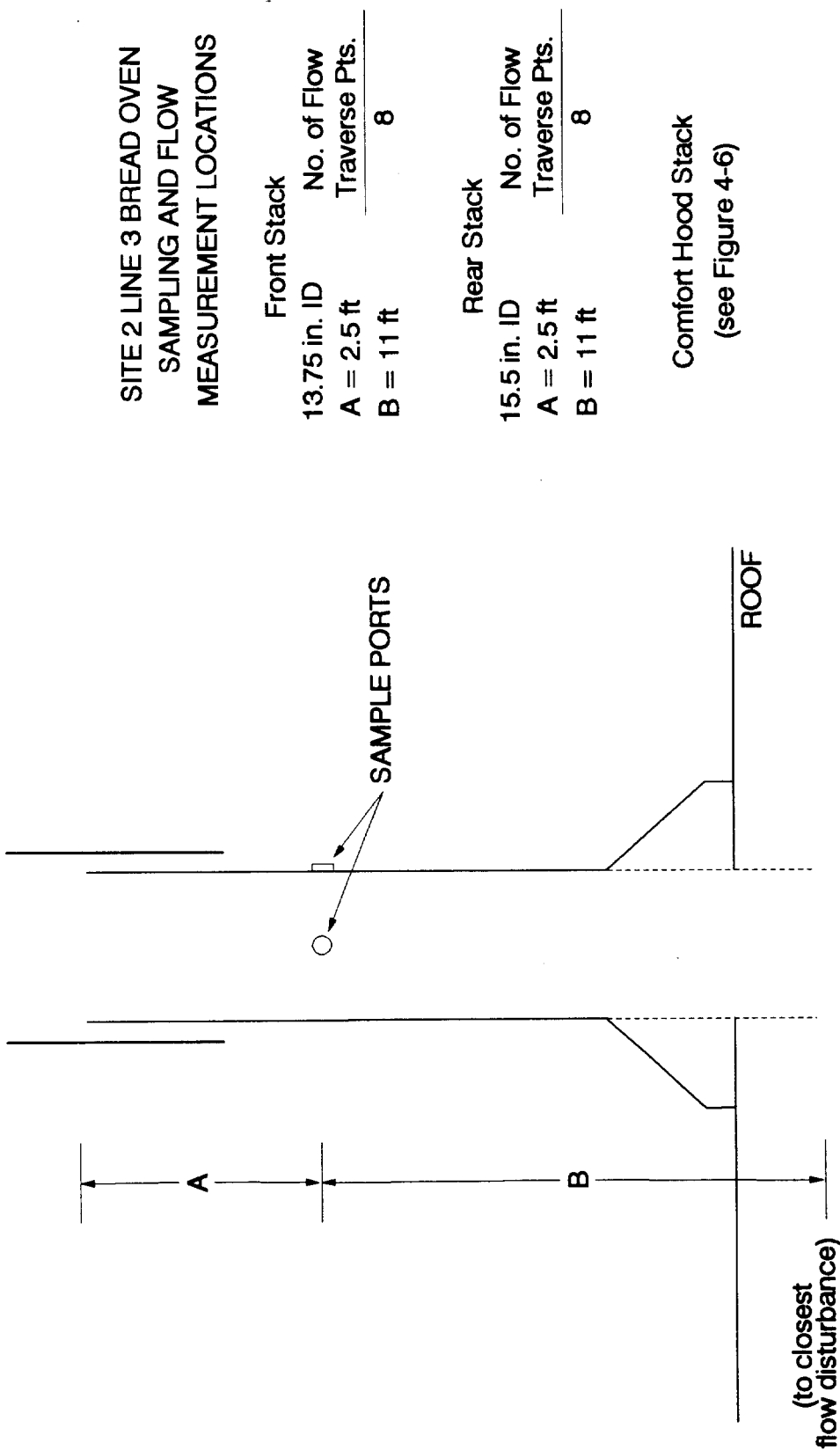
The comfort hood on Line 2 was identical to that described except that the fan was operating. Flows were measured as described above.

The Bread oven on Line 3 was a direct-fired unit with stacks located approximately 90 feet apart. There were 2 oven stacks and a comfort hood. The front stack and comfort hood were alternately sampled using a 100-foot section of heat-traced tubing. The rear stack was sampled using a 150-foot section.

The sampling locations on Line 3 are shown in Figure 4-6. The front stack had a 13.75-inch ID. Rain caps were not present on any of the Line 3 stacks. Ports on the front stack were located 11-feet (9.6 diameters) downstream and 2.5-feet (2.2 diameters) upstream of the nearest flow disturbances. Flow was measured at 8 traverse points.

The rear stack on Line 3 had a 15.5-inch ID. Ports were located approximately 11-feet (8.9 diameters) downstream and 2.5-feet (1.9 diameters) upstream of the nearest flow disturbances. Flow was measured at 8 traverse points.

The comfort hood on Line 3 was identical to that described and the fan was operating. Flows were measured as described above.



**FIGURE 4-6. SITE 2 LINE 3 BREAD OVEN STACK CONFIGURATION
EPA BAKERIES (1992)**

5.0 SAMPLING AND ANALYTICAL METHODS

This section briefly summarizes the procedures used for sampling and analysis. Procedures are presented for Method 25A testing in Section 5.1, Method 18 procedures in Section 5.2, and Methods 1-4 procedures in Section 5.3. The detailed protocols can be found in the U.S. EPA reference methods located in the appendices.

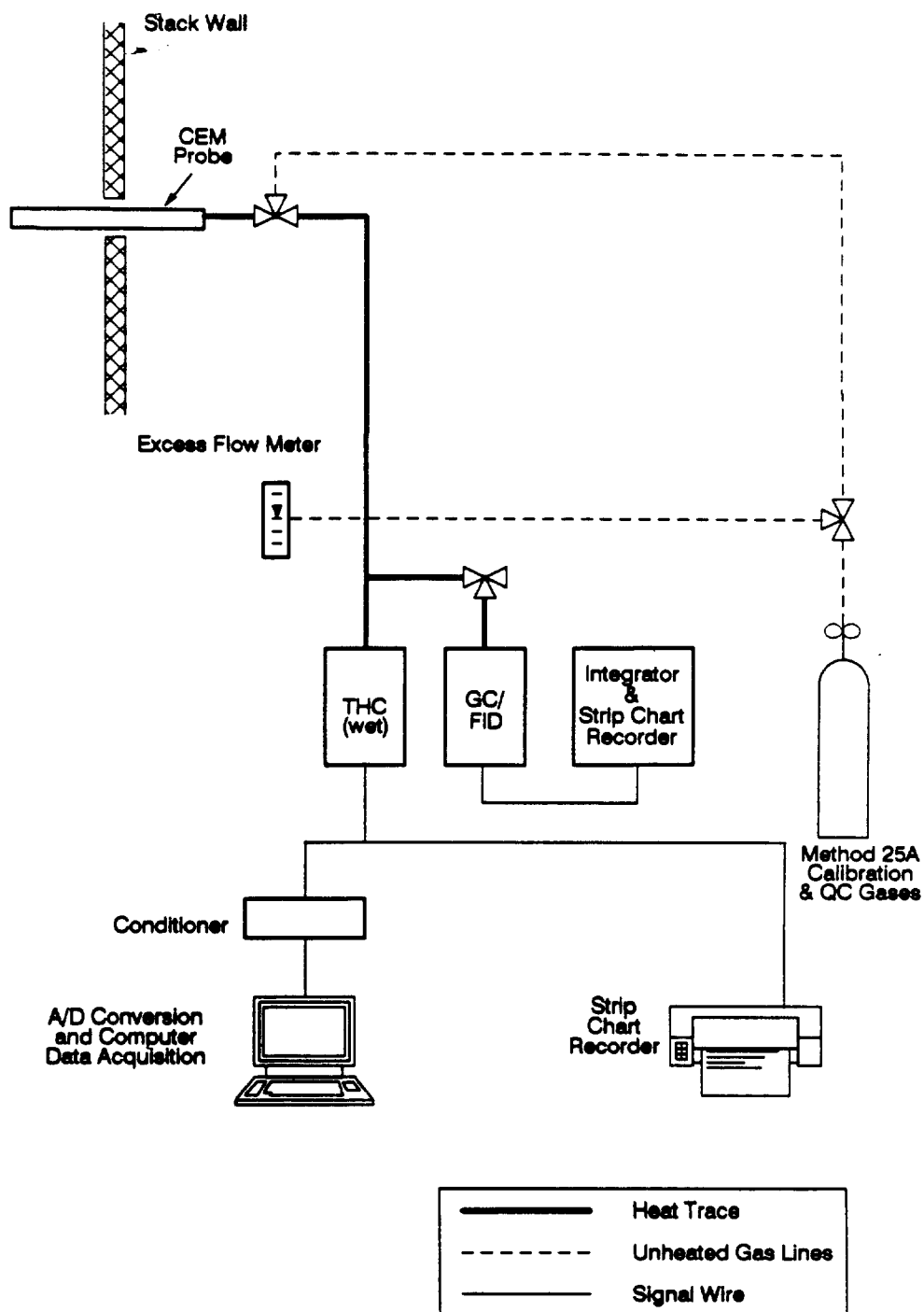
5.1 Method 25A Sampling and Analysis for THC

Total hydrocarbon concentration was determined on a continuous basis using the U.S. EPA Method 25A procedure. Procedures incorporate QA/QC protocols stipulated as "Measurement System Performance Specifications" in the reference methods. The QA parameters will be reported in Section 6.0 while the QC procedures are fully detailed in the test plan written for this test program.

The following discussion presents Sample Extraction Equipment and Procedures in Section 5.1.1, THC Analyzers and Operating Principal in Section 5.1.2, Data Acquisition Procedures in Section 5.1.3, Instrument Calibration in Section 5.1.4, and an Example Daily Operating Procedure in Section 5.1.5.

5.1.1 Sample Extraction Equipment and Procedure

A continuous gas sample was extracted from the stack and transported to the analyzer through a heated Teflon® sample line (heat trace). The gas only came into contact with inert materials such as stainless steel, glass, or teflon. The sample gas temperature was maintained above 100°C (212°F) so that there was no condensation of moisture or hydrocarbons in the tubing. A generalized schematic of a typical extractive system is shown in Figure 5-1.



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Figure 5-1. General Schematic of Method 18/25A Extractive Stack Gas Sampling System

The probe was used to extract gas from the stack was constructed of a short length of stainless steel or teflon tubing. The gas was extracted using a heated head pump that was placed just upstream of the THC analyzer. An excess flow dump was also upstream from the analyzer, so that the gas in the analyzer would not be under any back pressure created by the sample pump.

In addition to one heated sample tube for sample gas extraction, a separate tube was run from the calibration gas cylinders to the probe. This tube was connected to the system with a 3-way valve (calibration valve) at the junction of the probe and the heat trace. This allowed for leak checks, sample bias checks and calibration drift checks to be completed, as was discussed in Section 6. These procedures required a calibration or QC gas be directed to the probe and back through the entire sampling system. The difference between the resulting values and the values observed when the gas was passed directly to the instrument is referred to as sample bias. When the bias was above acceptable limits, corrective actions were implemented.

5.1.2 THC Analyzers and Analytical Principles

The THC analyzers used in Method 25A procedures employ a flame ionization detector (FID) to quantify the quantity of THC. As the flue gas enters the detection chamber, the hydrocarbons are combusted in a hydrogen flame. The ions and electrons formed in the flame enter an electron gap, decrease the gas resistance, and permit a flow in an electric circuit. The resulting current is proportional to the instantaneous concentration of the total hydrocarbons. These analyzers are not selective between species; however, different hydrocarbon species respond differently in the FID. Straight chain hydrocarbons (alkanes), alkenes, and aromatics respond in proportion to the number of carbons atoms in the molecule. For example, 100 ppmv propane (C_3H_8) responds approximately the same as 300 ppm methane (CH_4). When measuring THC of these type of compounds, there are no substantial inaccuracies in reporting THC as ppmv as methane. However, oxygenated compounds such as ethanol (CH_3CH_2OH) and

acetaldehyde (CH_3CHO) have a depressed response so that what appears to be 300 ppmv as methane may actually be 1200 ppmv ethanol. The resulting THC concentrations as ppmC were adjusted to ppmv ethanol or ppmv acetaldehyde based on the results of the Method 18 analysis.

5.1.3 Data Acquisition

The signal from the analyzer is typically an analog voltage response (i.e., 0-5 volts). The meter panel on the front of the instrument usually translates the voltage signal to concentration units (i.e., ppmv). However for long term data acquisition, the voltage signals coming from the electrical output leads need to be translated to actual concentration data. The system used to perform this function is known as the data acquisition system or DAS. This process will either be accomplished with the use of a strip chart recorder (SCR) or a computerized system. A SCR is the simplest procedure; however additional man hours were needed to reduce the SCR trace to individual readings (i.e., 1/minute). If a computerized version is used, the analog signal is converted to a digital signal and directed to a computer so that the signal was translated to concentration units and saved to magnetic media. For this test program, a computerized DAS was used and a SCR was used as a back-up system.

5.1.4 Instrument Calibration

Calibrations were performed by passing known concentrations of a hydrocarbon gas standard through the instrument and recording the associated response. A response factor was then calculated and used to adjust sample gas responses to concentration units. Typical calibration calculations were completed as shown in Section 7. The THC instrument was calibrated twice daily. The first calibration was used to determine the response factor, and the second calibration was performed after completing the test runs so that calibration drift can be determined and the test data corrected for drift (if necessary). Calibrations were completed on a two point basis:

zero gas (generally N₂), and a high-range or "span" gas. Methane was used as the calibration gas, and the concentrations were reported as ppmv methane which are the same as ppmv Carbon (ppmC). The gas was certified by the manufacturer guaranteeing the concentration within $\pm 2\%$ accuracy.

Other QC operations were also performed to verify the accuracy of the data produced. These operations included calibration drift and calibration error determinations. Additional procedures such as linearity check, sample bias, leak checks, and gas stratification were also performed. These are further discussed in Section 6.

5.1.5 Example Daily Operating Procedure

The following is a detailed standard operating procedure for calibrating and operating the CEMS:

1. Turn on computer and printer, put printer on-line, and load the DAS program. Be sure that the THC instrument has been on with the FID flame lit for several hours.
2. Synchronize watch with sample location leaders.
3. Turn on strip chart recorders (SCR) and make appropriate notes on charts and in logbook (write down all procedures and observations in logbook and on SCRs as the day progresses).
4. Open all calibration gas cylinders so that they may be introduced to the instruments.
5. Perform daily pre-test leak check on CEMs as discussed in Section 6. If a zero gas is used for this procedure, zero all instruments at this time. Enter these values in the computer calibration routine. Be sure to check and maintain all flows throughout calibration and operation.
6. Introduce the THC span gas.

7. Make adjustments to the THC instrument as required and enter the value into the computer calibration routine.
8. Introduce QC gases to instruments to determine calibration error. Record at least one minute of data for each. If the QC gas response is not within $\pm 5\%$ of the calibration gas value, the operator will recalibrate the instrument, or perform other corrective actions.
9. Begin sampling routine, with the computer on standby.
10. Start the data acquisition system when signaled by radio that system is in stack.
11. Carefully check all flows and pressures during the operation of the instruments and watch for apparent problems in any of the instruments, such as unusual readings or unreasonable fluctuations.
12. Stop the data acquisition system at the end of the test when signaled.
13. Perform the final calibration (Repeat Steps 5-8) except make no adjustments to the system. This procedure was completed through the calibration valve so that gas is extracted through the entire system.
15. Calculate calibration drift.

All QA/QC procedures are fully explained in Section 6.

5.2 Method 18 for Determining Ethanol and Acetaldehyde Concentrations

The following sections summarize the sampling and analytical protocols for Method 18 testing procedures targeted for ethanol and acetaldehyde.

5.2.1 Sample Collection

A slip stream of sample gas was taken off the main heat trace line and directed to the GC injection loop as shown in Figure 5-2. Discrete GC injections were made to quantify the gas phase concentration of the two target analytes. This was accomplished by first allowing the gas to vent through the injection loop. Then the injection valve was turned so that the sample gas in the loop is directed into the GC/FID. The number of sample injections in a given testing time frame was determined based on how long it takes for the target compounds to elute from the GC column to the detector. This period of time is known as the retention time (RT). If other compounds are contained in the gas which elute at much longer RT than the target species, they may interfere with the later analyses and the column may have to be periodically cleaned. This is done by raising the oven temperature for a period of time. Cleaning the column decreases the number of GC injections that can be performed during the run time.

5.2.2 Sample Analysis

The U.S. EPA Method 18 analysis is performed using a GC/FID to separate hydrocarbon species present in the exhaust gas stream. The FID employed in the GC works in a similar manner to that discussed in Section 5.1.2. By using a column filled with a sorbent, the various hydrocarbons in a given gas stream were separated so that the instantaneous concentrations measured relate to a specific hydrocarbon. Before sampling the source gas, the GC/FID system was calibrated with standard gas mixtures containing the hydrocarbons of interest. The calibration procedure established both calibration curves (response factors) and retention times for the hydrocarbons. The retention times were used to identify similar compounds in the source samples and the calibration curve was used to quantify the concentrations of the hydrocarbons.

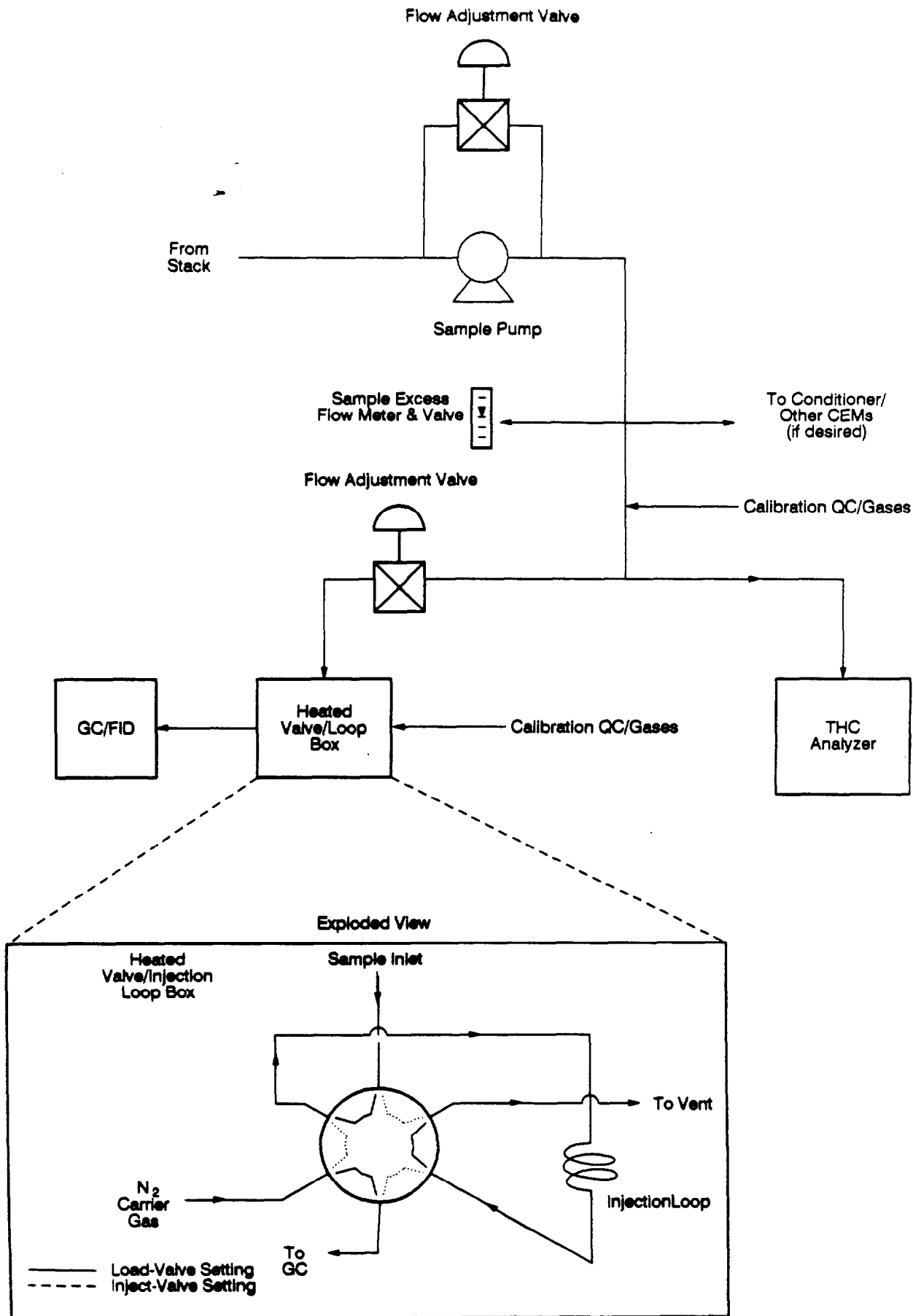


Figure 5-2. General Schematic of Method 18 Sample Injection System

To use Method 18 effectively, standards were prepared to include concentrations over the entire range expected. For ethanol, a suitable collection of standards for bakery emissions concentrations are 0, 200, 800, 2000 and 8000 ppmv ethanol. If stack concentrations are higher than the highest standard, then either higher standards need to be prepared or purchased or the sample needs to be diluted with a gas tight syringe. Levels of acetaldehyde were expected to be less than 100 ppmv, therefore, standards of 0, 20, and 80 ppmv acetaldehyde were used.

The response and retention times of the individual hydrocarbons were recorded on a strip chart recorder. An integrator was used to measure peak areas and compile retention times and area counts. The peaks on the integrator recording were identified from the established retention times for each hydrocarbon of interest and the associated concentrations determined using the calibration curve as a reference.

The column and conditions were as follows:

- Column - 80/120 Carbopack B AW/6.6% Carbowax 20M;
- Carrier Gas - N₂; and
- Temperature - 30°C (isothermal).

5.3 Determination of Volumetric Gas Flow Rates

Determination of gas flow rate incorporates the designation of traverse points by the U.S. EPA Method 1, the measurement of average duct gas velocity by Method 2, the measurement of gas molecular weight by Method 3, and the determination of gas moisture content by Method 4. The following sections discusses those procedures, and the U.S. EPA methods are included in the Appendices.

5.3.1 Method 2 Flow Rate by Pitot Tube

Methods 2 calls for flow determination by measuring the velocity pressure with either an S type pitot or a standard pitot. The following discussion presents the principals of a Method 2 flow determination.

The pitot tube measurements in the ducts were obtained by moving the pitot tube and thermocouple to each of the traverse points designated in Method 1. The velocity pressure and temperature readings at each of those points were recorded. A static duct pressure determined at a single sample point was usually sufficient. This was accomplished by first rotating the pitot tube perpendicular to the flow (as in the cyclonic flow check) until the pressure reading was zero. One leg of the tubing was then disconnected from the manometer and the static pressure was compared against ambient pressure. If the positive tube was left attached to the manometer and the reading was positive, then the overall static was positive. If the negative leg was left attached, and the reading was positive, then the static was negative. The average duct gas velocity and volumetric flow rate was then calculated as shown in Section 7.

5.3.2 Method 3 Molecular Weight Determination

The U.S. EPA Method 3 describes the procedures for obtaining the molecular weight of gas being sampled, which was necessary for the flow calculation. The composite molecular weight of the gas was determined from the relative amounts of individual constituents of the gas stream. In most cases, these principal constituents are oxygen, nitrogen, and carbon dioxide. Some stack gases, however, contain a significant amount of volatile organic or other compounds which can be included in the calculation.

The concentrations of O₂ and CO₂ were determined by a Fyrite analyzer. The molecular weights of such compounds were multiplied by their relative concentrations as shown in Section 7. The products were summed to give the dry

molecular weight of the gas being emitted. The final wet molecular weight calculation required gas moisture content values.

5.3.3 Method 4 Stack Gas Moisture Content

Method 4 is the U.S. EPA method for establishing the moisture content of a stack gas. There are two recognized ways to obtain this moisture content. The first measures the amount of direct condensation of gas moisture in an impinger train. An alternate approximation technique used for stack gases with a temperature lower than 59°C (138°F) employs a wet-bulb/dry-bulb measurement.

Method 4 explains how a sample of the gas is drawn into impingers and condensed using an ice bath. Following the condensation impingers is a desiccant impinger (filled with silica gel) which removes the remaining non-condensed moisture from the gas stream. At the end of the test, the volume of the gas was measured with a dry gas meter and recorded; the impinger weights and silica gel weights were also measured and recorded. These data were used to calculate the percent moisture in the gas stream.

It is important to perform sampling train leak checks at the start and finish of sampling as well as before and after a port change. The method only calls for a post-test leak check but completion of a pre-test leak check indicates that the post-test check was successful as well. To leak check the assembled train, the nozzle end was capped off and a vacuum was pulled in the system of 1 inch Hg higher than the highest measured vacuum. When the system is evacuated, the volume of gas flowing through the system was timed for 60 seconds. The leak rate was required to be less than 4% of the sample rate or 0.02 cfm, whichever was less. After the leak rate was determined, the cap was slowly removed from the nozzle end until the vacuum drops off, and then the pump was turned off.

If the leak rate requirement is not met, the train can be systematically checked by first capping the train at the filter, at the first impinger, etc., until the leak is located and corrected. In the event that a final leak rate is found to be above the minimum acceptable rate upon removal from a port, the run may be rejected.

When the sampling train was ready for operation, the leak rates and sampling stop/start times were recorded on the sampling test log. Other events that occur during sampling, such as pitot cleaning, thermocouple malfunctions, or any other unusual occurrences, were recorded on the test log.

6.0 QUALITY ASSURANCE/QUALITY CONTROL

Specific Quality Assurance/Quality Control (QA/QC) procedures were completed during the test program to ensure the production of useful and valid data throughout the course of the project.

Section 6.1 presents a summary of the QA program and parameters attained. The definitions of the terminology used in conjunction with QA/QC information is presented in Section 6.2. Section 6.3 presents the QA parameters for Method 25A tests. Section 6.4 presents the QA parameters for the Method 18 analyses. Section 6.5 presents a discussion of the carbon equivalent correction factors as well as a comparison of the two methods.

6.1 QA Summary

The majority of reference method QA acceptance criteria were met during this test program. There were 10 days of testing using two THC monitoring systems (20 system days). Method 25A daily calibration drift did not exceed the criterion of $\pm 3\%$ on nineteen of the twenty system days. The Site 1, Day 1 Method 25A test data exhibited calibration drift of 3.2% and the drift was corrected by assuming linear drift between the initial and final calibration. Method 25A calibration error was determined extensively over the course of the test program. Over 150 calibration error checks were performed during the test program and the majority these checks met the Method 25A criterion of $\pm 5\%$ of the gas concentration. Method 25A sample bias checks, as well as O₂ leak checks, were also completed. The majority of these QA parameters met the acceptance limits.

Extensive Method 18 QA/QC procedures were also followed. Initial and final calibrations were performed. Calibrations for ethanol and acetaldehyde were all completed using from 3 to 5 calibration points. Multi-point calibrations were also

performed on methane for low concentrations on all of the test days (< 900 ppmC). On five of the test days, a single point calibration was used on higher methane values. This was due to the detector "overranging". After checking the methane values determined from a single point calibration against a multi-point calibration curve, no substantial difference was found.

Sample bias checks were also extensively conducted on the Method 18 sampling system. The majority of checks verified acceptable non-biased sampling. However, some bias checks revealed sample bias caused by the loss of heat in the heated tubing adjacent to the GC. These data points were invalid and testing was not continued until the problem was remedied and a successful bias check had been completed.

6.2 Definitions

The overall QA/QC objective was to ensure precision, accuracy, completeness, comparability, and representativeness for each major measurement parameter called for in this test program. The terms used to define the QA/QC objectives are designed as follows:

- Data Quality: The characteristics of a product (measurement data) that bear on its ability to satisfy a given purpose. These characteristics are defined as follows:
 - Precision - A measure of mutual agreement among individual measurements of the same property, usually under prescribed similar conditions. Precision can be expressed in terms of the standard deviation (or the relative standard deviation).
 - Accuracy - The degree of agreement of a measurement (or an average of measurements of the same thing), X, with an accepted reference or true value, T, usually expressed as the difference between two values, X-T, or the difference as a percentage of the reference or true value, $100 (X-T)/T$, and

sometimes expressed as a ratio, X/T . Accuracy is a measure of the bias in a system.

- Completeness - A measure of the amount of valid data obtained from a measurement system compared with the amount that was expected to be obtained under prescribed test conditions.
- Comparability - A measure of the confidence with which one data set can be compared with another.
- Representativeness - The degree to which data accurately and precisely represent a characteristic of a population, variations of a parameter at a sampling point, or an environmental condition.
- Quality Control: The overall system of activities whose purpose is to provide a quality product or service: for example, the routine application of procedures for obtaining prescribed standards of performance in the monitoring and measurement process.
- Quality Assurance: A system of activities whose purpose is to provide assurance that the overall quality control is being done effectively. The completion of QA procedures generates indicating parameters that are a measurement of the general quality of the data.

6.3 Method 25A Sampling and Analytical QA Parameters

6.3.1 Calibration Drift

The Method 25A Calibration drift values are given in Table 6-1.

6.3.2 Calibration Error

The calibration error checks are presented in Table 6-2. Table 6-3 presents on-site response THC response to ethanol QC challenges.

Table 6-1

Method 25A Calibration Drift EPA Bakeries (1992)

Site	Day	System 1 Drift (% of Range)		System 2 Drift (% of range)	
		Zero Drift	Span Drift	Zero Drift	Span Drift
1	1	0.04	3.22	0.03	-0.69
1	2	-0.01	-0.01	0.16	0.39
2	1	0.09	-0.13	0.04	-0.2
2	2	ND	-1.34	ND	-2.57
3	1	0.07	0.02	-0.14	-0.61
3	2	ND	-0.06	ND	-0.2
4	1	0.17	-0.08	-0.01	0.16
4	2	0.08	0.04	0.04	-0.47
4	3	0.03	-0.13	0.04	0.14
4	4	-0.09	-0.05	-0.01	-0.24

Note: Full range of analyzer was 0-10,000 ppmC. All calibrations performed with methane.

ND = Not determined

Table 6-2. Method 25A Calibration Error Results.
EPA Bakeries, Site 1 (1992)

Methane QC Gas Conc. (ppmC)	System 1			System 2	
	THC Instrument Response (ppmC)	Calibration Error (%)		THC Instrument Response (ppmC)	Calibration Error (%)
SITE 1 - DAY 1					
2000	2039	2.0		2124	6.2
803	805	0.2		GC DOWN	NA
80.2	81.9	2.1		GC DOWN	NA
199.1	198.4	-0.4		GC DOWN	NA
0	4.3	NA		20.3	NA
0	2.7	NA		12.9	NA
2000	1982	-0.9		1963	-1.9
199.1	199.5	0.2		209.3	5.1
2000	1981	-1.0		2089	4.5
803	804.2	0.1		853.5	6.3
199.1	204.3	2.6		224	12.5
SITE 1 - DAY 2					
2000	2014	0.7		1980	-1.0
803	801	-0.2		807	0.5
199.1	197	-1.1		210	5.5
80.2	77.3	-3.6		89.6	11.7
2000	2003	0.2		1937	-3.2
0	3.7	NA		14	NA
2000	1990	-0.5		1986	-0.7
803	805	0.2		803	0.0
199.1	202	1.5		206	3.5

Table 6-2. Method 25A Calibration Error Results, (cont).
EPA Bakeries, Site 2 (1992)

Methane QC Gas Conc. (ppmC)	System 1		System 2	
	THC Instrument Response (ppmC)	Calibration Error (%)	THC Instrument Response (ppmC)	Calibration Error (%)
SITE 2 - DAY 1				
1490	1512.6	1.5	1514.2	1.6
798	812.9	1.9	814.2	2.0
199.1	213.6	7.3	217.6	9.3
3980	3979.6	-0.0	4013.4	0.8
199.1	215.9	8.4	204.9	2.9
798	807.6	1.2	748.6	-6.2
1490	1496.5	0.4	1436.1	-3.6
3980	3931.3	-1.2	3752.8	-5.7
1490	1493.1	0.2	1515.3	1.7
80.2	90.9	13.3	92.5	15.3
80.2	89.7	11.8	87.5	9.1
80.2	89	11.0	88.5	10.3
0	11.1	NA	1.5	NA
80.2	90	12.2	86.8	8.2
798	809.7	1.5	772.4	-3.2
199.1	212	6.5	217.9	9.4
1490	1505.1	1.0	1524.3	2.3
3980	3966.9	-0.3	3953.9	-0.7
0	9.2	NA	4.1	NA
SITE 2 - DAY 2				
199.1	209.3	5.1	206.3	3.6
798	782.6	-1.9	801.2	0.4
1490	1467.5	-1.5	1488.9	-0.1
2000	2041.4	2.1	1936.4	-3.2
2000	2099.5	5.0	1937.6	-3.1
3980	3924	-1.4	3836.6	-3.6
80.2	97.7	21.8	86.8	8.2
199.1	159.4	-19.9	102	-48.8
798	810.2	1.9	754.8	-5.4
1490	1481.1	-0.6	1428.9	-4.1
2000	2008	0.4	2031	1.6
3980	3846	-3.4	3723	-6.5

Table 6-2. Method 25A Calibration Error Results, (cont).
EPA Bakeries, Site 3 (1992)

Methane QC Gas Conc. (ppmC)	System 1		System 2	
	THC Instrument Response (ppmC)	Calibration Error (%)	THC Instrument Response (ppmC)	Calibration Error (%)
SITE 3 - DAY 1				
798	817	2.4	769.7	-3.5
1490	1490	0.0	1390	-6.7
0	1.9	NA	3.4	NA
1490	1490.3	0.0	1419	-4.8
1490	1491.5	0.1	1429.2	-4.1
2000	2030.7	1.5	2071.6	3.6
0	7.1	NA	-14.1	NA
SITE 3 - DAY 2				
0	1.16	NA	-1.5	NA
80.2	77.7	-3.1	68.1	-15.1
199.1	198	-0.6	183	-8.1
80.2	75.3	-6.1	82.5	2.9
199.1	198.4	-0.4	188.4	-5.4
2000	2023	1.2	1909	-4.6
2030	2011	-0.9	1944	-4.2
798	801.5	0.4	783.2	-1.9
3960	3948	-0.3	3849	-2.8
80.2	77.2	-3.7	81.5	1.6
199.1	197.5	-0.8	189.7	-4.7
798	798	0.0	789.4	-1.1
2000	2016	0.8	1874	-6.3
3960	3945	-0.4	3847.2	-2.8
0	-1.97	NA	23.8	NA
1490	1484.5	-0.4	1518.8	1.9

Table 6-2. Method 25A Calibration Error Results, (cont).
EPA Bakeries, Site 3 (1992)

Methane QC Gas Conc. (ppmC)	System 1		System 2	
	THC Instrument Response (ppmC)	Calibration Error (%)	THC Instrument Response (ppmC)	Calibration Error (%)
SITE 4 - DAY 1				
3960	3964	0.1	3966	0.2
80.2	72.9	-9.1	64.4	-19.7
199.1	180.7	-9.2	179.9	-9.6
80.2	60.1	-25.1	60	-25.2
0	-21.8	NA	-6.6	NA
798	810.2	1.5	801.9	0.5
1490	1507.4	1.2	1504.8	1.0
2000	2036	1.8	1939	-3.1
SITE 4 - DAY 2				
3960	3954	-0.2	3960.4	0.0
1490	1506.7	1.1	1506.1	1.1
0	2.1	NA	5.1	NA
80.2	84.5	5.4	75.2	-6.2
199.1	207	4.0	192.6	-3.3
798	804.9	0.9	804.8	0.9
1490	1499	0.6	1509	1.3
2000	2030.2	1.5	1943.2	-2.8
3960	3938	-0.6	3981	0.5
0	8.3	NA	4.05	NA
3960	3964	0.1	3912	-1.2
200	201.6	0.8	192.2	-3.9
200	205.1	2.5	194.3	-2.8
80.2	83.8	4.5	82.9	3.4

Table 6-2. Method 25A Calibration Error Results, (cont).
EPA Bakeries, Site 3 (1992)

Methane QC Gas Conc. (ppmC)	System 1		System 2	
	THC Instrument Response (ppmC)	Calibration Error (%)	THC Instrument Response (ppmC)	Calibration Error (%)
SITE 4 - DAY 3				
3960	3963	0.1	3958	-0.1
3960	3949	-0.3	3873	-2.2
0	-0.7	NA	-0.3	NA
3960	3954	-0.2	3941	-0.5
0	14.5	NA	-0.2	NA
3960	3936.5	-0.6	3930.6	-0.7
0	-0.96	NA	-2.7	NA
3960	3967.2	0.2	3988.9	0.7
199.1	202	1.5	189.3	-4.9
0	2.7	NA	3.8	NA
3960	3947	-0.3	3974	0.4
3960	3964	0.1	3969	0.2
3960	3948	-0.3	3990	0.8
798	796.5	-0.2	808.9	1.4
1490	1486.6	-0.2	1516.6	1.8
2030	2017.3	-0.6	2019.1	-0.5
SITE 4 - DAY 4				
199.1	202	1.5	187.7	-5.7
798	803	0.6	799.7	0.2
2030	2034.8	0.2	2032.8	0.1
80.2	84.4	5.2	67.6	-15.7
0	0.6	NA	-10.8	NA
0	-3.9	NA	-4.6	NA
199.1	200.2	0.6	187.4	-5.9
200	206.8	3.4	191.7	-4.2
2030	2034.6	0.2	2047.5	0.9
0	5.3	NA	-0.8	NA
199.1	199.6	0.3	193.7	-2.7
80.2	766	855.1	76.3	-4.9
0	-2.4	NA	-0.9	NA
80.2	77.8	-3.0	75.5	-5.9
199.1	196	-1.6	183.8	-7.7
798	793.2	-0.6	774.6	-2.9
80.2	83.5	4.1	75.1	-6.4
199.1	202.6	1.8	187.1	-6.0
798	796	-0.3	794.9	-0.4

**Table 6-3. On-Site Ethanol QC Challenges to the Method 25A THC Monitor
EPA Bakeries (1992)**

Site	Test Day	Ethanol QC Gas Conc. (ppmC)	System 1		System 2	
			THC Instrument Response (ppmC)	Carbon Equivalent Correction Factor	THC Instrument Response (ppmC)	Carbon Equivalent Correction Factor
1	1	200	267.5	1.34	238.4	1.19
1	1	200	275.5	1.38	280.5	1.40
1	2	10000	11862	1.19	13569	1.36
1	2	2000	2852	1.43	2948	1.47
1	2	2000	2421	1.21	2731	1.37
1	2	200	272	1.36	274	1.37
			AVG	1.32	AVG	1.36
2	1	200	305.9	1.53	295.5	1.48
2	1	200	310.6	1.55	259.9	1.30
			AVG	1.54	AVG	1.39
3	1	200	320	1.60	283	1.42
3	1	200	302.4	1.51	277	1.39
3	1	498	763.2	1.53	720	1.45
3	1	498	759.6	1.53	694.9	1.40
3	1	498	756.6	1.52	756.6	1.52
3	2	200	307	1.54	286.2	1.43
3	2	200	300.1	1.50	316	1.58
3	2	498	755.5	1.52	765.7	1.54
			AVG	1.53	AVG	1.46
4	1	200	313.5	1.57	299.1	1.50
4	3	200	309.1	1.55	307.6	1.54
4	3	200	313.4	1.57	306.3	1.53
4	3	200	300	1.50	302	1.51
4	4	200	304.6	1.52	307.9	1.54
4	4	200	312.8	1.56	304.1	1.52
4	4	200	297.8	1.49	298.9	1.49
4	4	200	296.8	1.48	304.4	1.52
4	4	200	308.4	1.54	297.2	1.49
4	4	200	DOWN		300.2	1.50
			AVG	1.53	AVG	1.51

6.4 Method 18 QA Parameters

All calibration data from the Method 18 analyses is included in the Appendices. Both an initial and final calibration were performed on each day. Excessive drift was not found during any of the test days.

6.4.1 Sample Bias

Table 6-4 presents the Method 18 sample bias checks for Sites 2-4. The Site 1 bias check results are included in the appendices.

**Table 6-4. Method 18 Sample Bias Checks
EPA Bakeries (1992)**

INJ. NO	Site/Day	Oven Location	Stack/ System Location	GAS CONC.(ppm)	GC ANALYTICAL RESULT	(%) DIFF	COMMENTS
190	4/1		Rack	80.2 METHANE	97.4	21	
191	4/1		Table	80.2 METHANE	84.7	5.6	
192	4/1		Rack	199.1 METHANE	200.5	0.7	
193	4/1		Table	199.1 METHANE	201.2	1	
194	4/1		Rack	80.2 METHANE	80	-0.2	
195	4/1		Rack	80.2 METHANE	78.1	-2.6	
196	4/1		Rack	80.2 METHANE	76.1	-5.1	
208	4/1		Rack	798 METHANE	804	0.8	SINGLE PT RUN 284 (6/30/92)
209	4/1		Table	798 METHANE	810	1.5	SINGLE PT RUN 284 (6/30/92)
210	4/1		Rack	1490 METHANE	1502	0.8	SINGLE PT RUN 286 (6/30/92)
211	4/1		Table	1490 METHANE	1514	1.6	SINGLE PT RUN 286 (6/30/92)
212	4/1		Rack	2000 METHANE	2040	2	SINGLE PT RUN 287 6/30/92)
213	4/1		Table	2000 METHANE	2003	0.1	SINGLE PT RUN 287 6/30/92)
233	4/1		Rack	199.1 METHANE	196.3	-1.4	SINGLE PT RUN 288
234	4/1		Table	199.1 METHANE	194	-2.6	SINGLE PT RUN 288
235	4/1		Table	200 ETHANOL	207	3.5	
255	4/2		Rack	3980 METHANE	3898	-1.6	
256	4/2		Table	3980 METHANE	4026	1.2	
257	4/2		Rack	1490 METHANE	1499	0.6	
258	4/2		Table	1490 METHANE	1540	3.4	
269	4/2		Table	80.2 METHANE	64.9	-19	
270	4/2		Rack	199.1 METHANE	194.8	-2.2	
271	4/2		Table	199.1 METHANE	197.3	-0.9	
272	4/2		Table	798 METHANE	788	-1.2	
273	4/2		Rack	798 METHANE	797	-0.1	SINGLE PT RUN #284
274	4/2		Table	1490 METHANE	1515	1.7	SINGLE PT RUN #284
275	4/2		Rack	1490 METHANE	1534	3	SINGLE PT RUN #286
276	4/2		Table	2000 METHANE	2037	1.9	SINGLE PT RUN #286
277	4/2		Rack	2000 METHANE	2014	0.7	SINGLE PT RUN # 287
298	4/2		Table	200 ETHANOL	212	6	SINGLE PT RUN # 287

RUN ANOTHER CHECK AT SEVERAL LEVELS

Table 6-4. Method 18 Sample Bias Checks (Cont)
EPA Bakeries (1992)

INT. NO	Site/Day	Oven Location	Stack/ System Location	GAS CONC. (ppm)	GC ANALYTICAL RESULT	(%) DIFF	COMMENTS
27	2/1		Front	1490 METHANE	14.89	0.1	S.P., COMPARISON TO SYRINGE INJECTION RUN 28 SMALL BACKGROUND < 1.5ppm USED USED FINAL METHANE CAL. PROBLEM/CHECK REPLACE PROBLEM/CHECK, RERUN/REPLACE BETTER/CHECK/REPLACE BETTER/CHECK/REPLACE REPLACEMENT O.K. SINGLE PT. RUN #26
41	2/1			N2	485.121	NA	
45	2/1	Bun	Rear	80.2 METHANE	77	-3.9	
46	2/1	Bun	Rear	80.2 METHANE	78.8	-1.6	
47	2/1	Bun	Front ^a	80.2 METHANE	43.2	-46	
48	2/1	Bun	Front ^a	80.2 METHANE	56.3	-30	
49	2/1	Bun	Front ^a	80.2 METHANE	77	-3.9	
50	2/1	Bun	Front ^a	80.2 METHANE	78.8	-1.7	
51	2/1		b		78.7	-1.9	
52	2/1		b		78.8	-1.7	
68	2/1		Rear	80.2 METHANE	70.6	-12	
70	2/1		Front	798 METHANE	771	-3.4	
71	2/1		Rear	199.1 METHANE	189	-5	
72	2/1		Front	199.1 METHANE	188	-5.5	
73	2/1		Front	200 ETHANOL	204	2	SINGLE PT, CAL. USING RUN 152 SINGLE PT, CAL. USING RUN 151 SINGLE PT, RUN 152 SINGLE PT SINGLE PT, RUN 151
74	2/1		Rear	200 ETHANOL	209	4.5	
122	2/2		Front	80.2 METHANE	77.8	-2.9	
123	2/2		Front	80.2 METHANE	78.9	-1.6	
116	2/2		Front	2000 METHANE	1896	-5.2	
130	2/2		Front	798 METHANE	777	-2.6	
135	2/2		Front	2000 METHANE	2099	-5	
136	2/2		Rear	2000 METHANE	2012	-0.6	
137	2/2		Front	3980 METHANE	3975	-0.1	
131	2/2		Rear	798 METHANE	779	-2.4	

^a Nittia Moore Heat Trace check.

New 1/4 inch H.T. jumper to replace Nittia Moore.

Table 6-4. Method 18 Sample Bias Checks (Cont)
EPA Bakeries (1992)

INJ. NO	Site/Day	Oven Location	Stack/ System Location	GAS CONC. (ppm)	GC ANALYTICAL RESULT	(%) DIFF	COMMENTS
20	3/1	Bun	Burner	798 METHANE	799	0.1	SINGLE PT, RUN #19
21	3/1	Bun	Oven	798 METHANE	776	-2.8	SINGLE PT, RUN #19
26	3/1		Burner	200 ETHANOL	203	1.5	INITIAL CAL.
42	3/1		Oven	1490 METHANE	1512	1.5	SINGLE PT, RUN #45
43	3/1		Burner	1490 METHANE	1508	1.2	SINGLE PT, RUN #45
65	3/1		Burner	498 ETHANOL	482	-3.2	
66	3/1		Oven	498 ETHANOL	486	-2.4	
67	3/1			80.2 METHANE	88.6	10.5	
68	3/1			80.2 METHANE	86.7	8.1	
69	3/1			199.1 METHANE	214	7.5	
70	3/1			199.1 METHANE	213	7	
104	3/2		Burner	80.2 METHANE	73.1	-8.9	
105	3/2		Oven	80.2 METHANE	82.6	3	
106	3/2		Burner	199.1 METHANE	168	-15.6	RERUN
107	3/2		Burner	199.1 METHANE	196	-1.5	O.K.
108	3/2		Oven	199.1 METHANE	205	3	
124	3/2		Burner	80.2 METHANE	80.6	0.5	
125	3/2		Oven	199.1 METHANE	198	-0.5	
126	3/2		Burner	199.1 METHANE	199	0	
147	3/2		Burner	80.2 METHANE	89.9	12.1	PEAK WIDTH SUSPECT
148	3/2		Oven	80.2 METHANE	76.3	-4.9	
149	3/2		Burner	199.1 METHANE	201	1	
150	3/2		Oven	199.1 METHANE	201	1	
151	3/2		Burner	798 METHANE	800	0.2	SINGLE PT RUN #158
153	3/2		Burner	798 METHANE	705	-11.6	RUN MIOMER LEVELS
154	3/2		Burner	2000 METHANE	2027	1.3	SINGLE PT RUN #159
155	3/2		Oven	2000 METHANE	2027	1.3	SINGLE PT RUN #159
156	3/2		Burner	3960 METHANE	3978	0.4	SINGLE PT RUN #160
157	3/2		Oven	3960 METHANE	3973	0.3	SINGLE PT RUN #160
161	3/2		Burner	200 ETHANOL	204	2	
162	3/2		Oven	498 ETHANOL	511	2.6	RERUN
163	3/2		Burner	82.5 ACETALDEHYDE	81.6	-1.1	
164	3/2		Oven	82.5 ACETALDEHYDE	79.3	-3.9	

**Table 6-4. Method 18 Sample Bias Checks (Cont)
EPA Bakeries (1992)**

INJ. Site/Day NO	Oven Location	Stack/ System Location	GAS CONC.(ppm)	GC ANALYTICAL RESULT	(%) DIFF	COMMENTS
391	4/4	Table	200 ETHANOL	152	-24	
398	4/4	Table	200 ETHANOL	175	-13	
419	4/4	Table	200 ETHANOL	181	-9.5	
421	4/4	Rack	80.2 METHANOL	82.7	3.1	
422	4/4	Table	80.2 METHANE	82.3	2.6	
423	4/4	Rack	199.1 METHANE	199.3	0.1	

7.0

DATA REDUCTION PROCEDURES

The following section details the calculations used for the U.S. EPA Bakeries test program.

7.1

Emission Calculations

The objective of the U.S. EPA Bakeries test program was to determine emissions of Total VOC as well as emissions of two of the primary VOC constituents, namely ethanol and acetaldehyde. The emission calculations were done using several methods. All rates are in units of lbs/hr.

7.1.1

VOC Emissions

Emission rates of VOC as ethanol were calculated by multiplying the average VOC as ethanol concentration by the stack gas flow rate as follows:

$$\text{VOC}_{\text{ETOH}}^{\circ} = [\overline{\text{VOC}_{\text{ETOH}}}] \times Q_a \times \left(\frac{P_s}{T_s \times R \times 10^6} \right)$$

Where:

Q_a = Volumetric flow of stack gas (acf/hr)

P_s = Absolute stack Pressure (in Hg)

T_s = Stack Gas Temperature (°R)

R = Universal Gas Constant (21.85 in Hg-cf/lb-mole-°R)

7.1.2 Ethanol and Acetaldehyde Emissions

Ethanol and acetaldehyde emissions were calculated by multiplying the average concentration by the stack gas flow rates. Average concentrations were determined as shown in Section 7.2.2 through 7.2.5. Emission rates were calculated as follows:

$$\overset{o}{\text{ETOH}} = [\overline{\text{ETOH}}] \times Q_s \times \left(\frac{P_s}{T_s \times R \times 10^6} \right)$$

$$\overset{o}{\text{AA}} = [\overline{\text{AA}}] \times Q_s \times \left(\frac{P_s}{T_s \times R \times 10^6} \right)$$

7.2 Average VOC Concentration Calculations

The calculations used for determining concentrations are given in the following section.

7.2.1 Average VOC as Ethanol Concentration

The average VOC as ethanol concentration (ppmV as ethanol) was calculated as follows:

$$[\overline{\text{VOC}}]_{\text{ETOH}} = \frac{[\overline{\text{NMHC}}]}{1.42}$$

where:

1.42 = Ethanol Carbon Equivalent Correction Factor
(i.e., 10 ppmv ethanol = 14 ppmC THC)

The average non-methane hydrocarbon concentration (ppmC/wet) was calculated as follows:

$$[\overline{\text{NMHC}}] = \left(1 - \left[\frac{\overline{\text{CH}_4}}{\overline{\text{THC}}} \right] \right) \times [\overline{\text{THC}}]$$

The average CH_4 to THC ratios (dimensionless) were calculated as follows:

$$\left[\frac{\overline{\text{CH}_4}}{\overline{\text{THC}}} \right] = \frac{\sum_{i=1}^N \left(\frac{[\text{CH}_4]_i}{[\text{THC}]_i} \right)}{N}$$

where:

N = Number of GC injections during test period

$[\text{CH}_4]_i$ = CH_4 concentration at the time of the GC injection
(ppmC/wet)

$[\text{THC}]_i$ = THC concentration at the time of the GC injection
(ppmC/wet)

The average THC concentration (ppmC/wet) was calculated as follows:

$$[\overline{\text{THC}}] = \frac{\sum_{i=1}^n [\text{THC}]_i}{n}$$

where:

n = Number of THC readings during the test period

7.2.2 Average Ethanol Concentration

The average ethanol concentration (ppmV/wet) using both the Method 18 ethanol and Method 25A THC results was calculated as follows:

$$[\overline{\text{ETOH}}]_{\text{THC}} = \left[\frac{\overline{\text{ETOH}}}{\overline{\text{THC}}} \right] \times [\overline{\text{THC}}]$$

The average ethanol-to-THC ratios (ppmV/ppmC) were calculated as follows:

$$\left[\frac{\overline{\text{ETOH}}}{\overline{\text{THC}}} \right] = \frac{\sum_{i=1}^N \left(\frac{[\text{ETOH}]_i}{[\text{THC}]_i} \right)}{N}$$

where:

$[\text{ETOH}]_i$ = Ethanol Concentration from GC analysis (ppmv/wet)

N = Number of GC injections

7.2.3 Average Ethanol Concentration By GC Only

The average ethanol concentrations (ppmV/wet) determined from the Method 18 analyses were calculated as follows:

$$[\overline{\text{ETOH}}]_{\text{GC}} = \frac{\sum_{i=1}^N [\text{ETOH}]_i}{N}$$

7.2.4 Acetaldehyde Concentration By GC and THC

The average acetaldehyde concentration (ppmV/wet) determined using both the Method 18 acetaldehyde and Method 25A THC results was calculated as follows:

$$[\overline{\text{AA}}]_{\text{THC}} = \left[\frac{\overline{\text{AA}}}{\overline{\text{THC}}} \right] \times [\overline{\text{THC}}]$$

The average acetaldehyde to THC ratios (ppmV/ppmC) were calculated as follows:

$$\left[\frac{\overline{\text{AA}}}{\overline{\text{THC}}} \right] = \frac{\sum_{i=1}^N \left(\frac{[\text{AA}]_i}{[\text{THC}]_i} \right)}{N}$$

7.2.5 Average Acetaldehyde Concentration By GC Only

The average acetaldehyde concentration (ppmV/wet) determined from the Method 18 analyses was calculated as follows:

$$[\overline{AA}]_{GC} = \frac{\sum_{i=1}^N [AA]_i}{N}$$

7.2.6 Comparison Of GC And THC Results

The comparison of the corrected sum of ethanol, acetaldehyde, and methane Method 18 concentrations to the THC concentration was determined as follows:

$$\left(\frac{\overline{GC}}{\overline{THC}} \right) = \frac{\sum_{i=1}^N \frac{GC_i}{THC_i}}{N} \times 100$$

where:

THC_i = THC concentrations determined from the Method 25A monitor at the same time as the GC injection (ppmC).

$$GC_i = \left(\frac{[ETOH]_i}{1.42} + \frac{[AA]_i}{1.23} + [CH_4]_i \right)$$

where:

$[ETOH]_i$ = Ethanol concentration determined from a single GC analysis (ppmv/wet)

$[AA]_i$ = Acetaldehyde concentration determined from a single GC analysis (ppmv/wet)

$[CH_4]_i$ = Methane concentration determined from a single GC analysis (ppmv/wet)

7.3 Method 25A Calculations

This section briefly summarizes calculations used for the Method 25A analysis. The computer controlled data acquisition system scanned each channel approximately 1800 times per minute and stored periodic averages on disk and hard copy. The averaging computer period varied throughout the test program ranging from 10 seconds to 1 minute. Pre-test calibration, post-test calibration drift checks, and calibration error checks were saved on disk. Instrument drift was evaluated after the post-test calibration with an acceptable criterion of ± 3 . The computer DAS reported THC concentrations calculated as follows:

$$C_{\text{sample}} = RSP_{\text{sample}} \times RFAC + C_{\text{rsp}=0}$$

where:

C_{sample} = Observed concentration of sample gas (ppmv or %v, dry)

RSP_{sample} = Observed instrument sample voltage response (volts)

$C_{\text{rsp}=0}$ = Calculated concentration corresponding to an instrument response of 0 volts (Y intercept)

RFAC = Calibration response factor (slope)

$$RFAC = \frac{(SPAN - ZERO)}{(RSP_{\text{span}} - RSP_{\text{zero}})}$$

where:

SPAN = Concentration of high (span) calibration gas (ppmv)

ZERO = Concentration of low (zero) calibration gas (ppmv)

RSP_{span} = Observed instrument voltage response to the span calibration gas (volts)

RSP_{zero} = Observed instrument voltage response to the zero calibration gas (volts)

Span and zero calibration drifts are calculated as follows:

$$\text{Drift} = \frac{(C_F - C_I)}{FULL\ RANGE} \times 100$$

where:

Drift = Span calibration drift (% of Scale)

Full Range = Full Range of the Instrument (i.e. 0-500 ppmv)

C_F = Observed concentration predicted by the final calibration - (ppmv)

C_I = Observed concentration predicted by the initial calibration (ppmv)

Average concentrations of THC were calculated for the test duration of interest.

7.3.1 Method 18 Data Reduction

The concentration of ethanol, acetaldehyde, methane and ethane in the stack gas was determined directly as parts per million by volume (ppmv) on a wet basis. An electronic integrator would convert the GC electrical peak signals to a peak area value. A linear regression was completed using calibration gas concentration versus peak area response. Sample responses (peak areas) were then used in the calibration regression to determine the respective concentration.

7.3.2 Manual Gas Sampling Methods

Calculations for determining flow rate, moisture content, and gas molecular weight are described in Figures 7-1 and 7-2.

**RADIAN SOURCE TEST
EPA METHODS
DEFINITION OF TERMS**

Parameter	Units	Definition
t	min.	Total Sampling Time
D _n	in.	Sampling Nozzle Diameter
V _m	ft ³	Absolute Volume of Gas Sample Measured by DGM (uncorrected)
M _w	g	Total Mass of Water Collected
M _p	g	Total Mass of Particulate Collected
P _m	in. Hg	Absolute Meter Pressure
ΔH	in. H ₂ O	Average Static Pressure of DGM
T _m	°F	Average Temperature of DGM
P _{bar}	in. Hg	Barometric Pressure
%CO ₂	% vol-dry	Carbon Dioxide Content of Flue Gas
%O ₂	% vol-dry	Oxygen Content of Flue Gas
%N ₂	% vol-dry	Nitrogen Content of Flue Gas (by difference)
A _s	ft ³	Cross-sectional Area of Stack (Duct)
T _s	°F	Temperature of Stack
P _s	in. Hg	Absolute Stack Gas Pressure
Static	in. H ₂ O	Stack Static Pressure
V _{m(std)}	dscf	Volume of Gas Sampled at Standard, Dry Conditions ^a
V _w	scf	Volume of Water Vapor in Gas Sample, Std

Figure 7-1. Definition of Terms for Method 1-4 Calculations

**RADIAN SOURCE TEST
EPA METHODS
DEFINITION OF TERMS
(Continued)**

Parameter	Units	Definition
B_{ws}		Fraction of Water Vapor in Stack Gas
M_d		Fraction by Volume of Dry Gas in Gas Sample ($1-B_{ws}$)
MW_d	lb/lb mole	Molecular Weight of Dry Stack Gas, Dry Basis
MW_s	lb/lb mole	Molecular Weight of Stack Gas, Wet Basis
C_p		Pitot Coefficient (typically 0.84)
C_s	grains/ft ³	Concentration of Particulate in Flue Gas
E	lb/hr	Emission Rate of Particulate
Q_{sd}	dry, ft ³ /min.	Average Stack Dry Volumetric Flow Rate
V_s	ft/sec	Velocity of Stack Gas
Y		Test Meter Calibration Coefficient
ΔP	in. H ₂ O	Stack Gas Velocity Pressure

Figure 7-1. Continued

RADIAN SOURCE TEST **EPA METHOD 2 - 5** **SAMPLE CALCULATION**

- 1) Volume of dry gas sampled at standard conditions (68°F, 29.92 in. Hg):

$$V_{m(std)} = \frac{Y \times V_m \times 528 \times [P_{bar} + (\Delta H/13.6)]}{29.92 \times (T_m + 460)}$$

- 2) Volume of water vapor at standard conditions:

$$V_w = \frac{0.04715 \text{ ft}^3}{g \times M_w}$$

- 3) Fractional moisture content in stack gas:

$$B_{ws} = \frac{V_w}{V_{m(std)} + V_w}$$

- 4) Mole fraction of dry stack gas:

$$M_d = 1 - B_{ws}$$

- 5) Absolute stack gas pressure:

$$P_s = P_{bar} + \frac{\text{Static}}{13.6}$$

Figure 7-2. Example of Method 1-4 Calculations

6) Average molecular weight of dry stack gas:

$$\text{Dry: } MW_d = (0.32 \times \%O_2) + (0.44 \times \%CO_2) + [0.28 \times (100 - (\%O_2 + \%CO_2))]$$

7) Stack gas velocity at stack conditions:

$$V_s = 85.49 \times 0.84 \times \sqrt{\Delta P} \times \sqrt{\frac{T_s + 460}{P_s \times MW_s}}$$

8) Average stack gas volumetric flow at dry, standard conditions:

$$Q_{sd} = V_s \times A_s \times M_d \times \frac{528 \times P_s}{T_s \times 29.92} \times \frac{60 \text{ sec}}{\text{min}}$$

Figure 7-2. Continued

APPENDIX B

Site 2

- B.1 Method 25A (THC) Log**
- B.2 Method 25A (THC) Data**
- B.3 Method 18 Analytical Summary**
- B.4 Method 18 Chromatogram**
- B.5 Field Flow Measurements Data Sheets**
- B.6 Field H₂O Data Sheets**
- B.7 Flow Calculations**
- B.8 Test Log**
- B.9 Method 25A SCR Copies**

Method B.1

Method 25A (THC) Log

CALCULATION SHEET

CALC. NO. _____

SIGNATURE _____ DATE _____ CHECKED _____ DATE _____

PROJECT EPA EMB B.L.W. - Norristown JOB NO. _____

SUBJECT THC Log SHEET _____ OF _____ SHEETS

SITE 2
TEST DATE 6/17

- DAY 1

TIME

EVENT

RESULT

10:14

CAL

3980 ppm C, 0

1020

1490 QC

(Tag)

T

1512.6

(Rock)

R

1514.2

1023

798 QC

T

812.9

R

814.2

1027

199 QC

T

213.6

R

217.8

3980 QC

T

3979.6

R

4013.1

1037.50

RECAL (0617B.CAL)

1056

RECAL (0617C.CAL)

1132.49-

1259.49

1217

1309

SAMPLE

T = FRONT

R = REAR

N₂ up the line

179.1 QC

T

215.9

R

204.9

1317

798 QC

T

807.6

R

748.6

1320

1490 QC

T

1496.5

R

1436.1

1324

3980 QC

(RE-CAL ON R)

T

3931.3

R

3752.8

1345:54 - 1422

SAMPLE -

T = REAR

R = FRONT

SIGNATURE _____ DATE _____ CHECKED _____ DATE _____

PROJECT _____ JOB NO. _____

SUBJECT _____ SHEET _____ OF _____ SHEETS

 SITE 2 - DAY 1 (6/17/92)
 (cont)

TIME	EVENT	RESULT
1430	1490 QC	T = 1493.1 R = 1515.2
1432	80.2 QC	T = 90.9 R = 92.5
1440	80.2 QC	T = 89.7 R = 87.5
1451-1513	80.2 QC (trying to iron out GC problems)	T = 89.2 n=14 R = 88.5 n=13
1517-1615	Sample	Rear = T Front = R
1615	O GAS QC \Rightarrow SCR only \Rightarrow OK	
1622-1626	LINE 1 COMFORT READ on T = 1113 ppmC	
1640	LINE 2 COMFORT READ on T = 121.1 ppmC	
1647-1747	LINE 2 Area Sample; combustion stack	Front: T = 669.4 Rear = R = 48.4
1753-1755	O GAS QC	T = 11.1 R = 1.5
1756-1759	80.2 QC	T = 90.0 R = 86.8
1800-1804	79.8 QC	T = 809.7 R = 772.4

SIGNATURE _____ DATE _____ CHECKED _____ DATE _____

PROJECT _____ JOB NO. _____

SUBJECT _____ SHEET _____ OF _____ SHEETS

SITE 2 - DAY 1 (cont) 7/17/92

TIME
EVENT
RESULT

1805 - 1809

199.1 AC

T = 212.0

R = 217.9

1811 - 1814

200 Exhaust

T = 305.9

R = 295.5

1815 - 1818

1490 AC

T = 1505.1

R = 1524.3

1819 - 1820

3980 AC

T = 3966.9

R = 3953.9

1822 - 1824

200 Exhaust

T = 310.6

R = 295.9

1834 - 1835

Q Gas AC

T = 9.2

R = 5.1

1836 - 1844

LINE 1 COMPOST 1600

1072.3

LINE 2 COMPOST 1600

149.2

CALCULATION SHEET

CALC. NO. _____

SIGNATURE _____ DATE _____ CHECKED _____ DATE _____

PROJECT _____ JOB NO. _____

SUBJECT _____ SHEET _____ OF _____ SHEETS

SITE 2

DAY 2

(6/18/92)

TIME

EVENT

RESULT

14:56

CAL

0 @ 2000 ppm

1501 - 1503

199.1 QC

T = 209.3

R = 206.3

1506 - 1507

798 QC

T = 782.6

R = 801.2

1509 - 1510

1490 QC

T = 1467.5

R = 1448.9

1522 - 1527

LINE 3 C.H. = R

Rear. T = 2781.6

1529

3980 QC

T = 3124

R = 3036.6

C.H. = R = 626.4

n = 10

 1535 - 1545 ~~1545 - 1553~~
 1646

LINE 3 - Rear

Rear = R =

1535 - 1549

LINE 3 CH

C.H. = R = 707.4

n = 29

1552 - 1609

LINE 3 FRONT

F = R =

1609 - 1642

 LINE 3 FRONT + multiple shots (apparent noise)
 (multiple QC's)

1644 - 1647

2000 QC

T = 2041.4

Front = R = 1936.4

1648 - 1652

LINE 3 FRONT

1654 - 1703

LINE 3 FRONT

1648 - 1703

LINE 3 Rear

17004 - 1707

2000 QC

T = 2099.5

R = 1937.6

SIZE 2 - DAY 2 (cont)

TIME	EVENT	RESULT
1709-1717	LINE 3 FRONT	Front Rack =
1709-1737	LINE 3 RUN	R = Table =
1722-1737	LINE 3 FRONT	F = Rack =
1745-1808	LINE CH	→ R = Table =
1750-1815	LINE 3 RUN	
1818-1822	80.2 QC	T = 92.7 R = 86.8 (H)
1823-1911	LINE 3	FRONT = R : RUN = T :
1915-1917	199.1 QC	T = 159.4 R = 102
1919-1921	798 QC	T = 813.2 R = 754.8 (C)
1927-1930	1490 QC	T = 1480 A = 1428.9 (C)
1934-1935	2000 QC	T = 2008.5 R = 2031.9 (H)
1940-1942	3980 QC	T = 3846.4 (C) A = 3723.7 (C)
- 0.79	← SPAN DRIFT CHC @ 3980	→ - 1.17

Appendix B.2

Method 25A (THC) Data

06-18-1992 SITE 2 DAY 2

TIME	THC 2 (table) (ppmC)	THC 2 (rack) (ppmC)	Comments	FRONT				REAR	
				ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
14:58:46	1943.976	1644.847							
14:59:46	271.2307	209.8175				AA/THC :			
15:00:46	223.4724	210.7397				:			
15:01:01	211.7186	206.8361				:			
15:01:16	211.0331	208.2457				:			
15:01:31	210.7684	207.0617				:			
15:01:46	208.7186	207.0169				:			
15:02:01	208.3118	205.9635				:			
15:02:16	207.8076	206.0426				:			
15:02:31	208.8938	204.1604				:			
15:02:46	207.4395	204.7147				:			
15:03:01	205.9644	144.3826				:			
15:03:16	83.55556	15.86107				:			
15:03:31	44.56439	590.0475				:			
15:03:46	667.9737	708.1881				:			
15:04:01	768.6145	726.632				:			
15:04:16	777.8843	732.4269				:			
15:04:31	780.0513	720.4459				:			
15:04:46	781.2154	729.6679				:			
15:05:01	780.9995	771.1944				:			
15:05:16	781.7652	800.8113				:			
15:05:31	781.3041	803.6083				:			
15:05:46	781.1827	806.4679				:			
15:05:56	783.1445	802.5641				:			
15:06:06	782.7897	798.1838				:			
15:06:16	782.7065	793.6049				:			
15:06:26	783.2715	808.9261				:			
15:06:36	783.4602	776.2615				:			
15:06:46	782.0455	800.3516				:			
15:06:56	780.8074	655.7911				:			
15:07:06	606.0389	175.7626				:			
15:07:16	112.7545	1310.974				:			
15:07:26	786.3737	1387.016				:			

ETH/THC CH4/THC AA/THC

06-18-1992 SITE 2 DAY 2

TIME	THC 2		Comments	FRONT			REAR		
	(table)	(rack)		ETH-OH (ppmV/wet)	CH ₄ (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH ₄ (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:07:36	1059.945	1416.867		:	:	:	:	:	:
15:07:46	1129.225	1496.055		:	:	:	:	:	:
15:07:56	1402.788	1462.717		:	:	:	:	:	:
15:08:06	1444.08	1488.8		:	:	:	:	:	:
15:08:16	1449.553	1473.248		:	:	:	:	:	:
15:08:26	1448.807	1491.162		:	:	:	:	:	:
15:08:36	1451.758	1472.384		:	:	:	:	:	:
15:08:46	1467.175	1464.984		:	:	:	:	:	:
15:08:58	1466.342	1482.532		:	:	:	:	:	:
15:09:06	1468.398	1523.317		:	:	:	:	:	:
15:09:16	1468.642	1476.158		:	:	:	:	:	:
15:09:26	1467.896	1480.766		:	:	:	:	:	:
15:09:36	1468.293	1468.851		:	:	:	:	:	:
15:09:46	1466.438	1509.188		:	:	:	:	:	:
15:09:56	1466.63	1481.202		:	:	:	:	:	:
15:10:06	1469.702	1467.766		:	:	:	:	:	:
15:10:16	1466.674	1460.997		:	:	:	:	:	:
15:10:26	1385.767	1792.144		:	:	:	:	:	:
15:10:36	1453.781	2112.945		:	:	:	:	:	:
15:10:46	1957.926	2129.275		:	:	:	:	:	:
15:10:56	1991.585	2136.169		:	:	:	:	:	:
15:11:06	2006.345	2117.886		:	:	:	:	:	:
15:11:16	2007.011	2126.896		:	:	:	:	:	:
15:11:26	2013.084	2081.63		:	:	:	:	:	:
15:11:36	2019.19	2028.353		:	:	:	:	:	:
15:11:46	2024.628	2034.119		:	:	:	:	:	:
15:11:56	2019.65	2046.688		:	:	:	:	:	:
15:12:06	2023.042	1948.711		:	:	:	:	:	:
15:12:16	2025.332	1967.364		:	:	:	:	:	:
15:12:26	2026.607	1971.07		:	:	:	:	:	:
15:12:36	2028.15	1980.634		:	:	:	:	:	:
15:12:46	2025.949	1975.602		:	:	:	:	:	:
15:12:56	2026.069	1973.941		:	:	:	:	:	:

06-18-1992 SITE 2 DAY 2

TIME	THC 2		Comments	FRONT			REAR		
	(table)	(rack)		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:13:06	2026.483	1976.645							
15:13:16	2028.145	1968.135							
15:13:26	2024.93	1980.453							
15:13:36	2026.39	1976.434							
15:13:46	2027.102	1970.321							
15:14:57	2024.755	1974.269							
15:14:57	2024.755	1974.269							
15:14:57	2024.755	1974.269							
15:14:58	2024.755	1974.269							
15:14:58	2024.755	1974.269							
15:14:59	2024.755	1974.269							
15:15:06	1476.579	1357.619							
15:15:16	1473.048	1342.564							
15:15:26	1470.725	1388.994							
15:15:36	1469.957	1362.338							
15:15:46	1473.474	1337.353							
15:15:56	1466.22	1351.184							
15:16:06	1467.493	1440.789							
15:16:16	1469.328	1450.26							
15:16:26	1467.912	1439.354							
15:16:36	1470.163	1463.688							
15:16:46	1467.416	1478.292							
15:16:56	1468.274	1486.526							
15:17:26	1469.922	1450.883							
15:17:56	1478.771	1731.643							
15:18:26	1951.486	2138.999							
15:18:56	2013.933	2142.138							
15:19:26	2020.438	2147.646							
15:19:56	2022.512	2077.066							
15:20:29	2026.032	2035.543							
15:20:29	2026.032	2035.543							
15:20:29	2026.032	2035.543							

06-18-1992 SITE 2 DAY 2

TIME	THC 2		Comments	FRONT				REAR	
	(table)	(rack)		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:20:36	2024.974	2027.843		:	:	:	:	:	:
15:20:46	2025.202	2039.197		:	:	:	:	:	:
15:20:56	2025.846	2029.526		:	:	:	:	:	:
15:21:06	2025.983	2036.491		:	:	:	:	:	:
15:21:16	2025.898	2041.826		:	:	:	:	:	:
15:21:57	2021.512	1500.184		:	:	:	:	:	:
			COMFORT	:	:	:	:	:	:
			HOOD	:	:	:	:	:	:
			SAMPLE	:	:	:	:	:	:
15:22:16	2771.563		529.4875	:	:	:	:	:	:
15:22:46	2779.288		627.1813	:	:	:	:	:	:
15:23:16	2744.91		639.5832	:	:	:	:	:	:
15:23:46	2729.335		618.4581	:	:	:	:	:	:
15:24:16	2791.507		623.8492	:	:	:	:	:	:
15:24:46	2781.733		703.6897	:	:	:	:	:	:
15:25:16	2742.532		631.322	:	:	:	:	:	:
15:25:46	2762.241		636.342	:	:	:	:	:	:
15:26:16	2849.168		651.4839	:	:	:	:	:	:
15:26:46	2864.143		602.6091	:	:	:	:	:	:
AVG	2781.642		626.4006	:	:	:	:	:	:
			10	:	:	:	:	:	:
			END	:	:	:	:	:	:
15:27:17				:	:	:	:	:	:
15:27:46				:	:	:	:	:	:
15:28:16				:	:	:	:	:	:
15:28:46				:	:	:	:	:	:
15:29:16				:	:	:	:	:	:
15:29:46				:	:	:	:	:	:
15:30:16				:	:	:	:	:	:
15:30:46				:	:	:	:	:	:
15:31:16				:	:	:	:	:	:

SITE 2 DAY 2

TIME	THC 2 (table) (ppmC)	THC 2 (rack) (ppmC)	Comments	FRONT			REAR		
				ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:31:46						2174.158			
15:32:16						2128.842			
15:32:46						2064.535			
15:33:16						187.7636			
15:33:46						15.06306			
15:34:16						531.7414			

REAR

SAMPLE

15:34:57	2816.961	579.7957
15:35:16	2746.707	579.4509
15:35:46	2723.444	677.3429
15:36:16	2814.428	634.7269
15:36:46	2855.104	685.1783
15:37:16	2868.365	638.0857
15:37:53	2856.638	628.3115
15:38:29	2895.52	638.3364
15:39:27	2962.732	735.1356
15:39:28	2962.732	735.1356
15:39:46	3087.749	691.0191
15:40:16	3009.593	691.7719
15:40:46	2934.627	729.1828
15:41:16	2915.588	631.7565
15:41:46	2879.072	619.1533
15:42:16	2906.247	683.5627
15:42:46	2910.014	743.3297
15:43:16	2960.489	734.718
15:43:46	2947.689	744.0379
15:44:16	2905.591	750.3389
15:44:46	2809.4	694.6087
15:45:16	2822.866	700.1744

06-18-1992

SITE 2 DAY 2

TIME	THC 2		Comments	FRONT			REAR		
	(table)	(rack)		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:45:46	2850.687		700.9904			:			
15:46:16	2900.24		727.1694			:			
15:46:46	2901.281		804.1381			:			
15:47:16	2859.222		767.6116			:			
15:47:46	2880.203		811.9131			:			
15:48:16	2967.107		902.6684			:			
15:48:46	2988.367		853.7667			:			
AVG	2894.429		707.3590			:			

END COMFORT
HOOD

REAR
(cont)

15:49:16	2986.68								
15:49:46	2982.872					178.1494			
15:50:16	2997.226					15.9634			
15:50:46	3042.19					12.9656			
15:51:16	3039.821					12.68983			
15:51:46	3032.455					77.36836			
15:52:16	3025.591					3527.847			
15:52:46	3062.125					3806.654			
						3977.829			

SAMPLE	FRONT		REAR (cont)	FRONT			REAR		
	ETH-OH	CH4		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:53:16	3062.043	4106.216				:			
15:53:46	3057.768	4084.392				:			
15:54:16	3126.671	4218.578				:			
15:54:46	3146.596	4078.046				:			
15:55:16	3138.681	4317.232				:			
15:55:46	3171.753	4125.537				:			
15:56:16	3178.059	4168.84				:			
15:56:46	3156.203	4175.098				:			
15:57:16	3157.481	4436.521				:			

1710 1980 78.4
ETH/THC CH4/THC AA/THC
54.34444 62.92514 2.491581378

06-18-1992 SITE 2 DAY 2

TIME	THC 2		Comments	FRONT			REAR		
	(table)	(rack)		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:57:46	3139.084	4333.136							
15:58:16	3092.338	4349.911							
15:58:46	3082.853	4522.271							
15:59:16	3092.099	4345.289							
15:59:46	3120.508	4218.676							
16:00:16	3162.707	4414.49							
16:00:46	3105.712	4241.556							
16:01:16	3070.81	4639.898							
16:01:46	3024.938	4524.827							
16:02:16	3037.371	4757.162							
16:02:46	3027.384	4415.563							
16:03:16	3066.947	4315.403							
16:03:46	3131.128	4250.123							
16:04:16	3148.569	4299.882							
16:04:46	3186.586	4223.482							
16:05:16	3221.043	4295.285							
16:05:46	3213.316	4530.658							
16:06:16	3222.069	4251.827							
16:06:46	3200.063	4272.474							
16:07:16	3199.175	4442.177							
16:07:46	3183.497	4216.242							
16:08:16	3182.526	3967.62							
16:08:46	3161.026	4135.291							
16:09:16	3144.58	4233.419							
AVG	3133.684	4300.215							

33

END REAR
FRONT (cont)

16:09:46
16:10:16
16:10:46
16:11:16

06-18-1992 SITE 2 DAY 2

TIME	THC 2		FRONT		REAR	
	(table)	(rack)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			ACETALDEHYDE: (ppmV/wet) :			
			(ppmV/wet) (ppmV/wet) (ppmV/wet) (ppmV/wet)			
			=====			
16:11:46						
16:12:16						
16:12:46					1750	1550
16:13:16						82
16:13:46					ETH/THC	AA/THC
16:14:16					56.35281	49.91249
16:14:46						2.640531841
16:15:16						
16:15:46						
16:16:16						
16:16:46						
16:17:16						
16:17:46						
16:18:16						
16:18:46						
16:19:16						
16:19:46						
16:20:16						
16:20:46						
16:21:16						
16:21:55						
16:22:28						
16:22:46						
16:23:16						
16:23:46						
16:24:16						
16:24:46						
16:25:16						
16:25:46						
16:26:16						
16:26:46						
16:27:16						
16:27:46						

2900	491	97.7	813.4313	2900	491	97.7
ETH/THC	CH4/THC	AA/THC	875.1298	ETH/THC	CH4/THC	AA/THC
356.5144345	60.36158185	12.01084836	847.821	88.67384	15.01339	2.987391191
			889.0707			
			814.7026			
			-339.692			
			3191.635			
			1037.256			
			648.6523			
			656.5995			
			2026.474			
			2712.847			
			1860.57			

06-18-1992 SITE 2 DAY 2

TIME	THC 2 (table) (rack) (ppmC) (ppmC) Comments	FRONT			REAR		
		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet) :	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
16:28:16				839.0237			
16:28:46				170.6055			
16:29:16				513.0793			
16:29:46				1596.031			
16:30:16				4058.852			
16:30:46				2827.736	1820	1970	78.2
16:31:16				1846.87	ETH/THC	CH4/THC	AA/THC
16:31:46				164.6906	61.80106	66.89456	2.655408459
16:32:16				1380.047			
16:32:46				2236.477			
16:33:16				1982.732			
16:33:46				789.797			
16:34:16				36.3135			
16:34:46				17.75572			
16:35:16				132.4754			
16:35:46				201.7341			
16:36:16				203.0156			
16:36:46				202.6795			
16:37:16				1146.619			
16:37:46				1973.024			
16:38:16				862.3318			
16:38:46				23.88713			
16:39:16				19.24692			
16:39:46				19.4103			
16:40:16				21.00238			
16:40:46				20.15888			
16:41:16				22.34725			
16:41:46				22.01925			
16:42:16				19.17829			
16:42:46				17.74096			
16:43:16				3489.432			
16:43:46				4449.579			
16:44:16				4459.884			

06-18-1992 SITE 2 DAY 2

TIME	THC 2		Comments	FRONT			REAR		
	(table) (ppmC)	(rack) (ppmC)		ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
=====									
SAMPLE									
						:	:	:	:
						:	:	:	:
						:	:	:	:
						:	:	:	:
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	THC 2	THC 2		FRONT		REAR	
TIME	(table)	(rack)		ETH-OH (ppmV/wet)	CH ₄ (ppmV/wet)	ETH-OH (ppmV/wet)	CH ₄ ACETALDEHYDE (ppmV/wet)
	(ppmC)	(ppmC)	Comments	:	:	:	: (ppmV/wet)
=====							
17:23:16	3108.18					3490.91	AA/THC 40.12623 65.45180 2.377972671

	FRONT		REAR	
SAMPLE	ETH-OH	CH ₄	ETH-OH	CH ₄
	REAR	FRONT	(ppmV/wet)	(ppmV/wet)
(cont)			=====	=====
			ACETALDEHYDE:	ACETALDEHYDE
			(ppmV/wet) :	(ppmV/wet)
			=====	=====

17:23:46 3166.132 3907.732
17:24:16 3121.638 3839.351
17:24:46 3006.246 3707.778
17:25:16 2870.223 3901.071
17:25:46 2780.466 3594.903
17:26:16 2816.794 3765.306
17:26:46 2810.917 3774.719
17:27:16 2724.283 3781.819
17:27:46 2712.519 4114.367
17:28:16 2685.548 4276.58
17:28:46 2709.733 3994.06
17:29:16 2990.676 4158.607

17:29:46 2753.491 4059.636
17:30:16 2770.663 4222.394
17:30:46 2882.125 3976.181
17:31:16 2912.431 3760.662
17:31:46 2893.981 3560.941
17:32:16 2912.332 3334.742
17:32:46 2922.649 3599.795
17:33:16 2902.529 3354.443
17:33:46 2885.504 3036.571
17:34:16 2865.906 2973.979
17:34:46 2834.179 3044.876
17:35:16 2787.992 2722.668
17:35:46 2735.944 2714.479
17:36:16 2661.176 2924.77
17:36:46 2698.582 3093.406

END

SITE 2 DAY 2

TIME	THC 2 (table)	THC 2 (rack)	Comments
0.00			
0.05			
0.10			
0.15			
0.20			
0.25			
0.30			
0.35			
0.40			
0.45			
0.50			
0.55			
0.60			
0.65			
0.70			
0.75			
0.80			
0.85			
0.90			
0.95			
1.00			
1.05			
1.10			
1.15			
1.20			
1.25			
1.30			
1.35			
1.40			
1.45			
1.50			
1.55			
1.60			
1.65			
1.70			
1.75			
1.80			
1.85			
1.90			
1.95			
2.00			
2.05			
2.10			
2.15			
2.20			
2.25			
2.30			
2.35			
2.40			
2.45			
2.50			
2.55			
2.60			
2.65			
2.70			
2.75			
2.80			
2.85			
2.90			
2.95			
3.00			
3.05			
3.10			
3.15			
3.20			
3.25			
3.30			
3.35			
3.40			
3.45			
3.50			
3.55			
3.60			
3.65			
3.70			
3.75			
3.80			
3.85			
3.90			
3.95			
4.00			
4.05			
4.10			
4.15			
4.20			
4.25			
4.30			
4.35			
4.40			
4.45			
4.50			
4.55			
4.60			
4.65			
4.70			
4.75			
4.80			
4.85			
4.90			
4.95			
5.00			
5.05			
5.10			
5.15			
5.20			
5.25			
5.30			
5.35			
5.40			
5.45			
5.50			
5.55			
5.60			
5.65			
5.70			
5.75			
5.80			
5.85			
5.90			
5.95			
6.00			
6.05			
6.10			
6.15			
6.20			
6.25			

17:47:16 3068.692 4017.734
17:47:46 3049.868 4104.956

17:48:16
17:48:46
17:49:16
17:49:46
17:50:16

17:50:46 3141.947
17:51:16 3117.182
17:51:46 3020.123
17:52:16 2995.351

17:52:46	2974.904	
17:53:16	2860.76	
17:53:46	2798.155	
17:54:16	2865.021	
17:54:46	2928.2	
17:55:16	3022.83	602.6726
17:55:46	3022.853	615.4163
17:56:16	2996.629	605.7041
17:56:46	2980.398	609.0621
17:57:16	2952.051	601.1946
17:57:46	3004.879	612.0377
17:58:16	3043.046	621.1059
17:58:46	2970.35	615.6436
17:59:16	2903.884	603.5606

FRONT		REAR	
ETH-OH	CH ₄	ETH-OH	CH ₄
(ppmV/wet)	(ppmV/wet)	(ppmV/wet)	(ppmV/wet)
ACETALDEHYDE:	ACETALDEHYDE:	ETH-OH	CH ₄
(ppmV/wet)	(ppmV/wet)	(ppmV/wet)	(ppmV/wet)

2347.253
3391.118
1535.588
34.40333
35.14402

ETH-OH	CH ₄	35.14402	REAR
PROBES SWITCHED	BACK	ACETALDEHYDE:	CH ₄
REAR	???	(ppmV/wet) :	ACETALDEHYDE
		(ppmV/wet)	(ppmV/wet)

	1390	2050	74.3
ETH/THC	CH4/THC	AA/THC	
46.72419	68.90978	2.497559585	

06-18-1992 SITE 2 DAY 2

TIME	THC 2		THC 2 (table) (rack) (ppmC) (ppmC)	Comments	FRONT			REAR		
					ETH-OH (ppmV/wet)	CH ₄ (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH ₄ (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
17:59:46	2786.782			591.7236						
18:00:16	2702.792			566.2424						
18:00:46	2769.421			566.5542						
18:01:16	2784.412			566.3031						
18:01:46	2799.693			568.2486						
18:02:16	2814.09			568.0712						
18:02:46	2757.321			569.2544						
18:03:16	2765.154			562.4448						
18:03:46	2827.04			570.1789						
18:04:16	2907.814			575.1313				1480	2030	66.7
18:04:46	2926.451			586.5651				ETH/THC	CH ₄ /THC	AA/THC
18:05:16	2911.401			584.205				50.89734	69.81189	2.293819343
18:05:46	2861.591			576.6274						
18:06:16	2842.337			578.6799						
18:06:46	2824.325			577.2324						
18:07:16	2768.551			570.361						
18:07:46	2762.035			566.321						
AVG	2897.422			585.7900						
				35						
					REAR	FRONT				
18:08:16	2848.645	2303.775								
18:08:46	2879.718	2728.938								
18:09:16	2859.489	2556.372								
18:09:46	2890.44	2607.902								
18:10:16	2881.295	2814.372								
18:10:46	2874.321	3273.104								
18:11:16	2820.809	3397.391								
18:11:46	2804.385	3587.195								
18:12:16	2830.558	3075.4								
18:12:46	2875.023	3226.874								
18:13:16	2870.182	3660.602								
18:13:46	2790.28	3688.223								

[illegible]

END

15

18:21:16 85.75092

REAR	FRONT	2923.611	REAR
ETH-OH	CH ₄	ACETALDEHYDE:	CH ₄
(ppmV/wet)	(ppmV/wet)	(ppmV/wet) :	(ppmV/wet)
ACETALDEHYDE			

18-22:46 2880.956 3989.504
18-23:16 2873.086 3907.535
18-23:46 2856.618 4016.318
18-24:16 2892.731 3933.137
18-24:46 3002.427 3751.498
18-25:16 3032.445 3882.373
18-25:46 3127.19 4315.188
18-26:16 3167.691 4325.199

SITE 2 DAY 2

TIME	THC 2 (table) (ppmC)	THC 2 (rack) (ppmC)	Comments	FRONT			REAR		
				ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
18:26:46	3114.099	4129.723		:	:	:	:	:	:
18:27:16	3062.249	4325.542		:	:	:	:	:	:
18:27:46	3041.269	4066.168		:	:	:	:	:	:
18:28:16	3021.512	4026.959		:	:	:	:	:	:
18:28:46	3007.612	4233.613		:	:	:	:	:	:
18:29:16	3014.276	4173.358		:	:	:	:	:	:
18:29:46	3029.308	4021.944		:	:	:	:	:	:
18:30:16	3062.783	4174.524		:	:	:	:	:	:
18:30:46	3038.136	4433.809		:	:	:	:	:	:
18:31:16	2992.207	4281.006		:	:	:	:	:	:
18:31:46	2985.836	4124.846		:	:	:	:	:	:
18:32:16	3029.013	4166.287		:	:	:	:	:	:
18:32:46	2951.915	3895.399		:	:	:	:	:	:
18:33:16	2934.01	3690.308		:	:	:	:	:	:
18:33:46	2952.376	3951.9		:	:	:	:	:	:
18:34:16	2994.42	4555.959		:	:	:	:	:	:
18:34:46	3030.901	4411.406		:	:	:	:	:	:
18:35:16	3032.032	4226.694		:	:	:	:	:	:
18:35:46	3045.045	4378.013		:	:	:	:	:	:
18:36:16	3082.534	4395.369		:	:	:	:	:	:
18:36:46	3102.094	4199.604		:	:	:	:	:	:
18:37:16	3080.072	4303.096		:	:	:	:	:	:
18:37:46	3069.91	4179.546		:	:	:	:	:	:
18:38:16	3073.908	4291.055		:	:	:	:	:	:
18:38:46	3071.431	4223.798		:	:	:	:	:	:
18:39:16	3005.503	4584.064		:	:	:	:	:	:
18:39:46	2916.143	4462.451		:	:	:	:	:	:
18:40:16	2988.747	4237.475		:	:	:	:	:	:
18:40:46	3072.797	4162.728		:	:	:	:	:	:
18:41:16	3124.871	4416.288		:	:	:	:	:	:
18:41:46	3158.302	4498.099		:	:	:	:	:	:
18:42:16	3181.904	4588.507		:	:	:	:	:	:
18:42:46	3148.418	4664.046		:	:	:	:	:	:

06-18-1992 SITE 2 DAY 2

TIME	THC 2 (table) (ppmC)	THC 2 (rack) (ppmC)	Comments	FRONT				REAR			
				ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
18:43:16	3150.436	4443.941		52.08665912	33.56211508	2.854959140					
18:43:46	3180.822	4422.763		:	:	:					
18:44:16	3168.212	4541.276		:	:	:					
18:44:46	3163.137	4367.647		:	:	:					
18:45:16	3158.801	4184.413		:	:	:					
18:45:46	3175.945	4343.411		:	:	:					
18:46:16	3173.449	4559.877		:	:	:					
18:46:46	3119.278	4483.246		:	:	:					
18:47:16	3106.163	4321.026		:	:	:					
18:47:46	3167.997	4557.874		:	:	:					
18:48:16	3177.981	4254.963		:	:	:					
18:48:46	3163.388	4098.399		:	:	:					
18:49:16	3138.348	4052.168		:	:	:					
18:49:46	3131.747	4468.989		:	:	:					
18:50:16	3135.133	4549.21		:	:	:					
18:50:46	3125.054	4449.696		:	:	:					
18:51:16	3127.012	4676.39		:	:	:					
18:51:46	3177.154	4650.754		:	:	:					
18:52:16	3168.432	4529.797		:	:	:					
18:52:46	3141.889	4786.65		:	:	:					
18:53:16	3096.68	4682.288		:	:	:					
18:53:46	3026.438	4591.033		:	:	:					
18:54:16	3029.514	4617.334		:	:	:					
18:54:46	2996.076	4749.428		:	:	:					
18:55:16	3003.734	4505.72		:	:	:					
18:55:46	3007.306	4500.131		:	:	:					
18:56:16	3022.229	4715.73		:	:	:					
18:56:46	2972.14	4206.72		:	:	:					
18:57:16	3013.294	4477.867		:	:	:					
18:57:46	3060.891	4474.124		:	:	:					
18:58:16	3114.996	4718.222		:	:	:					
18:58:46	3147.354	4479.313		:	:	:					
18:59:16	3218.114	4209.51		:	:	:					
							1850	1940	83.4		
							ETH/THC	CH4/THC	AA/THC		
							58.22821	61.06093	2.624990793		

06-18-1992 SITE 2 DAY 2

TIME	THC 2 (table) (ppmC)	THC 2 (rack) (ppmC)	Comments	FRONT			REAR		
				ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
19:58:06	635.8655	625.3951		:	:	:	:	:	:
19:59:06	634.7297	631.1142		:	:	:	:	:	:
20:00:06	635.4781	633.527		:	:	:	:	:	:
20:01:06	643.2603	654.9675		:	:	:	:	:	:
20:02:06	706.4955	732.9196		:	:	:	:	:	:
20:03:06	734.2877	781.7604		:	:	:	:	:	:
20:04:06	834.2021	872.818		:	:	:	:	:	:
20:05:06	944.9283	1012.063		:	:	:	:	:	:
20:06:06	1173.659	1275.422		:	:	:	:	:	:
20:07:06	1408.282	1588.23		:	:	:	:	:	:
20:08:06	1705.889	1935.15		:	:	:	:	:	:
20:09:06	2108.292	2449.26		:	:	:	:	:	:
20:10:06	2680.383	2958.52		:	:	:	:	:	:
20:11:06	2937.173	3300.674		:	:	:	:	:	:
20:12:06	3436.265	3823.128		:	:	:	:	:	:
20:13:06	3740.343	3997.332		:	:	:	:	:	:
20:14:06	3557.354	3830.674		:	:	:	:	:	:
20:15:06	3714.861	4004.346		:	:	:	:	:	:
20:16:06	3620.39	3857.153		:	:	:	:	:	:
20:17:06	3643.444	3886.207		:	:	:	:	:	:
20:18:06	3605.41	3902.047		:	:	:	:	:	:
20:19:06	3712.749	3928.857		:	:	:	:	:	:
20:20:06	3742.865	4109.281		:	:	:	:	:	:
20:21:06	3776.126	3971.901		:	:	:	:	:	:
20:22:06	3790.215	3971.828		:	:	:	:	:	:
20:23:06	3709.615	3980.841		:	:	:	:	:	:
20:24:06	3706.063	3903.103		:	:	:	:	:	:
20:25:06	3633.346	3840.364		:	:	:	:	:	:
20:26:06	3513.443	3749.316		:	:	:	:	:	:
20:27:06	3479.935	3670.18		:	:	:	:	:	:
20:28:06	3474.626	3781.054		:	:	:	:	:	:
20:29:06	3529.363	3734.221		:	:	:	:	:	:
20:30:06	3546.61	3827.716		:	:	:	:	:	:

CALIBRATION SUMMARY
06-17-1992 10:14:00
CALIBRATION FILE NAME =C:\CENDATA\0617A.CAL

=====								
Chan.	Name	Units	Zero		Span		Slope	Int.
			Conc.	Resp.	Conc.	Resp.		
=====								
1	THC1	PPM	0.00	-0.0046	3980.00	3.980	998.022	4.55
2	O2	%	0.00	0.0004	20.90	0.005	247.868	-0.11
3	THC2	PPM	0.00	-0.0011	3980.00	3.966	1003.200	1.12
4		PPM	0.00	0.0000	0.00	0.000	1.000	0.00
=====								

Site 2
Day 1

Press Shift-PrtSc to Print Out Table
Press (C) to Continue

CEM INSTRUMENT DRIFT SUMMARY
06-17-1992 10:14:23

=====								
Chan.	Name	Units	Zero Conc.		Span		Drift % of Scale	
			(Actual	Observed)	(Actual	Observed)	Zero	Span
=====								
1	THC1	PPM	0.000	%-3.844	3980.00	4000.88	-0.04	0.11
2	O2	%	0.000	0.160	20.90	0.00	0.64	-83.60
3	THC2	PPM	0.000	%-1.426	3980.00	3977.52	-0.01	-0.02
4		PPM	0.000	0.000	0.00	0.00	0.00	0.00
=====								

Press Shift-PrtSc to Print Out Table
Press (C) to Continue

Field Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
BAKERIES
.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 10:17:12

File Name = C:\CEM\DATA\261792.PRN Calibration File: C:\CEM\DATA\0617A.CAL

Time	<u>Table</u>		<u>Rack</u>	
	THC1 PPM	O2 %	THC2 PPM	FPM
=====				
10:17:22	3936.7	0.1	2017.6	-3.7
10:18:28	3241.9	0.1	2998.2	-3.7
10:19:28	3241.9	0.1	2998.2	-3.7
10:19:29	3241.9	0.1	2998.2	-3.7
10:19:42	1525.9	-0.1	1531.0	-3.7
10:19:42	1518.3	0.2	1518.6	-3.7
10:19:42	1518.1	0.1	1512.3	-3.7
10:19:42	1512.8	0.3	1510.4	-3.7
10:20:22	1510.3	0.0	1511.8	-3.7
10:20:22	1511.3	0.1	1509.7	-3.7
10:20:42	1518.2	0.2	1518.9	-3.7
10:21:02	1516.7	0.1	1522.5	-3.7
10:21:22	1509.5	0.2	1509.5	-3.7
10:21:42	1509.5	0.1	1475.7	-3.7
10:22:02	1228.5	0.2	921.9	-3.7
10:22:22	824.2	0.5	820.1	-3.7
10:22:42	818.5	0.0	813.6	-3.7
10:23:02	814.1	0.0	814.0	-3.7
10:23:22	813.6	0.0	815.5	-3.7
10:23:42	813.4	-0.0	813.2	-3.7
10:24:02	812.9	0.0	813.6	-3.7
10:24:22	812.4	0.0	814.7	-3.7
10:24:42	812.3	0.0	813.9	-3.7
10:25:02	811.8	-0.0	814.6	-3.7
10:25:22	811.4	0.0	803.1	-3.7
10:25:42	591.8	0.1	598.5	-3.7
10:26:02	221.1	1.0	213.7	-3.7
10:26:22	217.8	10.0	217.8	-3.7
10:26:42	213.5	10.0	219.2	-3.7
10:27:02	213.1	21.0	219.5	-3.7
10:27:22	213.5	21.4	215.7	-3.7
10:27:42	213.3	21.4	217.3	-3.7
10:28:02	213.8	21.5	218.3	-3.7
10:28:22	213.6	21.0	217.0	-3.7
=====				
Avg. =	1146.0	4.3	1155.6	-3.7
=====				

1490 ac

THC 2
1514.2

THC 1
1512.6

798 ac

814.2

812.9

199.1 ac

217.6

213.6

RADIAN CORPORATION SPAN 1983

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

94SERIES

JPA

Performed for:

Date Printed = 06-17-1991 Current Loc = 10:30:35

File Name = C:\CEM\DATA\1017-01.PPC Calibration File: C:\CEM\DATA\1017A.LAM

06-17-1991	CHC1	CHC2		
Time	PPM	PPM	PPM	PPM

10:30:35	3979.6	0.1	3985.7	-3.7
10:30:42	3978.9	0.2	4032.1	-3.7
10:31:02	3979.2	0.1	3986.7	-3.7
10:31:22	3982.0	0.1	4008.5	-3.7
10:31:42	3979.4	0.1	4025.6	-3.7
10:32:02	3978.8	0.2	4002.7	-3.7
10:32:12	3976.3	0.1	3982.2	-3.7
10:32:22	3977.9	0.1	4013.1	-3.7
10:32:32	3975.6	0.1	4063.4	-3.7
10:32:42	3979.5	0.1	4035.8	-3.7
10:32:52	3979.9	0.2	4016.1	-3.7
10:33:02	3981.2	0.0	4047.5	-3.7
10:33:12	3975.5	0.2	4011.0	-3.0
10:33:22	3982.8	0.2	4006.9	-3.7

Avg. =	3979.6	0.1	4013.4	-3.7
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Channel 3
on Gas going bad
Volts jumping
will re-cal.
6/17

CALIBRATION SUMMARY
 06-17-1992 10:37:50
 CALIBRATION FILE NAME =C:\CEMDATA\26172.CAL

=====							
Chan.	Name	Units	Zero		Span		Int.
			Conc.	Resp.	Conc.	Resp.	
=====							
1	THC1	PPM	0.00	-0.0046	3980.00	3.979	999.006
2	O2	%	0.00	0.0004	20.90	0.005	247.898
3	THC2	PPM	0.00	-0.0011	3980.00	3.880	1025.571
4		PPM	0.00	0.0000	0.00	0.000	1.000
=====							

Press Shift-Print to Print Out Table
 Press (C) to Continue

DEM INSTRUMENT DRIFT SUMMARY
 06-17-1992 10:37:59

=====							
Chan.	Name	Units	Zero Conc.		Span		Drift % of Scale
			(Actual	Observed)	(Actual	Observed)	
=====							
1	THC1	PPM	0.000	0.000	3980.00	3979.27	0.00
2	O2	%	0.000	0.000	20.90	2.00	-83.60
3	THC2	PPM	0.000	0.000	3980.00	3893.49	0.00
4		PPM	0.000	0.000	0.00	0.00	0.00
=====							

END

RADIAN CORPORATION span 1990

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 10:40:54

File Name = D:\CEM\DATA\061792.PRN Calibration File: C:\CEM\DATA\0617B.CAL

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM
10:41:06	4000.7	0.2	4091.9	-3.8
10:41:10	3986.3	0.3	4104.9	-3.8
10:41:29	3980.9	0.1	4110.0	-3.7
10:41:30	3983.6	0.2	4126.5	-4.1
10:41:40	3978.5	0.1	4104.8	-3.7
10:41:50	3981.7	0.2	4107.0	-3.7
10:42:00	3980.2	0.1	4090.8	-3.7
10:42:10	3976.2	0.1	4113.2	-3.7
10:42:20	3977.7	0.1	4082.2	-3.7
10:42:30	3980.0	0.1	4100.0	-3.7
10:42:40	3979.3	0.1	4103.1	-3.7
10:42:50	3982.7	0.1	4131.3	-3.7
10:43:00	3982.9	0.1	4116.4	-3.7
10:43:10	3983.9	0.0	4117.4	-3.7
10:43:20	3979.9	0.1	4124.1	-3.7
10:43:30	3981.6	0.1	4054.1	-3.7
10:43:40	3982.6	0.0	4128.4	-3.7
10:43:50	3982.8	0.0	4120.7	-3.7
10:44:00	3971.1	0.3	532.4	-3.7
10:44:10	3973.5	0.3	-278.1	-3.7
10:44:20	3976.2	0.0	2478.2	-3.7
10:44:30	3975.2	0.1	4108.2	-3.7
10:44:40	3974.3	0.2	4108.6	-3.7
10:44:50	3980.5	0.1	4093.7	-3.7

=====
Avg. = 3980.6 0.1 3707.2 -3.7
=====

Ch 3 failing

CALIBRATION SUMMARY
06-17-1992 10:56:13
CALIBRATION FILE NAME =C:\CEM\DATA\06170.CAL

=====								
Chan.	Name	Units	Zero		Span		Slope	Int.
			Conc. Resp.		Conc. Resp.			
=====								
1	THC1	PPM	0.00	-0.0046	3980.00	3.979	999.006	4.55
2	O2	%	0.00	0.0004	20.90	0.005	247.888	-0.11
3	THC2	PPM	0.00	-0.0011	3980.00	3.772	1054.814	1.18
4		PPM	0.00	0.0000	0.00	0.000	1.000	0.00
=====								

Press Shift-PrtSc to Print Out Table
Press <C> to Continue

RADIAN CORPORATION RUN01.DL

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 13:08:42

File Name = C:\CEM\DATA\061792.FRN Calibration File: C:\CEM\DATA\0617D.CAL

06-17-1992 THC1 O2 THC2
Time PPM % PPM PPM

1997 m

13:08:42	218.8	19.1	-3413.8	206.3
13:08:49	216.3	19.2	-5235.8	205.1
13:08:59	216.2	19.3	-5236.8	204.8
13:09:09	216.5	19.3	-5246.8	203.1
13:09:19	215.3	19.4	-5238.8	204.6
13:09:29	214.6	19.4	-5238.5	205.2
13:09:39	214.4	19.4	-5238.3	205.1
13:09:49	215.1	19.4	-5234.8	205.5

Avg. = 215.9 19.3 -4592.5 204.9

Field Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
BAKERIES

.PR
Performed for:
Date Printed = 06-17-1992 Current Time = 13:15:51
File Name = C:\CEM\DATA\061792.PRN Calibration File: C:\CEM\DATA\06170.CAL

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM
=====				
13:15:52	807.0	-0.5	-3977.9	749.4
13:15:59	807.8	-0.3	-4484.1	740.7
13:16:09	808.7	-0.5	-4039.3	751.0
13:16:19	806.6	-0.5	-4000.5	740.5
13:16:29	807.2	-0.5	-4028.4	745.8
13:16:39	806.6	-0.5	-4024.6	759.4
13:16:49	807.6	-0.3	-3988.6	751.0
13:16:59	808.8	-0.5	-3988.2	751.9
13:17:09	807.8	-0.5	-3988.5	758.2
13:17:19	808.0	-0.4	-4055.1	746.6
13:17:29	807.8	-0.4	-4047.2	742.8
13:17:39	806.3	-0.4	-4046.4	747.2
13:17:49	806.0	-0.4	-3927.2	1800.7
=====				
Avg. =	807.6	-0.5	-4044.9	744.4
=====				
=====				

748.6

RADIAN CORPORATION RUN01 GD 1490

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

JPA

Performed for:

Date Printed = 06-17-1992 Current Time = 13:19:13

File Name = C:\CEM\DATA\061792.FRN Calibration File: C:\CEM\DATA\06170.CAL

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM

13:19:13	1281.1	2.2	-2242.6	1426.7
13:19:14	1281.1	2.2	-2242.6	1426.7
13:19:14	1281.1	2.2	-2242.6	1426.7
13:19:14	1281.1	2.2	-2242.6	1426.7
13:19:19	1496.9	-0.2	-1754.9	1436.2
13:19:34	1494.9	-0.1	-1832.4	1437.8
13:19:49	1492.1	0.2	-971.6	1446.9
13:20:04	1497.7	0.1	-1857.4	1429.6
13:20:19	1498.3	-0.0	-1137.8	1435.1
13:20:34	1498.7	-2.1	-1817.1	1432.2
13:20:49	1496.9	0.0	-1847.4	1432.9

Avg. =	1418.2	0.8	-1557.1	1436.7
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1496.5

1436.4

RADIAN CORPORATION RUN QC 3980

Field Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 13:21:59

File Name = C:\CEM\DATA\061792.PRN Calibration File=C:\CEM\DATA\06170.CAL

TWC₁ = FRONT
TWC₂ = REAR
ppm =

06-17-1992	1901	02	1902	
Time	PPM	%	PPM	PPM

13:22:00	1488.7	0.4	-988.4	1427.8
13:22:04	3681.2	2.4	-1363.4	3683.0
13:22:19	3839.4	1.2	-320.4	3745.0
13:22:34	3913.5	0.4	-98.1	3783.1
13:22:49	3936.4	-0.1	-282.5	3647.3
13:23:04	3935.5	0.1	-100.2	3780.2
13:23:19	3939.9	0.1	-16.7	3756.2
13:23:34	3935.8	-0.0	-19.6	3763.7
13:23:49	3935.0	0.1	596.4	3734.5
13:24:04	3938.1	0.5	745.5	3851.9
13:24:19	3943.5	-0.6	1080.1	3764.8
13:24:34	3942.9	0.1	1378.2	3793.8
13:24:49	3942.1	-0.0	1448.7	3777.8
13:25:04	3943.1	0.1	1468.6	3783.1
13:25:19	3945.9	-0.1	1606.0	3771.7
13:25:34	3943.6	0.0	1655.0	3953.2

3980
QC

Span Adj.

Avg. =	3753.0	0.3	427.4	3653.9
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3931.7

RADIAN CORPORATION POST RUN RUN GC CHECK

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 16:19:35

File Name = C:\CEM\DATA\061792.PRN Calibration File: C:\CEM\DATA\061792.CAL

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM
16:19:54	9.2	19.7	-3520.5	11.6
16:20:54	8.6	19.6	-3520.0	10.9
16:21:49	868.2	19.7	-3319.8	66.3
16:21:49	868.2	19.7	-3319.8	66.3
16:21:54	1098.2	19.6	-3352.8	64.1
16:22:14	1116.7	19.8	-3147.6	63.4
16:22:34	1136.5	19.8	-3147.6	63.4
16:22:54	1163.0	19.8	-3195.5	60.9
16:23:14	1162.2	19.8	-3174.8	60.9
16:23:34	1195.7	19.8	-3228.5	58.6
16:23:54	1189.3	19.7	-3305.1	47.9
16:24:14	1161.4	19.7	-3332.4	44.5
16:24:34	1173.9	19.7	-3044.0	43.6
16:24:54	1157.1	19.7	-3336.5	43.0
16:25:14	1167.0	19.7	-3312.4	43.2
16:25:34	1161.9	19.7	-3319.6	41.6
16:25:54	1129.6	19.7	-3320.8	40.8
16:26:14	1133.9	19.7	-3312.5	42.0
16:26:34	1101.7	19.7	-3316.7	41.4
16:26:54	1050.4	19.7	-3292.1	42.4

Charlie @ Stack

Confmt Good @ THC!
Line 1

Avg. = 1002.6 19.7 -3289.8 47.8

$\bar{x} = 1113$

ADIAN CORPORATION COMFORT HOOD LINE 2

Field Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 16:35:34

File Name = C:\CEM\DATA\061792.PRN Calibration File: C:\CEM\DATA\060190.CAL

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM

16:39:54	122.8	19.8	-3705.4	56.4
16:40:07	124.0	19.8	-3708.4	57.0
16:40:24	116.4	19.7	-3710.5	57.5

Avg. =	121.1	19.8	-3709.0	56.7
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RADIAN CORPORATION POST TEST QC

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

.PA

Performed for:

Date Printed = 06-17-1992 Current Time = 17:50:41

File Name = C:\CEM\DATA\061792.PRN Calibration File: C:\CEM\DATA\061702.CAL

06-17-1992 Time	THC1 PPM	O2 %	THC2 PPM	PPM
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17:50:43	43.0	19.7	-3315.5	1.5
17:50:43	43.0	19.7	-3315.5	1.5
17:50:49	35.6	19.5	-3452.6	1.5
17:50:59	31.9	19.7	-3218.5	2.7
17:51:09	32.3	19.7	-3388.7	2.2
17:51:19	29.7	19.7	-3421.8	2.7
17:51:29	28.2	19.7	-3316.3	2.8
17:51:39	26.3	19.8	-3291.7	2.5
17:52:09	25.4	19.8	-3345.4	2.8
17:52:39	25.2	19.9	-3276.1	2.8
17:52:57	17.3	19.9	-3364.3	2.9
17:52:59	10.0	19.4	-3432.4	5.0
17:53:09	12.9	20.0	-3333.8	2.1
17:53:19	12.9	20.1	-3333.9	2.0
17:53:29	13.8	20.3	-3444.3	0.7
17:53:39	10.7	19.7	-3329.4	2.5
17:53:49	10.8	19.9	-3369.5	1.6
17:53:59	10.6	19.8	-3359.9	1.2
17:54:09	9.0	19.8	-3333.4	1.6
17:54:19	9.3	19.7	-3425.3	1.6
17:54:29	12.6	19.8	-3376.3	0.5
17:55:29	451.8	19.7	-3816.2	58.2
17:56:12	100.2	19.8	-4029.0	89.1
17:56:12	100.2	19.8	-4029.0	89.1
17:56:14	92.8	19.5	-4277.3	93.4
17:56:29	91.5	19.5	-4133.5	94.5
17:56:44	90.8	19.5	-3985.2	87.4
17:56:59	90.7	19.5	-3968.8	85.8
17:57:14	90.2	19.5	-4013.2	86.6
17:57:29	90.9	19.5	-4032.1	87.8
17:57:44	89.9	19.5	-3990.1	87.2
17:57:59	90.5	19.5	-4009.7	86.3
17:58:14	89.7	19.6	-4011.5	87.9
17:58:29	89.1	19.6	-3952.5	85.6
17:58:44	89.1	19.6	-4016.3	86.5
17:58:59	88.8	19.6	-4025.1	87.0
17:59:14	88.4	19.6	-3980.1	86.9
8:00:11	591.4	19.7	-3893.2	513.4
8:00:11	591.4	19.7	-3893.2	513.4
8:00:14	582.9	19.6	-4402.2	764.1
8:00:34	583.5	19.7	-3703.4	771.4
8:00:54	582.6	19.7	-3692.9	772.1
8:01:14	580.0	19.8	-3698.5	774.5
8:01:34	586.4	19.8	-3678.4	772.4
8:01:54	581.2	19.7	-3691.6	774.0
8:02:14	582.6	19.8	-3839.5	771.1

zero

$T = 11.1$
 $R = 1.5$
 $n = 10$
 $n = 9$

80 ppm

$T = 90.0$
 $R = 86.8$

798 ppm

79806
Cont

06-17-1992	THC1	02	THC2	
Time	PPM	%	PPM	PPM
18:02:34	811.1	19.7	-1692.1	778.2
18:02:44	810.4	19.6	-4226.1	775.2
18:02:54	811.9	19.7	-3780.3	778.4
18:03:04	810.3	19.7	-3705.2	775.8
18:03:14	811.4	19.7	-3702.5	770.1
18:03:24	811.6	19.6	-3728.4	771.4
18:03:34	809.8	19.7	-3744.2	770.3
18:03:44	806.4	19.7	-3741.4	758.5
18:03:54	750.9	19.7	-4285.0	113.4
18:04:04	623.7	19.7	-3771.2	61.7
18:04:14	847.4	19.8	-3876.1	69.3
18:04:24	486.8	19.7	-4483.7	548.0
18:04:34	133.1	19.7	-5195.5	215.1
18:04:44	218.6	19.7	-5188.3	229.8
18:04:54	215.6	19.6	-5197.9	225.3
18:05:04	213.5	19.7	-5217.5	223.5
18:05:14	212.3	19.7	-3731.2	225.3
18:05:24	211.4	19.7	-5185.8	218.6
18:05:34	210.8	19.7	-5211.7	219.4
18:05:44	210.9	19.6	-5207.2	217.8
18:05:54	210.7	19.6	-5211.8	218.0
18:06:04	210.8	19.6	-5214.6	217.2
18:06:14	211.0	19.6	-5217.1	217.1
18:06:24	212.2	19.7	-5221.9	217.2
18:06:34	212.0	19.6	-5235.8	217.7
18:06:44	212.5	19.6	-5236.5	218.2
18:06:54	213.1	19.7	-5197.5	217.8
18:07:04	213.1	19.7	-5197.1	217.7
18:07:14	212.9	19.7	-5199.0	217.4
18:07:24	282.5	19.7	-4677.4	154.9
18:07:34	653.2	19.7	-3777.4	53.4
18:07:44	825.9	19.7	-3756.2	57.5
18:07:54	526.8	19.7	-4339.2	186.5
18:08:04	389.1	19.7	-5186.5	267.3
18:08:14	303.8	19.7	-5159.9	279.3
18:08:24	324.9	19.7	-5182.3	334.3
18:08:34	306.2	19.6	-5192.1	237.7
18:08:44	305.3	19.7	-5183.7	250.1
18:08:54	304.0	19.7	-5173.5	292.2
18:09:04	324.2	19.7	-5182.0	290.8
18:09:14	324.9	19.7	-5173.6	292.7
18:09:24	387.2	19.7	-5174.9	283.2
18:09:34	307.5	19.7	-5174.5	284.3
18:09:44	327.4	19.7	-5180.2	284.4
18:09:54	379.4	19.7	-4730.7	275.8
18:10:04	911.8	19.6	-3982.1	110.1
18:10:14	924.0	19.6	-3209.8	347.5
18:10:24	1126.0	20.1	-1005.5	1501.4
18:10:34	1491.9	20.2	-1006.2	1526.7
18:10:44	1503.8	20.3	-1005.1	1527.7
18:10:54	1505.7	20.3	-1004.3	1523.3
18:11:04	1506.4	20.3	-1001.8	1518.5
18:11:14	1503.9	20.3	-1009.0	1519.0
18:11:24	1503.1	20.3	-1004.7	1523.1
18:11:34	1507.3	20.2	-1003.4	1518.8
18:11:44	1507.6	20.2	-864.1	1522.2

T = 809.7
R = 772.4

199

T = 212.0
R = 217.9

200 detuned

T = 305.9
R = 295.5

1490

T = 1505.1
R = 1524.3

RADIAN CORPORATION COMFORT HOOD

Field Testing and Process Engineering Dept.

Continuous Emissions Monitoring Data

BAKERIES

,PA

Performed for:

Date Printed = 06-17-1992 Current Time = 18:36:44

File Name = C:\CEM\DATA\061792.PRN Calibration File = C:\CEM\DATA\061792.CAL

Inlet

Exhaust

06-17-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM

LINE 2

LINE 1

18:36:45	157.9	19.9	-3671.1	1056.7
18:37:04	144.8	19.8	-3528.6	1026.9
18:37:24	155.2	19.8	-3534.5	1053.1
18:37:44	158.9	19.9	-3552.2	1056.1
18:38:04	147.5	19.9	-3528.5	1060.3
18:38:24	162.8	19.8	-3678.2	1139.5
18:38:44	148.8	19.9	-3623.3	1141.9
18:39:04	146.8	19.8	-3553.0	1062.4
18:39:24	152.0	19.8	-3579.5	1092.9
18:39:44	142.0	19.8	-3571.6	1098.6
18:40:04	155.9	19.8	-3575.6	1094.5
18:40:24	141.3	19.8	-3547.3	1097.5
18:40:44	153.9	19.8	-3543.6	1077.3
18:41:04	153.6	19.8	-3534.6	1032.5
18:41:24	145.4	19.7	-3545.1	1040.5
18:41:44	150.7	19.8	-3549.0	1026.5
18:42:04	141.3	19.8	-3512.1	1057.2
18:42:24	141.8	19.8	-3531.1	1055.5
18:43:04	143.9	19.8	-3561.1	1091.2
18:43:54	139.6	19.8	-3568.6	1084.1

Avg. =	149.2	19.8	-3564.4	1072.3
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06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
10:57:11	4006.787							
10:57:21	3977.121							
10:57:31	3976.694							
10:57:41	3974.307							
10:57:51	3981.442							
10:58:01	3980.657							
10:58:11	3979.615							
10:58:21	3977.827							
10:58:31	3981.71							
10:58:41	3984.747							
10:58:51	3980.237							
10:59:01	3978.998							
10:59:11	3977.921							
10:59:21	3981.13							
10:59:31	3952.94							
10:59:41	3952.204							
10:59:51	3805.703							
11:00:01	2817.113							
11:00:11	2275.551							
11:00:21	1594.169							
11:00:31	1537.706							
11:00:41	1521.905							
11:00:51	1518.286							
11:01:01	1512.359							
11:01:11	1511.693							
11:01:21	1509.81							
11:01:31	1508.906							
11:01:41	1508.282							
11:01:51	1509.852							
11:02:01	1507.443							
11:02:11	1507.615							
11:02:21	1505.522							
11:02:31	1502.224							

MISC.

06-17-1992

SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
11:02:41	1499.428					:			
11:02:51	1508.356					:			
11:03:01	1507.287					:			
11:03:11	1508.181					:			
11:03:21	1505.782					:			
11:03:31	1507.357					:			
11:03:41	1487.182					:			
11:03:51	1301.82					:			
11:04:01	1512.111					:			
11:04:11	1511.207					:			
11:04:21	1501.282					:			
11:04:31	1500.557					:			
11:04:41	1514.969					:			
11:04:51	1509.369					:			
11:05:01	1506.611					:			
11:05:11	1504.148					:			
06-17-1992THC1						:			
TIME	PPM					:			
11:14:29	4015.029					:			
11:14:39	3979.846					:			
11:14:49	3974.238					:			
11:14:59	3972.744					:			
11:15:09	3975.31					:			
11:15:19	3969.643					:			
11:15:29	3969.032					:			
11:15:39	3978.644					:			
11:15:49	3976.934					:			
11:15:59	3975.507					:			
11:16:09	3973.393					:			
11:16:19	3968.319					:			
11:16:29	3969.144					:			
11:16:39	3964.912					:			
11:16:56	3951.24					:			

[illegible]

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
11:27:59	10.49756							
11:28:09	10.87808							
11:28:19	10.45465							
11:28:29	9.672779							
11:28:39	9.875825							
11:28:49	9.733643							
11:28:59	9.560152							
11:29:09	8.699469							
11:29:19	8.691087							
11:29:29	7.716141							
11:29:39	7.061555							
11:29:49	8.185887							
11:29:59	6.220094							
11:30:09	6.698687							
11:30:19	6.610427							
11:30:29	7.459379							
11:30:39	6.967408							
11:30:49	7.023473							

TIME	FRONT	REAR	SAMPLE	ETH-OH B (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)
11:30:59	5.980845						
11:31:09	6.10041						
11:31:19	6.521301						
11:31:29	5.810229						
11:31:39	5.624887						
11:31:49	4.990615						
=====							
11:32:49	1042.862	29.39402					
11:33:49	1414.083	34.2084		1062		0.83	37.8
11:34:49	1490.96	34.50138					
11:35:49	1467.786	36.12374					
11:36:49	1491.193	37.23773					
11:37:49	1542.576	36.77304					

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
11:38:49	1530.38	36.57618						
11:39:49	1550.659	35.67297						
11:40:49	1588.506	41.74496						
11:41:49	1611.51	65.52142						
11:42:49	1636.956	69.7119						
11:43:49	1661.46	70.95698						
11:44:49	1612.144	72.72072						
11:45:49	1647.274	69.27358						
11:46:49	1597.756	63.67231						
11:47:49	1556.852	40.36945						
11:48:49	1524.049	41.1626						
11:49:49	1534.923	37.51579						
11:50:49	1563.872	40.54655						
11:51:49	1573.515	38.26907						
11:52:49	1647.053	36.60846						
11:53:49	1624.323	36.0976						
11:54:49	1580.709	37.9423						
11:55:49	1594.424	55.01956						
11:56:49	1681.554	75.47709						
11:57:49	1664.469	75.89907						
11:58:49	1700.236	78.98765						
11:59:49	1751.779	65.71471						
12:00:49	1666.432	50.95728						
12:01:49	1650.976	45.96999						
12:02:49	1664.422	45.84506						
12:03:49	1656.515	42.98654						
12:04:49	1652.378	44.52901						
12:05:49	1628.099	51.4452						
12:06:49	1696.77	78.58185						
12:07:49	1761.214	80.85557						
12:08:49	1697.731	80.99433						
12:09:49	1749.408	80.71996						
12:10:49	1686.202	81.80733						

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
12:11:49	1613.438	77.44265						
12:12:49	1619.937	73.33865						
12:13:49	1616.101	72.79445						
12:14:49	1635.107	70.9634						
12:15:49	1637.347	70.18611						
12:16:49	1573.965	69.50216						
12:17:49	1510.245	100.6866						
12:18:49								
12:19:49								
12:20:49	1158.068	33.7184						
12:21:49	1269.681	29.86975						
12:22:49	1087.291	29.84524						
12:23:49	1001.511	32.66129						
12:24:49	891.5979	33.73835						
12:25:49	922.9741	56.84198						
12:26:49	1146.596	56.32072						
12:27:19	1292.044	36.27996						
12:27:49	1300.143	35.64198						
12:28:19	1397.836	36.00331						
12:28:49	1536.229	34.91889						
12:29:19	1652.659	36.18098						
12:29:49	1808.089	35.74922						
12:30:19	1706.216	35.50997						
12:30:49	1713.329	38.99809						
12:31:19	1739.357	37.03702						
12:31:49	1789.889	42.13118						
12:32:19	1757.148	43.24084						
12:32:49	1762.063	43.39158						
12:33:19	1776.11	41.46397						
12:33:49	1770.028	41.51437						
12:34:19	1877	40.69119						
12:34:49	1852.557	42.40943						
12:35:19	1808.696	29.30888						

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
12:35:49	1834.508	29.24157	:	:	:	:	:	:
12:36:19	1834.365	28.81687	:	:	:	:	:	:
12:36:49	1868.067	34.14518	:	:	:	:	:	:
12:37:19	1841.417	38.55045	:	:	:	:	:	:
12:37:49	1864.824	34.212	:	:	:	:	:	:
12:38:19	1873.072	40.68833	:	:	:	:	:	:
12:38:49	1863.624	48.67173	:	:	:	:	:	:
12:39:19	1863.452	74.06374	:	:	:	:	:	:
12:39:49	1957.54	80.45522	:	:	:	:	:	:
12:40:19	1957.951	79.95548	:	:	:	:	:	:
12:40:49	1903.973	77.71337	:	:	:	:	:	:
12:41:19	1902.655	81.13132	:	:	:	:	:	:
12:41:49	1916.533	81.78783	:	:	:	:	:	:
12:42:19	1864.176	83.52328	:	:	:	:	:	:
12:42:49	1846.994	81.81888	:	:	:	:	:	:
12:43:19	1889.343	80.8882	:	:	:	:	:	:
12:43:49	1866.011	81.30882	:	:	:	:	:	:
12:44:19	1798.043	80.08022	:	:	:	:	:	:
12:44:49	1813.955	59.53167	:	:	:	:	:	:
12:45:19	1688.348	45.43704	:	:	:	:	:	:
12:45:49	1641.001	44.92567	:	:	:	:	:	:
12:46:19	1694.681	43.06486	:	:	:	:	:	:
12:46:49	1669.407	43.48089	:	:	:	:	:	:
12:47:19	1644.064	42.60461	:	:	:	:	:	:
12:47:49	1662.349	42.48032	:	:	:	:	:	:
12:48:19	1605.49	42.30225	:	:	:	:	:	:
12:48:49	1633.577	44.61112	:	:	:	:	:	:
12:49:19	1615.895	45.01712	:	:	:	:	:	:
12:49:49	1576.208	45.00491	:	:	:	:	:	:
12:50:19	1421.196	45.11719	:	:	:	:	:	:
12:50:49	1562.22	42.55563	:	:	:	:	:	:
12:51:19	1632.059	43.13315	:	:	:	:	:	:
12:51:49	1602.228	43.80753	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
12:52:19	1562.783	41.91368						
12:52:49	1621.381	45.7454						
12:53:19	1634.258	43.03591						
12:53:49	1692.989	44.4625						
12:54:19	1698.29	50.17965						
12:54:49	1747.649	72.49113						
12:55:19	1753.669	76.70416						
12:55:49	1734.983	77.0721						
12:56:19	1776.372	75.18401						
12:56:49	1714.169	74.23149						
12:57:19	1747.235	75.5872						
12:57:49	1745.876	64.36565						
12:58:19	1675.333	48.44009						
12:58:49	1659.554	46.06833						
12:59:19	1641.468	44.52185						
12:59:49	1628.246	47.10246						
AVG	1637.485	52.72272						

END

13:00:49	1072.789	106.5716						
13:01:17	282.3601	4.611707						
13:01:29	38.62205	1.354882						
13:01:41	30.26346	1.621442						
13:01:49	25.50085	1.958055						
13:01:59	24.25096	1.892638						
13:02:09	23.42955	1.496656						
13:02:19	21.61629	1.836668						
13:02:29	19.22695	0.198332						
13:02:39	14.41056	-0.29192						
13:02:49	12.76342	-0.32870						
13:02:59	16.8141	-0.37501						
13:03:09	16.98508	-0.14182						

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
13:03:19	15.86139	-0.30809						
13:03:29	15.84753	-0.24275						
13:03:39	14.51408	0.851424						
13:03:49	15.56318	0.021666						
13:03:59	15.35984	0.444235						
13:04:09	16.17255	0.113692						
13:04:19	15.53276	0.291238						
13:04:29	15.19018	0.111067						
13:04:39	14.82277	0.082561						
13:04:49	14.2579	0.235488						
13:04:59	15.09802	-0.44925						
13:05:09	14.35928	0.020306						
13:05:19	14.57484	-0.32083						
13:05:29	12.82906	0.374176						
13:05:39	13.97013	0.379317						
13:05:49	13.6896	0.017300						
13:05:59	13.22921	0.599770						
13:06:09	13.42063	0.072418						
13:06:19	12.5994	-0.38563						
13:06:29	12.81038	172.6367						
13:06:39	402.4097	1465.793						
13:06:49	1400.726	1687.946						
13:06:59	1531.328	1796.088						
13:07:09	1554.078	1732.053						
13:07:19	1538.207	1154.425						
13:07:29	824.5981	211.3669						
13:08:29	223.942	208.5792						
13:08:30	223.942	208.5792						
13:08:30	223.942	208.5792						
13:08:30	223.942	208.5792						
13:08:30	223.942	208.5792						
13:08:31	223.942	208.5792						
13:08:42	218.7821	205.959						

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TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
13:08:49	216.3355	205.0622	:	:	:	:	:	:
13:08:59	216.1746	204.7546	:	:	:	:	:	:
13:09:09	216.547	203.1341	:	:	:	:	:	:
13:09:19	215.2818	204.6445	:	:	:	:	:	:
13:09:29	214.5812	205.2296	:	:	:	:	:	:
13:09:39	214.4425	205.1376	:	:	:	:	:	:
13:09:49	215.0672	205.5353	:	:	:	:	:	:
13:09:59	216.0106	203.7748	:	:	:	:	:	:
13:10:09	215.0372	203.8692	:	:	:	:	:	:
13:10:19	213.6133	204.998	:	:	:	:	:	:
13:10:29	215.0381	761.8077	:	:	:	:	:	:
13:10:39	817.0169	1788.709	:	:	:	:	:	:
13:10:49	1494.925	1582.247	:	:	:	:	:	:
13:10:59	1061.797	612.0588	:	:	:	:	:	:
13:11:09	685.4975	756.6094	:	:	:	:	:	:
13:11:19	810.3105	748.8432	:	:	:	:	:	:
13:11:29	811.4909	754.0825	:	:	:	:	:	:
13:11:39	812.136	742.6591	:	:	:	:	:	:
13:11:49	809.4355	755.2709	:	:	:	:	:	:
13:11:59	808.6151	747.1154	:	:	:	:	:	:
13:12:09	809.965	756.6021	:	:	:	:	:	:
13:12:19	809.8234	755.682	:	:	:	:	:	:
13:12:29	808.2613	749.6115	:	:	:	:	:	:
13:12:39	809.1453	742.5555	:	:	:	:	:	:
13:12:49	808.2839	755.3231	:	:	:	:	:	:
13:12:59	809.0898	754.0073	:	:	:	:	:	:
13:13:09	809.238	753.9104	:	:	:	:	:	:
13:13:19	809.549	744.633	:	:	:	:	:	:
13:13:29	808.321	744.2004	:	:	:	:	:	:
13:13:39	807.9456	747.2714	:	:	:	:	:	:
13:13:49	808.0755	749.3724	:	:	:	:	:	:
13:13:59	809.1729	742.0062	:	:	:	:	:	:
13:14:09	808.2324	748.2204	:	:	:	:	:	:

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SITE

SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS				
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	
13:14:19	808.1719	742.8021								
13:14:29	809.2661	753.649								
13:14:39	808.2669	750.0101								
13:14:49	807.4323	745.1548								
13:14:59	808.0364	755.2931								
13:15:09	808.5294	750.7493								
13:15:19	809.2736	747.8971								
13:15:29	808.2723	741.7552								
13:15:39	808.11	753.6313								
13:15:52	807.0104	749.3977								
13:15:59	809.8135	740.678								
13:16:09	808.7317	750.9661								
13:16:19	806.644	740.8857								
13:16:29	807.1852	745.824								
13:16:39	806.6326	759.382								
13:16:49	807.6148	751.0069								
13:16:59	808.7731	751.8873								
13:17:09	807.7873	756.1888								
13:17:19	807.9649	746.6207								
13:17:29	807.8412	742.8358								
13:17:39	806.2531	747.2026								
13:17:49	805.9938	1083.749								
13:18:04	1070.609	1362.208								
13:19:13	1281.085	1426.665								
13:19:14	1281.085	1426.665								
13:19:14	1281.085	1426.665								
13:19:14	1281.085	1426.665								
13:19:19	1496.898	1438.248								
13:19:34	1494.909	1437.828								
13:19:49	1492.088	1446.875								
13:20:04	1497.71	1429.649								
13:20:19	1498.253	1435.072								
13:20:34	1498.681	1432.16								

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
13:20:49	1496.928	1432.925	:	:	:	:	:	:
13:21:04	1496.061	1432.879	:	:	:	:	:	:
13:21:19	1496.137	1440.514	:	:	:	:	:	:
13:21:34	1493.764	1475.058	:	:	:	:	:	:
13:22:00	1488.718	1627.75	:	:	:	:	:	:
13:22:04	3681.247	3682.987	:	:	:	:	:	:
13:22:19	3839.446	3744.976	:	:	:	:	:	:
13:22:34	3913.467	3753.074	:	:	:	:	:	:
13:22:49	3936.354	3647.274	:	:	:	:	:	:
13:23:04	3935.5	3779.954	:	:	:	:	:	:
13:23:19	3939.92	3738.185	:	:	:	:	:	:
13:23:34	3935.843	3763.705	:	:	:	:	:	:
13:23:49	3934.979	3734.453	:	:	:	:	:	:
13:24:04	3938.135	3851.859	:	:	:	:	:	:
13:24:19	3943.537	3764.824	:	:	:	:	:	:
13:24:34	3942.899	3793.844	:	:	:	:	:	:
13:24:49	3946.111	3777.916	:	:	:	:	:	:
13:25:04	3943.141	3933.164	:	:	:	:	:	:
13:25:19	3945.885	3914.658	:	:	:	:	:	:
13:25:34	3943.561	3953.16	:	:	:	:	:	:
13:25:49	3946.077	3989.677	:	:	:	:	:	:
13:26:04	3933.916	3902.166	:	:	:	:	:	:
13:26:19	3637.206	2722.059	:	:	:	:	:	:
13:26:34	1724.214	1913.377	:	:	:	:	:	:
13:26:49	2138.66	1868.196	:	:	:	:	:	:
13:27:04	849.0496	45.26967	:	:	:	:	:	:
13:27:19	51.63179	18.06028	:	:	:	:	:	:
13:27:34	30.3059	12.72092	:	:	:	:	:	:
13:27:49	19.3924	8.976061	:	:	:	:	:	:
13:28:04	16.29148	5.43848	:	:	:	:	:	:
13:28:19	16.31548	4.563832	:	:	:	:	:	:
13:28:34	15.2391	3.743904	:	:	:	:	:	:
13:28:49	15.21998	3.163213	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
13:29:04	14.25889	2.22843	:	:	:	:	:	:
13:29:19	13.65504	2.701864	:	:	:	:	:	:
13:29:34	42.40237	876.3954	:	:	:	:	:	:
13:29:51	1823.81	3570.031	:	:	:	:	:	:
13:30:04	3768.705	3938.388	:	:	:	:	:	:
13:30:19	3881.112	3977.051	:	:	:	:	:	:
13:30:34	3917.367	3880.529	:	:	:	:	:	:
13:30:44	3933.202	3797.622	:	:	:	:	:	:
13:30:54	3937.292	3973.919	:	:	:	:	:	:
13:31:04	3940.816	3981.042	:	:	:	:	:	:
13:31:14	3942.771	4028.609	:	:	:	:	:	:
13:31:24	3941.266	4014.005	:	:	:	:	:	:
13:31:34	3945.452	3975.444	:	:	:	:	:	:
13:31:44	3943.696	3995.422	:	:	:	:	:	:
13:31:54	3937.354	3980.492	:	:	:	:	:	:
13:32:04	3943.143	3970.279	:	:	:	:	:	:
13:32:14	3944.708	3977.403	:	:	:	:	:	:
13:32:24	3944.19	3992.738	:	:	:	:	:	:
13:32:34	3945.426	3918.706	:	:	:	:	:	:
13:32:44	3934.099	3974.394	:	:	:	:	:	:
13:32:54	3929.99	3175.2	:	:	:	:	:	:
13:33:04	2569.345	1822.362	:	:	:	:	:	:
13:33:14	1458.469	1736.481	:	:	:	:	:	:
13:33:24	1354.819	1706.639	:	:	:	:	:	:
13:33:34	1347.781	1598.977	:	:	:	:	:	:
13:33:44	1327.669	1686.198	:	:	:	:	:	:
13:33:54	1338.955	1676.6	:	:	:	:	:	:
13:34:04	1334.68	2290.777	:	:	:	:	:	:
13:34:14	2300.811	620.881	:	:	:	:	:	:
13:34:24	478.123	117.4856	:	:	:	:	:	:
13:34:34	68.84455	38.61887	:	:	:	:	:	:
13:34:44	40.31632	17.11532	:	:	:	:	:	:
13:34:54	28.00314	12.65847	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
13:35:04	20.1203	9.743205	:	:	:	:	:	:
13:35:14	16.69067	7.573807	:	:	:	:	:	:
13:35:24	14.56262	6.153206	:	:	:	:	:	:
13:35:34	14.29635	6.835116	:	:	:	:	:	:
13:35:44	15.06107	5.977743	:	:	:	:	:	:
13:35:54	15.90812	5.412708	:	:	:	:	:	:
13:36:04	15.93148	5.311615	:	:	:	:	:	:
13:36:14	15.26119	3.82786	:	:	:	:	:	:
13:36:24	15.04067	5.157952	:	:	:	:	:	:
13:36:34	13.99906	3.453489	:	:	:	:	:	:
13:36:44	13.80126	4.063683	:	:	:	:	:	:
13:36:54	12.63249	4.792696	:	:	:	:	:	:
13:37:04	13.62309	3.714633	:	:	:	:	:	:
13:37:14	13.26846	3.249627	:	:	:	:	:	:
13:37:24	13.00579	4.594259	:	:	:	:	:	:
13:37:34	13.34566	2.458976	:	:	:	:	:	:
13:37:44	13.00905	3.261137	:	:	:	:	:	:
13:37:54	13.34089	2.941173	:	:	:	:	:	:
13:38:04	11.67922	4.514632	:	:	:	:	:	:
13:38:14	11.50085	3.879251	:	:	:	:	:	:
13:38:24	11.65623	2.844111	:	:	:	:	:	:
13:38:34	12.51189	2.40731	:	:	:	:	:	:
13:38:44	11.67494	3.200307	:	:	:	:	:	:
13:38:54	11.40698	2.314573	:	:	:	:	:	:
13:39:04	11.82771	2.306038	:	:	:	:	:	:
13:39:14	10.86656	3.157882	:	:	:	:	:	:
13:39:24	10.82043	1.897912	:	:	:	:	:	:
13:39:34	12.08174	2.467547	:	:	:	:	:	:
13:39:44	10.79829	2.245547	:	:	:	:	:	:
13:39:54	11.75324	2.741355	:	:	:	:	:	:
13:40:04	11.80704	1.853957	:	:	:	:	:	:
13:40:14	11.76955	2.388265	:	:	:	:	:	:
13:40:24	11.38982	1.403385	:	:	:	:	:	:

SITE 2 DAY 1

[illegible]

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
13:45:54	1498.176	1738.782	:	:	:	:	:	:
13:46:24	1468.369	1824.056	:	:	:	:	:	:
13:46:54	1470.537	1787.481	:	:	:	:	:	:
13:47:24	1499.821	1847.601	:	:	:	:	:	:
13:47:54	1514.652	1824.698	:	:	:	:	:	:
13:48:24	1529.859	1868.041	:	:	:	:	:	:
13:48:54	1596.799	1906.222	:	:	:	:	:	:
13:49:24	1630.094	1989.972	:	:	:	:	:	:
13:49:54	1655.305	1995.272	:	:	:	:	:	:
13:50:24	1653.863	2011.29	:	:	:	:	:	:
13:50:54	1635.043	2008.084	:	:	:	:	:	:
13:51:24	1613.896	1945.691	:	:	:	:	:	:
13:51:54	1566.765	1928.987	:	:	:	:	:	:
13:52:24	1528.744	1867.114	:	:	:	:	:	:
13:52:54	1497.478	1867.001	:	:	:	:	:	:
13:53:24	1470.607	1844.323	:	:	:	:	:	:
13:53:54	1453.932	1790.143	:	:	:	:	:	:
13:54:24	1444.795	1801.988	:	:	:	:	:	:
13:54:54	1462.873	1798.872	:	:	:	:	:	:
13:55:24	1482.424	1816.351	:	:	:	:	:	:
13:55:54	1492.202	1857.168	:	:	:	:	:	:
13:56:24	1512.002	1843.527	:	:	:	:	:	:
13:56:54	1518.74	1884.95	:	:	:	:	:	:
13:57:24	1479.597	1861.286	:	:	:	:	:	:
13:57:54	1516.528	1911.841	:	:	:	:	:	:
13:58:24	1519.228	1887.949	:	:	:	:	:	:
13:58:54	1524.397	1786.054	:	:	:	:	:	:
13:59:24	1559.621	1889.219	:	:	:	:	:	:
13:59:54	1591.812	1892.059	:	:	:	:	:	:
14:00:24	1620.811	1955.562	:	:	:	:	:	:
14:00:54	1596.347	1972.384	:	:	:	:	:	:
14:01:24	1600.427	1897.322	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
14:01:54	1568.983	1920.725	:	:	:	:	:	:
14:02:24	1542.168	1870.965	:	:	:	:	:	:
14:02:54	1506.259	1900.614	:	:	:	:	:	:
14:03:24	1467.428	1834.266	:	:	:	:	:	:
14:03:54	1464.683	1826.099	:	:	:	:	:	:
14:04:24	1471.005	1807.578	:	:	:	:	:	:
14:04:54	1477.453	1852.803	:	:	:	:	:	:
14:05:24	1495.213	1837.678	:	:	:	:	:	:
14:05:54	1505.493	1858.564	:	:	:	:	:	:
14:06:24	1514.355	1882.239	:	:	:	:	:	:
14:06:54	1462.606	1886.319	:	:	:	:	:	:
14:07:24	1498.267	1890.771	:	:	:	:	:	:
14:07:54	1491.844	1819.174	:	:	:	:	:	:
14:08:24	1450.248	1807.849	:	:	:	:	:	:
14:08:54	1430.411	1751.656	:	:	:	:	:	:
14:09:24	1407.669	1745.4	:	:	:	:	:	:
14:09:54	1401.985	1702.092	:	:	:	:	:	:
14:10:24	1417.509	1758.928	:	:	:	:	:	:
14:10:54	1396.024	1738.783	:	:	:	:	:	:
14:11:24	1411.958	1779.602	:	:	:	:	:	:
14:11:54	1426.392	1769.164	:	:	:	:	:	:
14:12:24	1438.677	1802.907	:	:	:	:	:	:
14:12:54	1471.542	1798.487	:	:	:	:	:	:
14:13:24	1482.016	1852.046	:	:	:	:	:	:
14:13:54	1504.002	1843.727	:	:	:	:	:	:
14:14:24	1495.474	1867.456	:	:	:	:	:	:
14:14:54	1483.998	1889.34	:	:	:	:	:	:
14:15:24	1519.258	1886.684	:	:	:	:	:	:
14:15:54	1493.88	1832.592	:	:	:	:	:	:
14:16:24	1462.557	1849.599	:	:	:	:	:	:
14:16:54	1434.156	1835.734	:	:	:	:	:	:
14:17:24	1394.371	1760.42	:	:	:	:	:	:
14:17:54	1409.201	1749.214	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)		
=====											
14:18:24	1394.167	1790.111	:	:	:	:	:	:	:	:	:
14:18:54	1386.25	1784.531	:	:	:	:	:	:	:	:	:
14:19:24	1359.699	1800.776	:	:	:	:	:	:	:	:	:
14:19:54	1401.104	1805.312	:	:	:	:	:	:	:	:	:
=====											
END											
14:20:24	1398.587	1760.885	:	:	:	:	:	:	:	:	:
14:20:54	1284.451	1721.861	:	:	:	:	:	:	:	:	:
14:21:24	1246.386	1679.437	:	:	:	:	:	:	:	:	:
14:21:54	1164.479	1548.691	:	:	:	:	:	:	:	:	:
14:22:24	1070.532	1448.444	:	:	:	:	:	:	:	:	:
14:22:54	962.4634	1294.997	:	:	:	:	:	:	:	:	:
14:23:24	851.8221	1143.297	:	:	:	:	:	:	:	:	:
14:23:54	755.832	1073.673	:	:	:	:	:	:	:	:	:
14:24:24	652.3893	892.5518	:	:	:	:	:	:	:	:	:
14:24:54	547.0892	714.1482	:	:	:	:	:	:	:	:	:
14:25:24	444.4109	619.4125	:	:	:	:	:	:	:	:	:
14:25:54	359.7599	507.0153	:	:	:	:	:	:	:	:	:
=====											
14:26:24	343.4171	421.0565	:	:	:	:	:	:	:	:	:
14:26:54	321.3966	358.4365	:	:	:	:	:	:	:	:	:
14:27:24	304.2171	339.4913	:	:	:	:	:	:	:	:	:
14:27:54	276.8226	363.6198	:	:	:	:	:	:	:	:	:
14:28:24	302.9322	395.0788	:	:	:	:	:	:	:	:	:
14:28:54	332.8347	417.2093	:	:	:	:	:	:	:	:	:
14:29:24	809.7207	1196.402	:	:	:	:	:	:	:	:	:
14:29:54	1486.797	1512.008	:	:	:	:	:	:	:	:	:
14:30:24	1496.252	1516.834	:	:	:	:	:	:	:	:	:
14:30:54	1496.097	1517.026	:	:	:	:	:	:	:	:	:
14:31:24	922.5669	728.6716	:	:	:	:	:	:	:	:	:
14:31:54	461.1092	367.3189	:	:	:	:	:	:	:	:	:
14:32:24	100.614	97.01382	:	:	:	:	:	:	:	:	:
14:32:54	93.14729	94.8696	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
			=====	=====	=====	=====	=====	=====
14:33:24	92.15985	92.89659	:	:	:	:	:	:
14:33:54	91.29941	94.00833	:	:	:	:	:	:
14:34:24	90.84695	91.73769	:	:	:	:	:	:
14:34:54	91.07748	91.84176	:	:	:	:	:	:
14:35:24	90.26055	103.591	:	:	:	:	:	:
14:35:54	199.5354	307.3006	:	:	:	:	:	:
14:36:24	224.3799	331.3313	:	:	:	:	:	:
14:36:54	245.1053	317.3661	:	:	:	:	:	:
14:37:24	307.887	322.108	:	:	:	:	:	:
14:37:54	335.2946	286.8743	:	:	:	:	:	:
14:38:24	106.1937	92.10699	:	:	:	:	:	:
14:38:54	90.6982	89.12624	:	:	:	:	:	:
14:39:24	89.66865	88.67318	:	:	:	:	:	:
14:39:54	90.43441	87.36819	:	:	:	:	:	:
14:40:24	90.05202	87.46663	:	:	:	:	:	:
14:40:54	90.33366	87.21962	:	:	:	:	:	:
14:41:24	89.73172	86.7821	:	:	:	:	:	:
14:41:54	89.27991	87.4389	:	:	:	:	:	:
14:42:24	88.9601	87.33456	:	:	:	:	:	:
14:42:54	89.11683	86.84642	:	:	:	:	:	:
14:43:24	89.13927	86.60008	:	:	:	:	:	:
14:44:54	88.81143	88.24014	:	:	:	:	:	:
14:46:29	88.9012	85.85589	:	:	:	:	:	:
14:46:54	1288.568	1575.159	:	:	:	:	:	:
14:47:54	1263.575	1537.521	:	:	:	:	:	:
14:48:54	1226.518	1539.094	:	:	:	:	:	:
14:49:54	1159.257	1455.683	:	:	:	:	:	:
14:50:54	970.9083	1295.791	:	:	:	:	:	:
14:51:54	837.5342	974.6697	:	:	:	:	:	:
14:52:54	249.2764	140.7001	:	:	:	:	:	:
14:53:54	92.81011	92.66132	:	:	:	:	:	:
14:54:54	90.90134	89.80783	:	:	:	:	:	:
14:55:54	89.92567	89.68206	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (rack) (ppmC)	THC2 (ppmC)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
14:55:54	89.92567	89.68206								
14:56:54	90.05106	88.20906								
14:57:54	89.63951	87.32652								
14:58:54	89.4286	88.90255								
14:59:54	89.88869	86.48393								
15:00:54	89.12128	86.54823								
15:01:54	88.26274	87.16266								
15:02:54	89.05706	87.06765								
15:03:54	1055.023	1508.498								
15:04:54	1397.954	1672.288								
15:05:54	1363.926	1661.862								
15:06:54	1333.971	1608.121								
15:07:54	402.9993	282.3545								
15:08:54	92.7411	93.20146								
15:09:54	89.32776	91.6059								
15:10:54	88.79375	89.35266								
15:11:54	87.37488	93.18111								
15:12:54	87.13413	88.84309								
15:13:54	87.07554	87.62646								

TIME	THC1 (table) (rack) (ppmC)	THC2 (ppmC)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
15:14:54	285.0155	532.0817								
15:15:54	1404.113	1771.647								
15:17:30	1416.601	1778.153								
15:17:54	1428.192	1812.909								
15:18:54	1423.691	1775.462								
15:19:54	1402.024	1784.082								
15:20:54	1413.664	1784.641								
15:21:54	1375.417	1744.135								
15:22:54	1358.179	1673.483								
15:23:54	1350.488	1720.186								

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
15:24:54	1378.793	1698.703									
15:25:54	1366.097	1675.724									
15:26:54	1405.218	1679.154									
15:27:54	1438.836	1763.352									
15:28:54	1469.473	1825.116									
15:29:54	1465.053	1819.024									
15:30:54	1452.781	1793.624									
15:31:54	1405.127	1767.034									
15:32:54	1370.62	1723.394									
15:33:54	1330.265	1655.804									
15:34:54	1287.856	1566.841									
15:35:54	1277.234	1590.61									
15:36:54	1310.633	1611.664	1300	3.54	12.4	53.2					
15:37:54	1322.584	1650.985									
15:38:54	1332.347	1656.38									
15:39:54	1321.793	1627.787									
15:40:54	1354.828	1648.912									
15:41:54	1404.149	1709.055									
15:42:54	1441.513	1763.321									
15:43:54	1463.174	1798.086									
15:44:54	1464.582	1799.121									
15:45:54	1475.71	1818.093									
15:46:54	1487.983	1818.065									
15:47:54	1485.072	1822.491									
15:48:54	1478.01	1808.728									
15:49:54	1453.904	1779.305									
15:50:54	1417.298	1725.495									
15:51:54	1422.289	1720.507									
15:52:54	1440.221	1753.525									
15:53:54	1453.292	1790.34									
15:54:54	1459.595	1801.318	1530	4.72	19	65.1					
15:55:54	1422.238	1810.917									
15:56:54	1436.818	1783.678									

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS				
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
=====										
15:57:54	1412.919	1754.319								
15:58:54	1390.117	1695.102								
15:59:54	1366.504	1712.997								
16:00:54	1348.811	1711.587								
16:01:54	1282.987	1616.375								
16:02:54	1207.58	1479.693								
16:03:54	1166.149	1417.805								
16:04:54	1215.733	1459.032								
16:05:54	1296.454	1585.31								
16:06:54	1368.024	1682.653								
16:07:54	1405.239	1689.202								
16:08:54	1412.548	1711.444								
16:09:54	1441.753	1716.317								
16:10:54	1482.461	1782.653								
16:11:54	1486.058	1807.33								
16:12:54	1473.795	1802.784								
16:13:54	1483.602	1792.884								
16:14:54	1487.113	1820.681								
16:15:54	1501.439	1843.867								
AVG	1398.312	1724.309								

END

LINE 1	FRONT			ACETALDEHYDE:		
	ETH-OH	CH4	C2H6	ETH-OH	CH4	C2H6
16:16:54	409.3594	224.7001				
16:18:02	17.68003	19.79696				
16:18:54	9.648371	13.98247				
16:19:54	9.202121	11.57869				
16:20:54	8.594005	10.88564				
16:21:49	868.1973	66.27567				
16:21:49	868.1973	66.27567				
16:21:54	1098.197	64.1273				

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[illegible]

16:22:14	1116.72	63.42145			
16:22:34	1135.547	63.36816			
16:22:54	1163.007	60.8689			
16:23:14	1162.203	60.91985			
16:23:34	1195.674	58.83215			
16:23:54	1189.272	47.93451			
16:24:14	1161.423	44.46025			
16:24:34	1173.901	43.62891			
16:24:54	1157.113	43.04488			
16:25:14	1166.983	43.18311			
16:25:34	1161.916	41.58257			
16:25:54	1129.57	39.97136			
16:26:14	1133.87	42.03884			
AVG	1157.476				

END

16:26:34	1101.719	41.44409	•
16:26:54	1050.395	42.37951	•
16:27:54	388.6343	13.47557	•
16:28:54	11.65843	7.039453	•
16:29:54	9.161827	6.068379	•
16:30:54	13.72197	25.33464	•
16:31:54	13.92983	60.50518	•
16:32:54	10.7202	62.38114	•
16:33:54	46.484	59.74147	•
16:34:54	108.5433	53.33368	•
16:35:54	105.5316	40.75153	•
16:36:54	107.7621	39.33812	•
16:37:54	99.75694	39.85096	•

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS	REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
16:38:54	117.0285	40.823	=====	=====	=====	=====

FRONT	FRONT GC RESULTS		
ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
=====	=====	=====	=====

SAMPLE

16:39:54	122.7671	55.44074	:
16:40:09	124.0163	56.98098	:
16:40:24	116.3763	57.53741	:
16:40:39	125.3041	60.82921	:
16:40:54	120.6612	58.0351	:
16:41:09	113.3846	57.70606	:
16:41:24	125.4202	58.18852	:
16:41:39	121.7216	58.34017	:
16:41:54	116.602	57.59104	:
16:42:09	120.49	57.82325	:
16:42:24	123.0352	57.83029	:
16:42:39	119.8497	58.48083	:
16:42:54	113.63	58.01651	:

16:43:09	125.9713	56.30906	:
16:43:24	123.8972	51.82061	:
120.8751			

END

16:43:39	102.6479	45.89133	:
16:43:54	316.2871	40.55352	:
16:44:09	677.5265	37.96023	:
16:44:24	629.6259	37.94843	:
16:44:39	530.7304	37.46262	:
16:44:54	681.8949	37.23357	:
16:45:09	687.6758	37.14516	:
16:45:24	554.2975	38.57404	:
16:45:39	663.685	40.23904	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (ppmC)	FRONT GC RESULTS				REAR GC RESULTS				
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
16:45:54	681.6486	39.47442				:					
16:46:38	661.835	37.72398				:					
16:46:39	661.835	37.72398				:					
16:46:39	694.0729	37.60699				:					
16:47:09	599.2235	39.93898				:					
16:47:39	46.70284										
			FRONT								
	FRONT	REAR	LITE RYE	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
			BREAD SAM=====								
16:48:09	626.0633	56.25227				:		85.7	2.02	0.53	4.63
16:48:39	650.7016	57.9347				:					
16:49:09	714.9216	59.46802				:					
16:49:39	637.5718	58.52269				:					
16:50:09	728.5926	57.4615				:					
16:50:39	649.2714	57.65371				:					
16:51:09	655.7234	57.68335				:					
16:51:39	688.1528	56.86594				:					
16:52:09	646.9548	52.72595				:					
16:52:39	665.9782	38.20032				:					
16:53:09	621.0528	38.02177				:					
16:53:39	595.2332	37.14312				:					
16:54:09	639.9388	37.90045				:					
16:54:39	564.2653	38.64099				:					
16:55:09	601.3074	38.07462				:					
16:55:39	595.1424	35.65527				:					
16:56:09	607.806	43.18403				:					
16:56:39	680.974	55.45557				:					
16:57:09	631.114	59.30193				:					
16:57:39	683.6387	59.48767				:					
16:58:09	660.5897	60.27737				:					
16:58:39	625.8167	57.68938				:					
16:59:09	699.8243	58.32999				:					

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS				
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
=====										
16:59:39	638.6313	59.07639								
17:00:09	699.9559	56.18863								
17:00:39	651.117	40.36681								
17:01:09	632.9659	37.90973								
17:01:39	650.3009	37.10459								
17:02:09	602.4631	37.88645								
17:02:39	665.9803	37.16931								
17:03:09	626.2248	36.09529								
17:03:39	607.6958	38.00441								
17:04:09	685.2701	51.87571								
17:04:39	629.8644	56.62453								
17:05:09	665.3479	57.24641								
17:05:39	670.04	57.40655								
17:06:09	654.3615	57.17914								
17:06:39	731.0815	56.05731						195	3.85	7.24
17:07:09	659.9935	56.66292								
17:07:39	703.5674	56.64257								
17:08:09	678.4631	55.79349								
17:08:39	650.8192	55.69491								
17:09:09	699.4058	43.38015								
17:09:39	623.7826	38.35152								
17:10:09	650.4582	36.74134								
17:10:39	655.4919	38.5859								
17:11:09	621.8656	38.22137								
17:11:39	673.4471	37.19929								
17:12:09	610.4166	37.44302								
17:12:39	607.255	35.7978								
17:13:09	655.9619	34.97104								
17:13:39	611.6173	36.34014								
17:14:09	682.8729	49.20992								
17:14:39	671.8676	55.49044								
17:15:09	646.2017	56.81381								
17:15:39	697.1576	57.32027								
			532	2.34	0.2	17				

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
=====											
17:16:09	637.533	57.4795	:	:	:	:	:	:	:	:	:
17:16:39	711.3087	56.74813	:	:	:	:	:	:	:	:	:
17:17:09	684.1605	57.11704	:	:	:	:	:	:	:	:	:
17:17:39	671.8986	56.84385	:	:	:	:	:	:	:	:	:
17:18:09	717.4572	56.56672	:	:	:	:	:	:	:	:	:
17:18:39	656.9058	55.5421	:	:	:	:	:	:	:	:	:
17:19:09	690.0143	55.62309	:	:	:	:	:	:	:	:	:
17:19:39	654.3862	55.9239	:	:	:	:	:	:	:	:	:
17:20:09	649.9485	47.29885	:	:	:	:	:	:	:	:	:
17:20:39	714.14	38.13419	:	:	:	:	:	:	:	:	:
17:21:09	614.5846	38.69368	:	:	:	:	:	:	:	:	:
17:21:39	666.6631	39.15244	:	:	:	:	:	:	:	:	:
17:22:09	634.5128	38.28349	:	:	:	:	:	:	:	:	:
17:22:39	599.8585	38.41755	:	:	:	:	:	:	:	:	:
17:23:09	660.5477	38.34941	:	:	:	:	:	:	:	:	:
17:23:39	601.2413	37.30553	:	:	:	:	:	:	:	:	:
17:24:09	669.0643	40.1539	:	:	:	:	:	:	:	:	:
17:24:39	620.2026	37.99926	:	:	:	:	:	:	:	:	:
17:25:09	589.0042	38.23737	:	:	:	:	:	:	:	:	:
17:25:39	639.7133	41.25425	:	:	:	:	:	:	:	:	:
17:26:09	609.1461	55.7198	:	:	:	:	:	:	:	:	:
17:26:39	661.7695	59.98919	:	:	:	:	:	:	:	:	:
17:27:09	676.5593	61.36253	:	:	:	:	:	:	:	:	:
17:27:39	643.7954	62.02855	:	:	:	:	:	:	:	:	:
17:28:09	740.913	61.68292	:	:	:	:	:	:	:	:	:
17:28:39	652.6617	60.97591	:	:	:	:	:	:	:	:	:
17:29:09	709.0215	60.7917	:	:	:	:	:	:	:	:	:
17:29:39	615.9484	59.19083	:	:	:	:	:	:	:	:	:
17:30:09	671.0632	58.03281	:	:	:	:	:	:	:	:	:
17:30:39	677.9738	59.165	:	:	:	:	:	:	:	:	:
17:31:09	691.6673	58.34163	:	:	:	:	:	:	:	:	:
17:31:39	776.2803	57.49446	:	:	:	:	:	:	:	:	:
17:32:09	713.0579	56.71746	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
17:32:39	736.8845	43.3849									
17:33:09	698.3229	37.74192									
17:33:39	661.9335	38.03193									
17:34:09	701.2498	37.12423				14					
17:34:39	655.426	38.83276	445	2.54							
17:35:09	690.9017	37.89458									
17:35:39	712.9224	38.39201									
17:36:09	661.9933	38.05943									
17:36:39	758.1708	35.87828									
17:37:09	661.8452	38.77887									
17:37:39	657.7046	52.38836									
17:38:09	712.0613	58.6278									
17:38:39	703.191	60.39643									
17:39:09	770.921	59.84307									
17:39:39	717.7374	60.01898									
17:40:09	722.3938	59.48373									
17:40:39	753.1239	59.34469									
17:41:09	691.03	58.23291									
17:41:39	779.9366	57.04627									
17:42:09	691.3047	48.56146									
17:42:39	705.1227	39.96888									
17:43:09	745.5781	41.13682									
17:43:39	694.8652	49.37172									
17:44:09	777.0125	51.76235									
17:44:39	731.4171	48.05511									
17:45:09	682.5397	39.99825									
17:45:39	715.243	40.70419									
17:46:09	684.2617	39.69753									
17:46:39	756.6442	41.61172									
	669.8078	48.77769									

END

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
=====											
17:47:39	681.9285	55.09089	:	:	:	:	:	:	:	:	:
17:48:44	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:46	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:47	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:47	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:47	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:47	120.3074	2.781838	:	:	:	:	:	:	:	:	:
17:48:49	70.24654	0.661293	:	:	:	:	:	:	:	:	:
17:48:59	67.53784	1.400337	:	:	:	:	:	:	:	:	:
17:49:09	60.99543	1.642246	:	:	:	:	:	:	:	:	:
17:49:19	58.23168	1.560768	:	:	:	:	:	:	:	:	:
17:49:29	57.17003	1.803209	:	:	:	:	:	:	:	:	:
17:49:39	56.04511	1.811643	:	:	:	:	:	:	:	:	:
17:49:49	50.77974	2.011231	:	:	:	:	:	:	:	:	:
17:49:59	48.81985	1.359404	:	:	:	:	:	:	:	:	:
17:50:09	47.34634	1.19302	:	:	:	:	:	:	:	:	:
17:50:19	46.63055	0.979048	:	:	:	:	:	:	:	:	:
17:50:43	43.01279	1.490016	:	:	:	:	:	:	:	:	:
17:50:43	43.01279	1.490016	:	:	:	:	:	:	:	:	:
17:50:49	35.63415	1.465338	:	:	:	:	:	:	:	:	:
17:50:59	31.76541	2.72116	:	:	:	:	:	:	:	:	:
17:51:09	32.25847	2.245968	:	:	:	:	:	:	:	:	:
17:51:19	29.68945	2.347241	:	:	:	:	:	:	:	:	:
17:51:29	28.20407	2.843178	:	:	:	:	:	:	:	:	:
17:51:39	26.78161	2.909467	:	:	:	:	:	:	:	:	:
17:52:09	25.40624	2.842643	:	:	:	:	:	:	:	:	:
17:52:39	25.20817	2.784778	:	:	:	:	:	:	:	:	:
17:52:57	17.29054	2.854283	:	:	:	:	:	:	:	:	:
17:52:59	9.999088	5.03663	:	:	:	:	:	:	:	:	:
17:53:09	12.85792	2.129465	:	:	:	:	:	:	:	:	:
17:53:19	12.8681	2.016967	:	:	:	:	:	:	:	:	:
17:53:29	13.80963	0.670703	:	:	:	:	:	:	:	:	:
17:53:39	10.72025	2.505692	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
17:53:49	10.83876	1.633	:	:	:	:	:	:	:	:	:
17:53:59	10.58895	1.195011	:	:	:	:	:	:	:	:	:
17:54:09	8.986586	1.640349	:	:	:	:	:	:	:	:	:
17:54:19	9.274217	1.57228	:	:	:	:	:	:	:	:	:
17:54:29	10.55985	0.588010	:	:	:	:	:	:	:	:	:
17:55:29	451.8296	58.2103	:	:	:	:	:	:	:	:	:
17:56:12	100.1822	89.05756	:	:	:	:	:	:	:	:	:
17:56:12	100.1822	89.05756	:	:	:	:	:	:	:	:	:
17:56:14	92.8154	93.44112	:	:	:	:	:	:	:	:	:
17:56:29	91.49847	94.46818	:	:	:	:	:	:	:	:	:
17:56:44	90.82996	87.44041	:	:	:	:	:	:	:	:	:
17:56:59	90.71393	85.75755	:	:	:	:	:	:	:	:	:
17:57:14	90.15969	86.60531	:	:	:	:	:	:	:	:	:
17:57:29	90.89558	87.7634	:	:	:	:	:	:	:	:	:
17:57:44	89.88288	87.18627	:	:	:	:	:	:	:	:	:
17:57:59	90.50361	86.27328	:	:	:	:	:	:	:	:	:
17:58:14	89.69139	87.89586	:	:	:	:	:	:	:	:	:
17:58:29	89.10184	85.6153	:	:	:	:	:	:	:	:	:
17:58:44	89.05611	86.53326	:	:	:	:	:	:	:	:	:
17:58:59	88.76582	87.02433	:	:	:	:	:	:	:	:	:
17:59:14	88.42382	86.92744	:	:	:	:	:	:	:	:	:
18:00:11	591.4034	513.3533	:	:	:	:	:	:	:	:	:
18:00:11	591.4034	513.3533	:	:	:	:	:	:	:	:	:
18:00:14	802.8655	764.2047	:	:	:	:	:	:	:	:	:
18:00:34	803.9227	771.3851	:	:	:	:	:	:	:	:	:
18:00:54	810.0183	772.1182	:	:	:	:	:	:	:	:	:
18:01:14	809.9528	774.9047	:	:	:	:	:	:	:	:	:
18:01:34	806.3943	772.4498	:	:	:	:	:	:	:	:	:
18:01:54	803.2319	773.9739	:	:	:	:	:	:	:	:	:
18:02:14	810.6462	772.1833	:	:	:	:	:	:	:	:	:
18:02:34	811.0723	770.2269	:	:	:	:	:	:	:	:	:
18:02:44	810.4399	775.2173	:	:	:	:	:	:	:	:	:
18:02:54	811.9366	770.4066	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS		
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
			=====	=====	=====	=====	=====	=====
18:03:04	810.3356	775.7841	:	:	:	:	:	:
18:03:14	811.3689	770.1296	:	:	:	:	:	:
18:03:24	811.6215	771.4312	:	:	:	:	:	:
18:03:34	809.8089	770.296	:	:	:	:	:	:
18:03:44	806.3568	756.5043	:	:	:	:	:	:
18:03:54	750.8615	113.3816	:	:	:	:	:	:
18:04:04	623.665	61.72632	:	:	:	:	:	:
18:04:14	847.4092	69.30756	:	:	:	:	:	:
18:04:24	456.7684	568.0385	:	:	:	:	:	:
18:04:34	233.0896	235.0568	:	:	:	:	:	:
18:04:44	218.5839	229.7705	:	:	:	:	:	:
18:04:54	215.6121	225.2643	:	:	:	:	:	:
18:05:14	213.5374	223.9262	:	:	:	:	:	:
18:05:34	212.2685	225.3451	:	:	:	:	:	:
18:05:54	211.4104	218.7863	:	:	:	:	:	:
18:06:14	210.8054	218.418	:	:	:	:	:	:
18:06:34	210.7571	217.8315	:	:	:	:	:	:
18:06:54	210.6822	218.0175	:	:	:	:	:	:
18:07:14	210.8186	217.6655	:	:	:	:	:	:
18:07:34	211.5915	217.7046	:	:	:	:	:	:
18:07:54	212.1565	217.2088	:	:	:	:	:	:
18:08:14	211.9785	217.6663	:	:	:	:	:	:
18:08:34	212.496	218.1896	:	:	:	:	:	:
18:08:54	213.0918	217.8068	:	:	:	:	:	:
18:09:14	213.08	217.6725	:	:	:	:	:	:
18:09:34	212.8918	217.4072	:	:	:	:	:	:
18:09:54	282.481	154.9094	:	:	:	:	:	:
18:10:14	853.193	50.38786	:	:	:	:	:	:
18:10:34	825.9102	57.47048	:	:	:	:	:	:
18:10:54	526.7836	186.4901	:	:	:	:	:	:
18:11:14	309.1061	267.2068	:	:	:	:	:	:
18:11:34	303.7529	279.3057	:	:	:	:	:	:
18:11:53	304.8595	284.279	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	
18:12:04	306.1873	287.685	:	:	:	:	:	:	:	:	:
18:12:19	305.3141	290.0695	:	:	:	:	:	:	:	:	:
18:12:34	303.9669	292.2198	:	:	:	:	:	:	:	:	:
18:12:49	304.177	290.7963	:	:	:	:	:	:	:	:	:
18:13:04	304.9	292.7295	:	:	:	:	:	:	:	:	:
18:13:19	307.1524	293.1521	:	:	:	:	:	:	:	:	:
18:13:34	307.5072	294.2939	:	:	:	:	:	:	:	:	:
18:13:49	307.394	294.3651	:	:	:	:	:	:	:	:	:
18:14:04	379.3589	276.7627	:	:	:	:	:	:	:	:	:
18:14:19	911.8297	110.0902	:	:	:	:	:	:	:	:	:
18:14:34	924.0176	347.5446	:	:	:	:	:	:	:	:	:
18:14:49	1125.983	1501.363	:	:	:	:	:	:	:	:	:
18:15:04	1491.935	1520.716	:	:	:	:	:	:	:	:	:
18:15:19	1503.841	1527.747	:	:	:	:	:	:	:	:	:
18:15:34	1505.735	1523.271	:	:	:	:	:	:	:	:	:
18:15:49	1506.401	1518.526	:	:	:	:	:	:	:	:	:
18:16:04	1508.946	1518.036	:	:	:	:	:	:	:	:	:
18:16:19	1508.109	1528.609	:	:	:	:	:	:	:	:	:
18:16:34	1507.276	1518.776	:	:	:	:	:	:	:	:	:
18:16:49	1507.557	1531.973	:	:	:	:	:	:	:	:	:
18:17:04	1506.585	1527.146	:	:	:	:	:	:	:	:	:
18:17:19	1505.945	1529.004	:	:	:	:	:	:	:	:	:
18:17:34	1505.072	1535.301	:	:	:	:	:	:	:	:	:
18:17:49	1505.68	1517.138	:	:	:	:	:	:	:	:	:
18:18:04	1503.496	1519.508	:	:	:	:	:	:	:	:	:
18:18:19	1505.034	1513.673	:	:	:	:	:	:	:	:	:
18:18:34	1406.092	2123.434	:	:	:	:	:	:	:	:	:
18:18:49	3466.067	3805.034	:	:	:	:	:	:	:	:	:
18:19:04	3899.812	3913.922	:	:	:	:	:	:	:	:	:
18:19:19	3946.385	3901.949	:	:	:	:	:	:	:	:	:
18:19:34	3962.67	3896.941	:	:	:	:	:	:	:	:	:
18:19:49	3966.923	3947.726	:	:	:	:	:	:	:	:	:
18:20:04	3968.708	3953.447	:	:	:	:	:	:	:	:	:

[illegible]

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS				REAR GC RESULTS			
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)
18:36:04	154.4772	954.85	FRONT							
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)

18:36:24 137.7674 978.4221

18:36:45 157.9362 1056.665

18:37:04 144.8045 1026.923

18:37:24 155.1883 1053.149

18:37:44 158.9215 1056.118

18:38:04 147.4999 1060.253

18:38:24 162.7742 1139.527

18:38:44 148.7737 1141.887

18:39:04 146.8079 1062.371

18:39:24 151.9991 1092.89

18:39:44 141.9763 1098.642

18:40:04 155.9081 1094.477

18:40:24 141.3086 1097.459

18:40:44 153.9112 1077.32

18:41:04 153.6363 1032.455

18:41:24 145.4254 1040.491

18:41:54 150.7155 1026.461

18:42:24 141.3125 1057.238

18:42:54 141.7647 1055.542

18:43:24 143.8538 1091.152

18:43:54 139.5858 1084.117

18:44:24 150.4721 1064.071

148.7428 1067.619

END

18:44:54 139.649 685.9791

18:45:24 15.14443 30.00577

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
18:45:54	5.178239	15.74595	:	:	:	:	:	:	:	:	:
18:46:24	6.58869	5.870663	:	:	:	:	:	:	:	:	:
18:46:54	6.038541	5.02869	:	:	:	:	:	:	:	:	:
18:47:24	5.989203	3.62267	:	:	:	:	:	:	:	:	:
18:47:54	7.756787	4.213714	:	:	:	:	:	:	:	:	:
18:48:24	12.72295	3.274329	:	:	:	:	:	:	:	:	:
18:48:54	11.26214	3.918955	:	:	:	:	:	:	:	:	:
18:49:24	10.68609	3.90776	:	:	:	:	:	:	:	:	:
18:49:54	12.12356	2.438648	:	:	:	:	:	:	:	:	:
18:50:24	10.49041	10.07376	:	:	:	:	:	:	:	:	:
18:50:54	10.19559	9.417857	:	:	:	:	:	:	:	:	:
18:51:24	9.967722	9.605755	:	:	:	:	:	:	:	:	:
18:51:54	10.12564	8.574289	:	:	:	:	:	:	:	:	:
18:52:24	9.975859	14.97295	:	:	:	:	:	:	:	:	:
18:52:54	9.773214	16.30111	:	:	:	:	:	:	:	:	:
18:53:24	9.553326	15.78343	:	:	:	:	:	:	:	:	:
18:53:54	9.322958	15.94985	:	:	:	:	:	:	:	:	:
18:54:24	9.315223	16.34886	:	:	:	:	:	:	:	:	:
18:54:54	9.114346	16.75189	:	:	:	:	:	:	:	:	:
18:55:24	9.170609	15.81572	:	:	:	:	:	:	:	:	:
18:55:54	8.756022	15.67152	:	:	:	:	:	:	:	:	:
18:56:24	9.023675	15.54117	:	:	:	:	:	:	:	:	:
18:56:54	8.733106	15.57214	:	:	:	:	:	:	:	:	:
18:57:24	8.952236	15.87402	:	:	:	:	:	:	:	:	:
18:57:54	9.628976	14.05409	:	:	:	:	:	:	:	:	:
18:58:24	9.321131	15.03831	:	:	:	:	:	:	:	:	:
18:58:54	9.292872	15.77618	:	:	:	:	:	:	:	:	:
18:59:24	9.343784	17.04217	:	:	:	:	:	:	:	:	:
18:59:54	9.147799	17.60257	:	:	:	:	:	:	:	:	:
19:00:24	9.401756	16.53976	:	:	:	:	:	:	:	:	:
19:00:54	9.049747	16.77811	:	:	:	:	:	:	:	:	:
19:01:24	8.49761	17.52147	:	:	:	:	:	:	:	:	:
19:01:54	8.286475	17.61579	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
19:02:24	8.6824	16.15211	:	:	:	:	:	:	:	:	:
19:02:54	8.343011	16.43673	:	:	:	:	:	:	:	:	:
19:03:24	8.336461	17.20231	:	:	:	:	:	:	:	:	:
19:03:54	8.856558	16.43602	:	:	:	:	:	:	:	:	:
19:04:24	8.293921	16.53472	:	:	:	:	:	:	:	:	:
19:04:54	8.255615	16.65649	:	:	:	:	:	:	:	:	:
19:05:24	7.838336	16.59431	:	:	:	:	:	:	:	:	:
19:05:54	7.574986	15.99384	:	:	:	:	:	:	:	:	:
19:06:24	7.658685	15.68118	:	:	:	:	:	:	:	:	:
19:06:54	7.288548	16.20261	:	:	:	:	:	:	:	:	:
19:07:24	7.891728	14.88964	:	:	:	:	:	:	:	:	:
19:07:54	8.292856	14.33759	:	:	:	:	:	:	:	:	:
19:08:24	7.843221	14.42201	:	:	:	:	:	:	:	:	:
19:08:54	8.176501	15.17377	:	:	:	:	:	:	:	:	:
19:09:24	9.332677	14.00873	:	:	:	:	:	:	:	:	:
19:09:54	8.350463	13.58108	:	:	:	:	:	:	:	:	:
19:10:24	8.688746	14.00756	:	:	:	:	:	:	:	:	:
19:10:54	8.372338	14.35222	:	:	:	:	:	:	:	:	:
19:11:24	7.818894	15.02003	:	:	:	:	:	:	:	:	:
19:11:54	7.459581	14.6134	:	:	:	:	:	:	:	:	:
19:12:24	8.321272	14.25297	:	:	:	:	:	:	:	:	:
19:12:54	7.736739	14.15343	:	:	:	:	:	:	:	:	:
19:13:24	7.072399	16.17689	:	:	:	:	:	:	:	:	:
19:13:54	7.396397	14.86033	:	:	:	:	:	:	:	:	:
19:14:24	7.16125	14.8829	:	:	:	:	:	:	:	:	:
19:14:54	7.245749	15.1684	:	:	:	:	:	:	:	:	:
19:15:24	7.233173	14.97965	:	:	:	:	:	:	:	:	:
19:15:54	6.355327	15.29974	:	:	:	:	:	:	:	:	:
19:16:24	6.475695	14.36567	:	:	:	:	:	:	:	:	:
19:16:54	6.767973	13.76901	:	:	:	:	:	:	:	:	:
19:17:24	124.5934	341.8776	:	:	:	:	:	:	:	:	:
19:17:54	7.241116	13.88786	:	:	:	:	:	:	:	:	:
19:18:24	-205.767	13.10095	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1		THC2 (table) (rack) (ppmC) (ppmC)	FRONT GC RESULTS				REAR GC RESULTS			
	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)
	=====	=====	=====	=====	=====	=====	=====	=====	=====	=====	=====
19:18:54	6.510637	14.37619		:				:			
19:19:24	6.46212	14.78465		:				:			
19:19:54	6.635694	14.83365		:				:			
19:20:24	6.596586	14.60167		:				:			
19:20:54	6.58477	13.14678		:				:			
19:21:24	6.540378	14.07096		:				:			
19:21:54	6.797896	13.90073		:				:			
19:22:24	6.526254	14.50373		:				:			
19:22:54	6.28041	13.77833		:				:			
19:23:24	6.393483	14.11921		:				:			
19:23:54	6.321751	13.88748		:				:			
19:24:24	6.516293	13.88031		:				:			
19:24:54	7.651951	10.1409		:				:			
19:25:24	8.037458	8.36982		:				:			
19:25:54	8.018306	8.292183		:				:			
19:26:24	6.983796	9.67176		:				:			
19:26:54	7.003756	10.03386		:				:			
19:27:24	7.535196	9.4997		:				:			
19:27:54	6.75662	10.28417		:				:			
19:28:24	6.909178	9.355187		:				:			
19:28:54	6.772536	10.24816		:				:			
19:29:24	8.41389	5.326598		:				:			
19:29:54	7.238598	9.126521		:				:			
19:30:24	7.835766	8.78858		:				:			
19:30:54	7.833635	9.23712		:				:			
19:31:24	7.801762	13.14612		:				:			
19:31:54	8.110219	13.00729		:				:			
19:32:24	8.705564	12.0252		:				:			
19:32:54	8.978779	10.62277		:				:			
19:33:24	8.995471	8.357552		:				:			
19:33:54	9.634267	7.13115		:				:			
19:34:24	9.024113	7.612613		:				:			
19:34:54	7.560564	7.748718		:				:			

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
19:35:24	7.561777	6.707781	:	:	:	:	:	:	:	:	:
19:35:54	6.076474	7.383619	:	:	:	:	:	:	:	:	:
19:36:24	4.971339	9.782568	:	:	:	:	:	:	:	:	:
19:36:54	4.126477	13.25467	:	:	:	:	:	:	:	:	:
19:37:24	2.638254	4.314458	:	:	:	:	:	:	:	:	:
19:37:54	1.491814	-5.36082	:	:	:	:	:	:	:	:	:
19:38:24	4.711289	-4.37476	:	:	:	:	:	:	:	:	:
19:38:54	2.98436	-4.53843	:	:	:	:	:	:	:	:	:
19:39:24	2.449214	-5.10511	:	:	:	:	:	:	:	:	:
19:39:54	1.463189	-5.13202	:	:	:	:	:	:	:	:	:
19:40:24	1.530494	-5.37116	:	:	:	:	:	:	:	:	:
19:40:54	1.068961	-5.15135	:	:	:	:	:	:	:	:	:
19:41:24	2.345182	-5.03986	:	:	:	:	:	:	:	:	:
19:41:54	1.350661	-5.27493	:	:	:	:	:	:	:	:	:
19:42:24	1.138724	-5.78354	:	:	:	:	:	:	:	:	:
19:42:54	1.79735	-5.38753	:	:	:	:	:	:	:	:	:
19:43:24	3.355201	-4.32676	:	:	:	:	:	:	:	:	:
19:43:54	2.146829	-5.5355	:	:	:	:	:	:	:	:	:
19:44:24	2.268527	-4.85690	:	:	:	:	:	:	:	:	:
19:44:54	2.525471	-4.95798	:	:	:	:	:	:	:	:	:
19:45:24	3.226761	-5.05443	:	:	:	:	:	:	:	:	:
19:45:54	2.092649	-4.80030	:	:	:	:	:	:	:	:	:
19:46:24	2.433929	-4.85832	:	:	:	:	:	:	:	:	:
19:46:54	2.516906	-4.56825	:	:	:	:	:	:	:	:	:
19:47:24	2.650885	-4.85126	:	:	:	:	:	:	:	:	:
19:47:54	3.772402	-4.32954	:	:	:	:	:	:	:	:	:
19:48:24	2.374555	-5.52757	:	:	:	:	:	:	:	:	:
19:48:54	3.717001	-4.16532	:	:	:	:	:	:	:	:	:
19:49:24	2.238339	-4.75790	:	:	:	:	:	:	:	:	:
19:49:54	2.461461	-4.41048	:	:	:	:	:	:	:	:	:
19:50:24	2.951044	-4.51266	:	:	:	:	:	:	:	:	:
19:50:54	2.659294	-4.32547	:	:	:	:	:	:	:	:	:
19:51:24	1.885306	-4.82469	:	:	:	:	:	:	:	:	:

06-17-1992 SITE 2 DAY 1

TIME	THC1 (table) (ppmC)	THC2 (rack) (ppmC)	FRONT GC RESULTS			REAR GC RESULTS					
			ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE: (ppmV/wet)	ETH-OH (ppmV/wet)	CH4 (ppmV/wet)	C2H6 (ppmV/wet)	ACETALDEHYDE (ppmV/wet)	
			=====	=====	=====	=====	=====	=====	=====	=====	=====
19:51:54	2.348802	-4.97562	:	:	:	:	:	:	:	:	:
19:52:24	0.830407	-5.31980	:	:	:	:	:	:	:	:	:
19:52:54	2.314882	-5.13503	:	:	:	:	:	:	:	:	:
19:53:24	3.360121	-4.25623	:	:	:	:	:	:	:	:	:
19:53:54	2.690171	-4.16376	:	:	:	:	:	:	:	:	:
19:54:24	2.371393	-4.57017	:	:	:	:	:	:	:	:	:
19:54:54	3.300642	-4.44474	:	:	:	:	:	:	:	:	:
19:55:24	2.130274	-5.09518	:	:	:	:	:	:	:	:	:
19:55:54	3.296118	-4.15433	:	:	:	:	:	:	:	:	:
19:56:24	1.727989	-4.89303	:	:	:	:	:	:	:	:	:
19:56:54	2.64618	-4.80947	:	:	:	:	:	:	:	:	:
19:57:24	3.831522	-4.18755	:	:	:	:	:	:	:	:	:
19:57:54	3.805472	-4.19625	:	:	:	:	:	:	:	:	:
19:58:24	3.093501	-4.23947	:	:	:	:	:	:	:	:	:
19:58:54	4.261861	-4.13070	:	:	:	:	:	:	:	:	:
19:59:24	24.38632	-4.51164	:	:	:	:	:	:	:	:	:
19:59:54	0.507401	-7.99708	:	:	:	:	:	:	:	:	:
20:00:24	-2.73937	-6.52642	:	:	:	:	:	:	:	:	:
20:00:54	-1.87291	-10.0269	:	:	:	:	:	:	:	:	:
20:01:24	-2.45613	-7.26911	:	:	:	:	:	:	:	:	:
20:01:54	-2.92930	-5.86568	:	:	:	:	:	:	:	:	:
20:02:24	-2.55187	-6.29291	:	:	:	:	:	:	:	:	:
20:02:54	-1.85876	-7.45107	:	:	:	:	:	:	:	:	:
20:03:24	-0.58284	-5.57371	:	:	:	:	:	:	:	:	:
20:03:54	818.3259	-4.00321	:	:	:	:	:	:	:	:	:
20:04:24	1476.719	-6.67082	:	:	:	:	:	:	:	:	:
20:04:54	1493.446	-1.74835	:	:	:	:	:	:	:	:	:
20:05:24	1497.036	127.8066	:	:	:	:	:	:	:	:	:
20:05:54	1500.67	483.0247	:	:	:	:	:	:	:	:	:
20:06:24	1500.347	136.5479	:	:	:	:	:	:	:	:	:
20:06:54	1500.978	247.4286	:	:	:	:	:	:	:	:	:
20:07:24	1502.73	1457.905	:	:	:	:	:	:	:	:	:
20:07:54	1498.644	3550.698	:	:	:	:	:	:	:	:	:

104105-1000-5010401
 04-12-1997 14:56:13
 CALIBRATION FILE NAME: 5010401.D

=====									
Chem. Name			zero		span		slope		
			Conc.	Resp.	Conc.	Resp.			
=====									
1	THC1	PPH	0.00	-0.0128	2000.00	2.000	992.185		11.95
2	O2	L	0.00	0.0055	20.00	0.005	267.378		-1.74
3	THC2	PPH	0.00	-2.9434	3580.00	3.772	592.620		744.45
4		PPH	0.00	-0.0056	2000.00	2.022	986.491		5.45
=====									

Press Shift-H Esc to Print out Table
 Press <C> to Continue

DEM INSTRUMENT DRIFT SUMMARY
06-18-1992 14:56:49

=====							
Chan.	Name	Units	Zero	Conc.	Span	Drift % of Scale	
			(Actual	Observed)	(Actual	Observed)	Zero
							Span
=====							
1	THC1	PPM	0.000	%-7.485	2000.00	2005.26	-0.07
2	O2	%	0.000	1.523	20.90	0.00	6.09
3	THC2	PPM	0.000	%-3103.583	900.00	0.00	-31.04
4		PPM	0.000	%-5.013	2000.00	2001.72	-0.05
=====							

* Ch3 disabled
Ch4 = THC2

Press Shift-FrtSc to Print Out Table
Press (C) to Continue

LIAM CORPORATION 2419 GC PAS TEST LINE 3 199PPM

At Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
SERIES

formed for:

ie Printed = 06-18-1992 Current Time = 15:30:28

ie Name = C:\CEM\DATA\261892.FRM Calibration File=C:\CEM\DATA\261892.CAL

06-18-1992	THC1	O2	THC2	
me	PPM	%	PPM	PPM

00:46	223.5	20.2	-1089.5	212.7
01:01	211.7	20.2	-1079.3	206.8
01:16	211.0	20.3	-1148.3	209.2
01:31	210.8	20.3	-1159.9	207.1
01:46	208.7	20.3	-1134.9	207.0
02:01	208.3	20.3	-1154.2	205.8
02:16	207.9	20.2	-1065.0	206.8
02:31	208.9	20.3	-1079.3	204.2
02:46	207.4	20.3	-1197.2	204.7

1. =	210.9	20.3	-1053.0	205.8
------	-------	------	---------	-------

209.3

204.3

100% HUMIDIFICATION 90.793

LC Testing and Process Engineering Dept.
Infrared Emissions Monitoring Data
SERIES

Formed for:

Printed = 04-18-1992 Current Time = 15:15:43

Name = C:\CEM\DATA\061892.PRM Calibration File=C:\CEM\DATA\061892.CAL

TIME	THC1 PPM	O2 %	THC2 PPM	PPM
------	-------------	---------	-------------	-----

05:46	781.2	-2.1	-459.3	806.5
05:51	783.1	-2.2	-527.8	821.8
05:56	782.8	-2.0	-353.9	798.2
05:15	782.7	-1.9	-338.5	793.8
05:26	783.3	-2.0	-327.5	803.9

Avg	782.6	-2.0	-401.4	801.9
-----	-------	------	--------	-------

IAA CORPORATION DC 1498

Id Testing and Process Engineering Dept.
Chlorous Emissions Monitoring Data
SERIES

formed for:

= Printed = 06-18-1992 Current Time = 15:08:56

= Name = D:\CENDATA\061892.PRN Calibration File=C:\CENDATA\061892.CAL

-18-1992	THC1	O2	THC2	
TE	PPM	%	PPM	PPM

08:58	1466.3	-1.4	-271.4	1482.5
09:06	1466.4	-1.6	-311.2	1522.3
09:16	1469.6	-1.7	-242.4	1476.2
09:26	1467.5	-1.6	-274.3	1486.6
09:36	1468.3	-1.6	-299.7	1468.9
09:46	1466.4	-1.6	-246.4	1507.1
09:56	1466.5	-1.7	-265.7	1481.2

0.0	1467.5	-1.6	-271.6	1488.9
-----	--------	------	--------	--------

Id Testing and Process Engineering Dept.
 Continuous Emissions Monitoring Data
 SERIES

formed for:

Printed = 06-16-1992 Current Time = 19:15:03

Name = C:\CEMDATA\CONFORT.PRN Calibration File: C:\CEMDATA\0618A.CAL

TIME	THC1 PPM	O2 %	THC2 PPM	PPM
------	-------------	---------	-------------	-----

16:06	171.7	19.8	-667.8	115.5
16:16	168.4	19.8	-617.5	106.4
16:31	157.2	19.8	-593.9	104.3
16:46	156.6	20.0	-545.4	100.2
16:51	161.4	19.9	-636.3	124.6
16:01	156.8	19.9	-579.3	105.5
16:11	164.6	19.9	-547.5	101.0
16:21	184.2	19.8	-536.5	96.5
16:31	185.0	19.9	-526.2	97.1
16:41	162.4	19.8	-564.0	105.2
16:51	147.5	19.9	-531.8	98.0
17:01	140.8	19.8	-533.5	94.7
17:11	142.7	20.0	-399.8	1499.2
17:21	139.9	20.6	1074.2	3922.2
17:31	2428.0	20.8	2010.5	4815.2
17:41	3122.0	20.7	2301.7	4231.5

$T = 159.4$ $n = 14$
 $R = 102.15$ $n = 10$

17:41	486.3	20.0	-117.8	980.6
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MIAMI CORPORATION QC 798

Mo Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
SERIES

Formed for:

Printed = 06-18-1992 Current Time = 19:19:35

File Name = C:\CEM\DATA\CONFORT.PRN Calibration File: C:\CEM\DATA\0618A.CAL

06-18-1992	THC1	O2	THC2	
Time	PPM	%	PPM	PPM

19:38	814.3	19.5	-868.8	757.3
19:41	818.0	19.8	-760.5	765.4
19:54	817.1	19.9	-471.3	757.4
20:01	820.6	19.8	-569.8	759.1
20:11	816.2	19.8	-481.5	758.5
20:21	814.3	19.8	-488.3	756.1
20:31	811.4	19.8	-528.0	753.9
20:41	807.3	19.9	-457.4	754.7
20:51	806.9	19.9	-486.5	751.9
21:01	805.2	19.9	-502.5	751.4
21:11	811.8	19.9	-521.4	749.9
21:21	856.9	19.9	-486.8	758.0

Sum	818.8	19.8	-551.0	754.8
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813.2

Job Name = C:\CEN\DATA\061892.FSH Calibration File=C:\CEN\DATA\061892.CAL

DATE	TIME	BY	TIME	BY	BY
11-18-1952	THO1	02	THO2		
05	PRM	%	PRM	PRM	

17:28	1497.6	18.2	-618.9	1385.3
17:31	1496.9	18.9	-471.5	1390.5
17:46	1492.1	19.9	-236.8	1376.1
18:01	1489.1	18.9	-125.8	1378.2
18:16	1485.4	17.9	-210.3	1373.2
18:31	1483.7	19.8	-195.2	1375.7
18:46	1474.5	17.9	-213.9	1373.2
18:01	1468.7	18.8	-201.9	1371.7
19:16	1477.0	19.9	-236.4	1422.0
19:31	1473.2	19.9	-264.2	1433.8
19:46	1470.8	20.8	-254.4	1431.9
20:01	1473.2	19.9	-259.1	1432.2
20:16	1477.7	20.0	-242.4	1424.5

$T = 1486.1$
 $R = 1428.9$

1. = 1481.1 19.9 -184.8 1396.6

SIAM CORPORATION at 2022 con

old Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
SERIES

1

formed for:

re Printed = 06-19-1992 Current Time = 19:33:35

re Name = C:\CEM\DATA\Q61892.PRN Calibration File:D:\CEM\DATA\Q618A.DAL

6-18-1992	THC1	O2	THC2	
TIME	PPM	%	PPM	PPM
=====				
33:43	2000.8	20.6	1395.4	2022.4
33:43	2000.8	20.6	1395.4	2022.4
33:46	2003.5	20.5	904.1	2014.1
33:56	2004.3	20.5	1312.8	2039.2
34:06	2004.4	20.6	1433.0	2039.4
34:16	2005.1	20.6	1445.8	2035.2
34:26	2005.5	20.6	1451.1	2039.4
34:36	2005.3	20.6	1435.2	2029.4
34:46	2007.2	20.6	1459.7	2034.8
34:56	2009.2	20.6	1461.4	2038.1
35:06	2028.6	20.6	1468.4	2033.8
35:16	2029.2	20.6	1455.8	2038.6
=====				
ave	2008.5	20.6	1376.8	2031.9
=====				

LA CORPORATION 3922 ssm .cc

LA Testing and Process Engineering Dept.
Continuous Emissions Monitoring Data
SERIES

Formed for:

Printed = 06-18-1992 Current Time = 19:42:35

Name = C:\CEMDATA\061892.PRN Calibration File=C:\CEMDATA\0618A.CAL

06-18-1992	THC1	O2	THC2	
18	PPM	%	PPM	PPM

40:36	3843.0	20.7	1629.4	3730.0
40:46	3840.9	20.6	1697.7	3709.9
40:56	3843.6	20.7	1617.0	3692.2
41:06	3872.7	20.7	1702.2	3750.7
41:16	3868.6	20.7	1702.9	3747.1
41:26	3837.6	20.6	1706.2	3720.7
41:36	3838.9	20.6	1710.5	3692.0
41:46	3837.2	20.7	1699.5	3740.3
41:56	3844.5	20.6	1703.0	3719.5
42:06	3839.6	20.6	1696.3	3745.2

42:16	3846.4	20.7	1676.4	3723.7
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Appendix B.3

Method 18 Analytical Summary

SIGNATURE M. D. [Signature]

 DATE 6-17-92

CHECKED _____

DATE _____

 PROJECT STROEMANN BAKERIES

JOB NO. _____

 SUBJECT Initial Calibration 6-17-92

SHEET _____

OF _____

SHEETS

ACETALDEHYDE:

Run#	Conc. (ppm)	AREA	
12	4.43	146,859	
13	8.86	259,823	
14	22.2	680,684	$r = 0.9955$
15	44.3	1,316,867	$m = 35,694$
16	82.5	2,953,533	$b = -85,064$

Ethanol:

Run#	Conc. (ppm)	AREA	
17	249	719,551	
18	498	1,475,122	$r = 0.9996$
19	1000	2,649,477	$m = 2,939$
20	2000	3,111,581 (BROUGHT IN)	$b = -96,53$
21	4000	11,776,876	

METHANE:

Run#	Conc. (ppm)	AREA	
24	80.2	3,109,558	$r = 0.9985$
25	199.1	7,840,528	$m = 29.53$
26	798	24,739,728	$b = 1,298,323$
27	1490 mg		

SIGNATURE M.D. [Signature] DATE 7-16-92 CHECKED _____ DATE _____

 PROJECT STROEHMANN BATTERIES JOB NO. _____

 SUBJECT 6-17-92 DATA REVIEW BUN OVEN SHEET _____ OF _____ SHEETS

RUN #	TIME	LOCATION	METHANE AREA/CONC.	Acetylene AREA/CONC.	Ethanol AREA/CONC.	METHANE
53	15:16:59	FRONT	1,139,122	1,948,856	4,270,717	305,388
54	15:26:10	REAR	17.1	62.5	1,490	4.82
54	15:26:50	REAR	927,232	1,558,866	3,432,185	263,266
			13.9	50.1	1,200	3.76
55	15:35:50	FRONT	830,736	1,656,815	3,731,862	254,716
			12.4	53.2	1,300	3.54
56	15:45:10	REAR	990,225	1,554,421	3,579,010	276,721
			14.8	49.9	1,250	4.10
57	15:54:30	FRONT	1,263,331	2,028,970	4,384,624	301,288
			19.0	65.1	1,530	4.72
58	16:03:50	REAR	597,619	1,194,742	3,203,726	216,130
				38.5	1,120	2.57
59	16:12:55	FRONT	1,121,578	1,954,586	4,385,379	302,400
			8.80	59.5	1,530	4.75
X X X X X X X						
60	16:24:15	COMFORT MOOD LINE # 59	396,137	824,318	2,983,765	185,776
			5.70	26.6	1,041	1.80

CALC. NO. _____

SIGNATURE

DATE _____

CHECKED

DATE _____

PROJECT

JOB NO.**SUBJECT**

SHEET

OF

-SHEETS

RUN #	TIME	METHANE AREA/ CONC.	Ethane AREA/ CONC.	Acetaldehyde AREA/ CONC.	Ethanol AREA/ CONC.
61 REAR	16:24:15 16:47:30	136,082 2.02	60,283 0.53	135,340 4.63	224,729 85.7
62 FRONT	16:56:30	152,985 2.28	39,659 0.21	524,631 17.1	1,567,012 550
63 REAR	17:05:55	258,943 3.85	216,947 7.24	216,947 7.24	540,835 195
64 FRONT	17:14:55	157,163 2.34	39,049 0.20	522,435 17.0	1,513,280 532
65 REAR	17:24:30	116,636 1.73	69,248 0.67	134,431 4.60	259,520 97.8
66 FRONT	17:30:51	170,653 2.54	—	427,778 14.6	1,263,085 445
67 REAR	17:42:50	131,807 1.96	64,200 0.59	149,448 4.96	310,582 115

SIGNATURE M.D. [Signature] DATE 6-17-92 CHECKED _____ DATE _____

 PROJECT STROEMANN BAKERIES JOB NO. _____

 SUBJECT FINAL CALIBRATION 6-17-92 SHEET _____ OF _____ SHEETS

METHANE :

Run #	Conc. (ppm)	AREA	
82	4.88	328,098	
80	9.76	475,650	$r = 0.9996$
77	20.05	941,458	$m = 39,584$
78	40.1	1,657,864	$b = 114,525$
79	80.2	3,304,614	

ACETALDEHYDE :

Run #	Conc. (ppm)	AREA	
83	1.52	55,751	$r = 0.9995$
84	3.03	97,849	$m = 31,319$
85	22.2	679,161	$b = -9,749$
86	44.3	1,323,395	
87	82.5	2,604,157	

Ethanol :

Run #	Conc. (ppm)	AREA	w% Run 88	
88	50.0	273,178	$r = 0.9999$	$r = 0.9999$
89	200	531,901	$m = 2.889$	$m = 2.873$
90	498	1,440,916	$b = -22,998$	$b = 34,149$
91	4000	11,531,848		

Ethane :

Run #	Conc. (ppm)	AREA	
80	10.0	676,559	$r = 0.9999$
81	2.5	189,242	$m = 64,952$
82	5.0	349,262	$b = 25,917$

SIGNATURE M.D. [Signature] DATE 7-16-92 CHECKED _____ DATE _____
 PROJECT STROEMMANN BAKERIES JOB NO. _____
 SUBJECT 6-18-92 DATA REVIEW SHEET _____ OF _____ SHEETS

Initial Calibration:

① METHANE

Run#	Conc. (ppm)	AREA	
103	4.88	312,128	$r = 0.9997$
104	9.76	448,572	$m = 39,708$
105	16.0	778,136	$b = 107,818$
106	40.2	1,706,462	
107	80.2	3,287,250	

② ACETALDEHYDE

Run#	Conc. (ppm)	AREA	
98	1.52	54,941	$r = 0.9995$
99	3.03	103,854	$m = 30,822$
100	22.2	706,527	$b = 2886$
101	44.3	1,310,965	
102	82.5	2,157,938	

③ Ethanol

Run#	Conc. (ppm)	AREA	
95	200	570,838	$r = 0.9996$
96	498	1,692,831	$m = 2,710$
97	4000	11,009,464	$b = 179,380$

SIGNATURE M.D. [Signature] DATE 7-16-92 CHECKED _____ DATE _____

 PROJECT STROEMANN Bunkers JOB NO. _____

 SUBJECT DATA REVIEW 6-18-92 SHEET _____ OF _____ SHEETS

RUN #	TIME	LOCATION	METHANE AREA / CONC.	Acetaldehyde AREA / CONC.	Ethanol AREA / CONC.
108	15:54:40	REAR	33,009,696 1980	2,419,269 78.4	4,815,984 1710
109	16:03:35	FRONT	25,472,032 826	3,842,582 125	9,104,762 3,290
110	16:12:26	REAR	31,711,728 1,550	2,529,998 82.0	4,922,352 1,750
111	16:21:25	FRONT	18,889,344 491	3,014,845 97.7	8,038,707 2,900
112	16:30:35	REAR	32,819,856 1970	2,412,774 78.2	5,110,506 1,820
113	16:49:28	REAR	7,119,914 185	589,026 19.0	4,461,712 1,580
117	17:22:56	REAR	33,276,128 1990	2,230,645 72.3	3,499,568 1,220
120	17:53:15	REAR	34,161,344 2050	2,786,022 74.3	3,954,416 1,390
121	18:04:20	REAR	33,956,192 2030	2,057,213 66.7	4,182,096 1,480
124	18:23:55	FRONT	28,875,520 1411	2,820,514 91.4	7,128,048 2,590
125	18:33:35	REAR	32,698,928 1960	2,372,341 76.9	4,680,170 1,660
126	18:42:35	FRONT	31,509,840 1540	4,042,120 131	6,648,192 2,390
127	18:52:08	REAR	32,361,392 1940	2,573,670 83.4	5,203,461 1,850
128	19:01:20	FRONT	27,168,160 1330	3,148,768 102	7,882,832 2,840
129	19:10:45	REAR	35,205,024 2110	2,665,440 86.4	5,732,659 2,050

SIGNATURE M.D. [Signature]

 DATE 7-16-92

CALC. NO. _____

 PROJECT STROHMANN BAKERY

CHECKED _____

DATE _____

 SUBJECT DATA REVIEW
6-18-92

JOB NO. _____

SHEET _____

OF _____

SHEETS

FINAL CAL. CURVE

ACETALDEHYDE :

Run #	Conc. (ppm)	AREA	
138	1.52	50,685	
139	3.03	103,392	
140	22.2	643,299	$r = 0.9999$
141	44.3	1,283,107	$m = 28,932$
142	82.5	2,398,866	$b = 7370$

Ethanol :

Run #	Conc. (ppm)	AREA	
143	249	702,080	$r = 0.9999$
144	498	1,414,304	$m = 2707$
145	4000	10,874,024	$b = 46,384$

METHANE :

Run #	Conc. (ppm)	AREA	
146	9.76	441,687	$r = 0.9986$
147	40.1	1,699,683	$m = 38,463$
148	80.2	3,241,046	$b = 16,685$
149	199.1	7,103,085	
150	399	15,605,400	

OFF SCALE SINGLE PT METHANE

Run #	Conc. (ppm)	AREA
151	798	24,621,344
152	1490	30,487,504
152	2000	33,375,424
153	3980	39,522,496

Appendix B.4

Method 18 Chromatogram

SITE # 02

STROEHMANN BAKERY
NORRISTOWN, PA

6-16-92 to 6-18-92

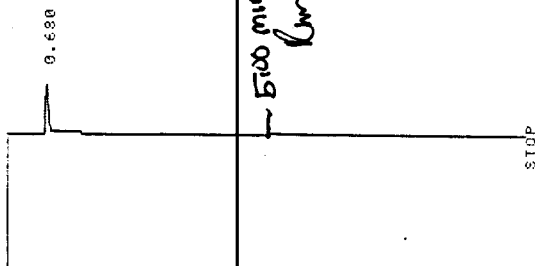
Column (40 psi) = 20 m/min
H₂ (20 psi) = 30 m/min
Air (30 psi) = 400 m/min

* LIST: LIST
PEAK CAPACITY: 1244

ZERO = 5. -3.782
ATT 2 = 6
CHT SP = 1.0
AR REJ = 10000
THRESH = 4
PK WD = 0.10

* RUN # 1 JUN 16, 1992 14:51:32
START

HAILEY AIR BLANK
LOOP & CHECK



RUN# 1 JUN 16, 1992 14:51:32

AREA%
RT AREA TYPE WIDTH AREA%
.680 115442 FB .062 100.00000

TOTAL AREA= 115442
MUL FACTOR=1.0000E+00

START

0.390
0.665

9.460

TIME/TABLE STOP

RUN# 2 JUN 16. 1992 15:09:45

AREA:

RT	AREA	TYPE	WIDTH	AREA%
.390	20403	BV	.042	.81330
.665	36264	PV	.053	1.47628
9.460	2433144	I BH	.445	97.70445

TOTAL AREA=2490310

MUL FACTOR=1.0000E+00

HEAD RE SOURCE TO 60 PSI

* RUN # 3 JUN 16. 1992 15:23:56

START

0.379

1.964

STOP 3

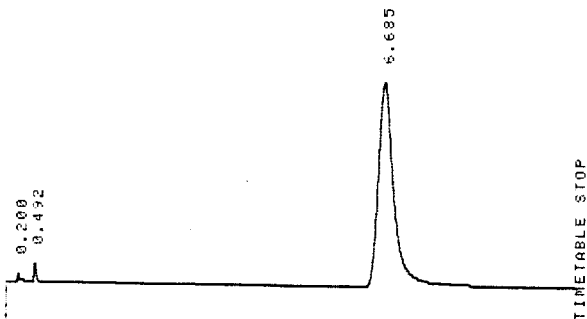
RUN# 3 JUN 16. 1992 15:23:56

RT	AREA	TYPE	WIDTH	AREA%
0.200	14224	BB	.033	.05820
0.492	2426912	SHB	.143	99.94179

TOTAL AREA=2.4441E+07
MUL FACTOR=1.0000E+00

* RUN # 4 JUN 16, 1992 15:32:56
START

4.951 Ethanol @ 100 ppm



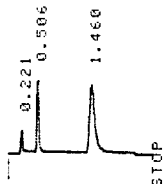
RUN# 4 JUN 16, 1992 15:32:56

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.200	12169	BB	.036	.52331	
.492	32895	BB	.045	1.41459	
6.685	2280341	BB	.303	98.06211	

TOTAL AREA=2325405
MUL FACTOR=1.0000E+00

* RUN # 5 JUN 16, 1992 15:55:54
START

*8.25 ppm
1:10 Injection CR# ALM 002105*



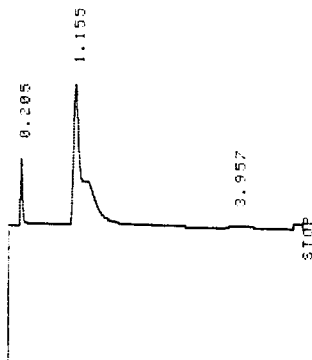
RT	AREA	TYPE	WIDTH	AREA2
.221	27369	BB	.033	6.30881
.506	120804	PB	.043	27.84645
1.450	285649	PB	.108	65.84477

TOTAL AREA= 433822
MUL FACTOR=1.0000E+00

* RUN # 6 JUN 16, 1992 16:00:57
START! not ready
STOP

RUN# 6 JUN 16, 1992 16:00:57
NO RUN PEAKS STORED

+ RUN # 7 JUN 16, 1992 16:01:15
START

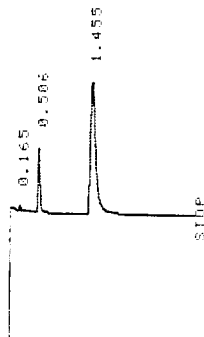


RUN# 7 JUN 16, 1992 16:01:15

RT	AREA	TYPE	WIDTH	AREA2
.205	105930	PB	.043	13.24029
1.155	621891	PV	.117	77.80416
3.957	71592	BP	.480	8.95555

TOTAL AREA= 799303
MUL FACTOR=1.0000E+00

+ RUN # 8 JUN 16, 1992 16:07:52 1:55 October
START

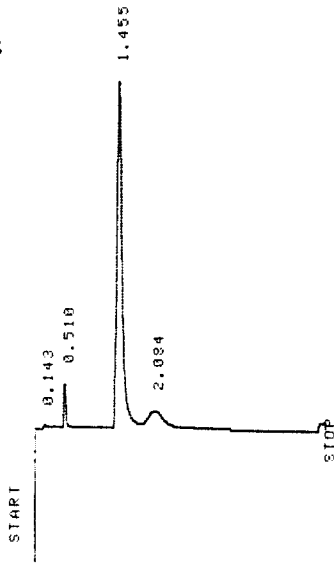


RUN# 8 JUN 16, 1992 16:07:52

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.506	104326	VB	.042	16.38142	
1.455	532530	BB	.106	83.61859	

TOTAL AREA= 636856
MUL FACTOR=1.0000E+00

* RUN # 9 JUN 16, 1992 16:12:30 1:2 *Obtain*

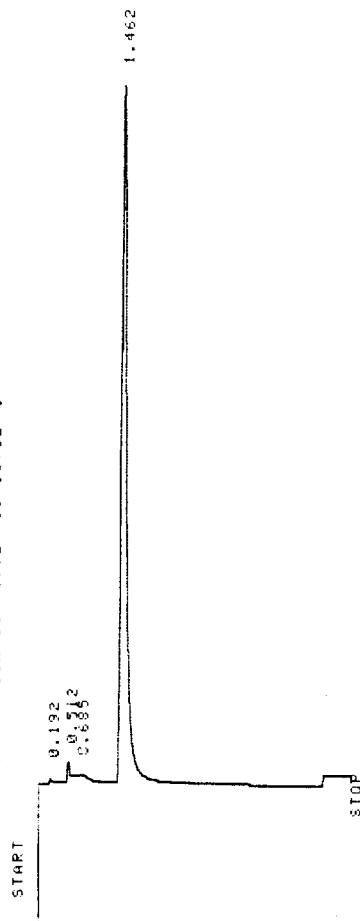


RUN# 9 JUN 16, 1992 16:12:30

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.510	77420	PB	.044	4.89549	
1.455	1356640	PB	.105	85.78419	
2.084	147397	BB	.249	9.32033	

TOTAL AREA=1581457
MUL FACTOR=1.0000E+00

* RUN # 10 JUN 16, 1992 16:18:32 No *Dilution*



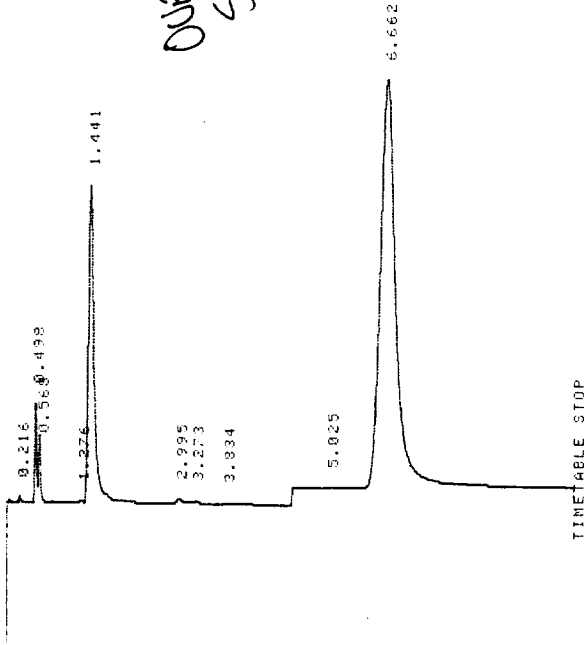
PUN# 10 JUN 16, 1992 16:18:32

0.12 9.650 57 .03 1.67359
 .685 105562 VP .382 3.70851
 1.462 263386 PB .104 94.61821

TOTAL AREA=2845478
 MUL FACTOR=1.0000E+00

*00 BREAK

* RUN # 11 JUN 16, 1992 17:09:12
 START

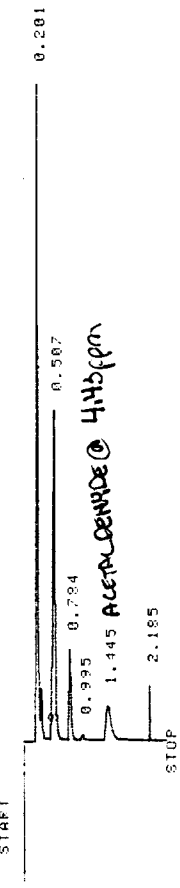


RUN# 11 JUN 16, 1992 17:09:12

AREA:	RT	AREA	TYPE	WIDTH	AREA2
	.498	146203	FV	.038	2.31387
	.568	103636	VB	.039	1.64019
	1.441	1232920	PB	.104	19.51272
	2.995	29304	VV	.121	.46378
	3.273	34808	VP	.145	.39262
	3.834	30401	FV	.229	.48114
	5.025	201777	PB	.379	3.19341
	6.662	4549498	PB	.382	72.00227

TOTAL AREA=6318544
 MUL FACTOR=1.0000E+00

* RUN # 12 JUN 17, 1992 08:41:30 1:10 Division Cyl # AAL 9441

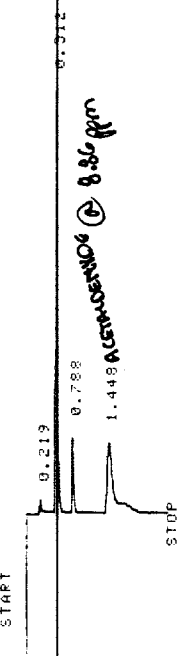


PUN# 12 JUN 17, 1992 08:41:30

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.201	0.995	849765	SPB	.034	49.18613
.507	1.445	558422	BB	.044	32.32261
.784	2.185	136332	PB	.039	7.89117
.995		15093	BP	.052	.87361
1.445		146859	PB	.106	8.58049
2.185		21181	BB	.009	1.22600

TOTAL AREA=1727652
MUL FACTOR=1.0000E+00

* RUN # 13 JUN 17, 1992 08:46:26 1:5 Division Cyl # AAL 9441



PUN# 13 JUN 17, 1992 08:46:26

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.219	0.219	20600	BB	.030	2.09037
.512	0.788	593147	PB	.038	60.19323
.798	1.448	111900	BB	.038	11.35499
1.448		259823	PB	.101	26.36538

TOTAL AREA= 985470
MUL FACTOR=1.0000E+00

* RUN # 14 JUN 17, 1992 08:51:49 1:2 Division Cyl # AAL 9441



STOP

RUN# 14 JUN 17, 1992 08:51:49

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.178	13402	BB	.039	1.00333	
.512	539365	VB	.037	40.37901	
.788	59953	PB	.039	4.41346	
1.286	35352	PV	.180	2.64659	
1.447	688684	VB	.186	51.55762	

TOTAL AREA=1335758

MUL FACTOR=1.0000E+00

* RUN # 15 JUN 17, 1992 08:55:56 MODL C4L# PAX 9441
START
0.150
0.505
1.444 ACETALDEHYDE @ 44.3 ppm
STOP

RUN# 15 JUN 17, 1992 08:55:56

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.505	27179	VB	.044	2.02211	
1.444	1316867	PB	.184	97.97792	

TOTAL AREA=1344045

MUL FACTOR=1.0000E+00

* RUN # 16 JUN 17, 1992 09:01:39 ALM 009105
START

0.174
0.502
1.436
STOP

1.436

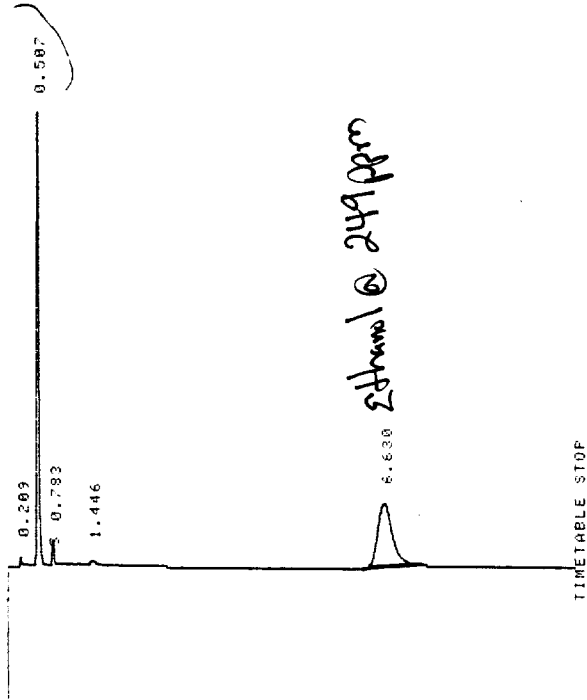
ACETALDEHYDE @ 82.5 ppm

RUN# 16 JUN 17, 1992 09:01:39

AREA%	RT	AREA	TYPE	WIDTH	AREA%
-------	----	------	------	-------	-------

TOTAL AREA=3011053
MUL FACTOR=1.0000E+00

* RUN # 17 JUN 17, 1992 09:09:46 112 Oibjia ALM029496
START

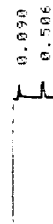


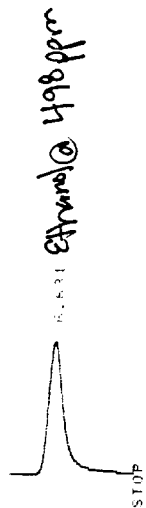
RUN# 17 JUN 17, 1992 09:09:46

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.209	15417	PV	.037	1.07272	
.507	637212	SHB	.037	44.33750	
.783	37615	BB	.038	2.61727	
1.446	27387	FB	.104	1.90560	
6.630	71951	FB	.303	50.06680	

TOTAL AREA=1437182
MUL FACTOR=1.0000E+00

* RUN # 19 JUN 17, 1992 09:12:11 117 ALM 029496
START



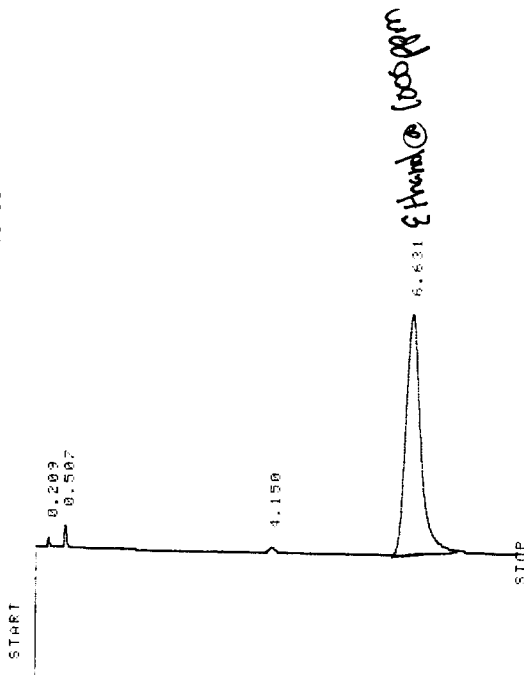


RUN# 18 JUN 17, 1992 09:21:17

AREA#	RT	AREA	TYPE	WIDTH	AREA%
1	6.631	13274	BB	.027	.87454
2	14.751	29423	PB	.044	1.93850
3	14.751	1475122	PB	.303	97.18694

TOTAL AREA=1517819
MUL FACTOR=1.0000E+00

* RUN # 19 JUN 17, 1992 09:30:35 ALM 0 20486



RUN# 19 JUN 17, 1992 09:30:35

AREA#	RT	AREA	TYPE	WIDTH	AREA%
1	0.209	13273	BB	.034	.48301
2	0.507	41269	PB	.046	1.50190
3	4.150	43959	BB	.166	1.59969
4	6.631	2649477	BB	.298	96.41549

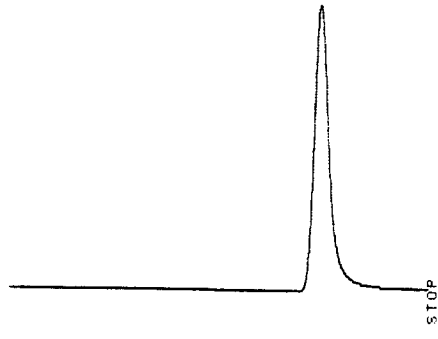
TOTAL AREA=2747978
MUL FACTOR=1.0000E+00

* RUN # 20 JUN 17, 1992 09:42:52 1:2 Dilution ALM 011208

START

CAL has very low
pressure to keep the
Ethanol from falling out
of the Gas: HARD.
get a good injection

Ethanol @ 2000 ppm.
BAD Injection Final Cal.
LEADS BURNING FINAL CAL.



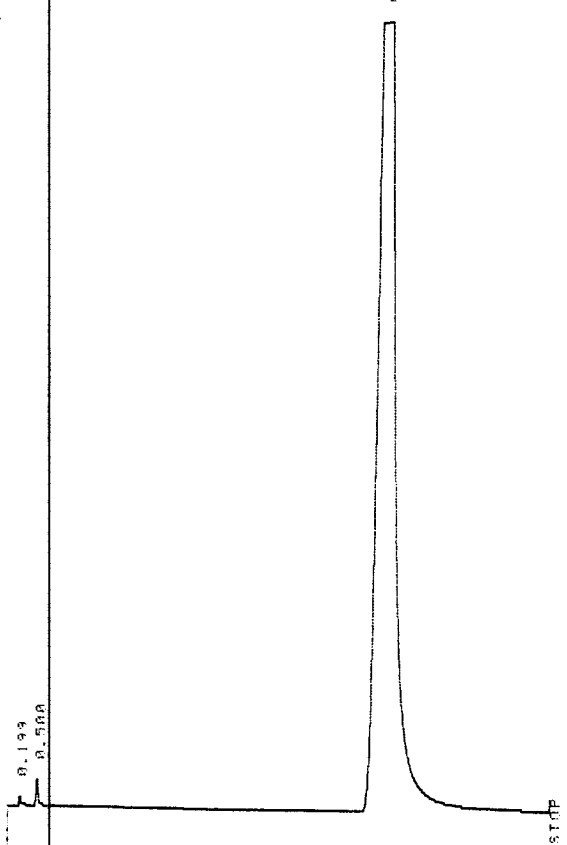
RUN# 20 JUN 17, 1992 09:42:52

AREA%	PT	AREA	TYPE	WIDTH	AREA%
.515	599338	BB	.037	15.53031	
.790	148232	PB	.038	3.84105	
6.637	311150	PB	.234	80.62864	

TOTAL AREA=3859150
MUL FACTOR=1.0000E+00

* RUN # 21 JUN 17, 1992 09:52:51 ALM 001008 Ethanol @ 4000 ppm

START
0.199
0.500

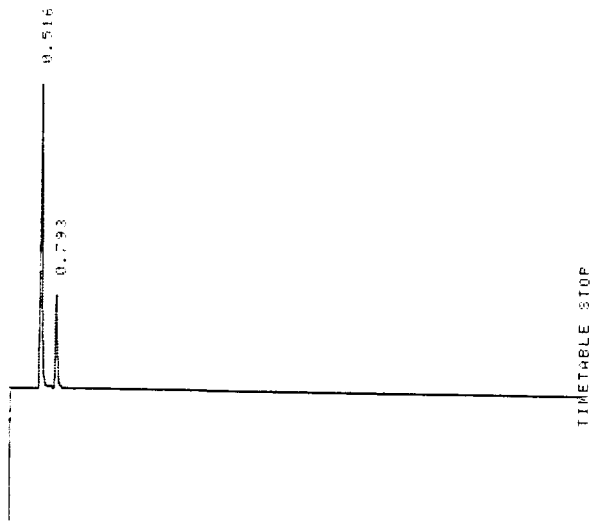


RUN# 21 JUN 17, 1992 09:52:51

.199	12936	PB	.033	.10920
.500	47747	BY	.044	.40335
6.645	1175896	PB	.209	94.48736

TOTAL AREA=1.1939E+07
MUL FACTOR=1.0000E+00

* RUN # 22 JUN 17, 1992 10:06:50
START

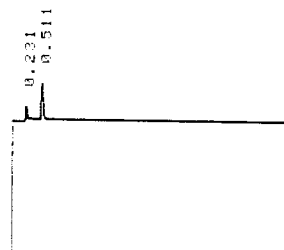


RUN# 22 JUN 17, 1992 10:06:50

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.516	435540	PB	.037	75.92806	
.793	138082	BB	.039	24.07195	

TOTAL AREA= 573622
MUL FACTOR=1.0000E+00

* RUN # 23 JUN 17, 1992 10:21:09 *SYNTHASE CHECK*
START



TIME/TABLE STOP

RUN# 23 JUN 17, 1992 10:12:108

AREA:

PT	AREA	TYPE	WIDTH	AREA2
.231	17709	BV	.031	23.09678
.511	58964	BB	.042	76.90320

TOTAL AREA= 76673

MUL FACTOR=1.0000E+00

* RUN # 24 JUN 17, 1992 10:38:158 CYL # 16-2046 METHANE @ 99.2 g/m

START

0.219

S

STOP

0.515

RUN# 24 JUN 17, 1992 10:38:158

AREA:

PT	AREA	TYPE	WIDTH	AREA2
.219	25633	PB	.037	.81759
.515	310958	BB	.036	93.16240

TOTAL AREA=3135190

MUL FACTOR=1.0000E+00

* RUN # 25 JUN 17, 1992 10:47:144 CYL # 16-2049 METHANE @ 109.1 g/m

START

0.226

0.780

STOP

0.503

RUN# 25 JUN 17, 1992 10:47:144

AREA:

PT	AREA	TYPE	WIDTH	AREA2
.226	17605	BV	.045	.22261
.503	7840528	BB	.037	99.14109
.730	50321	BB	.038	.63629

METHANE@1490

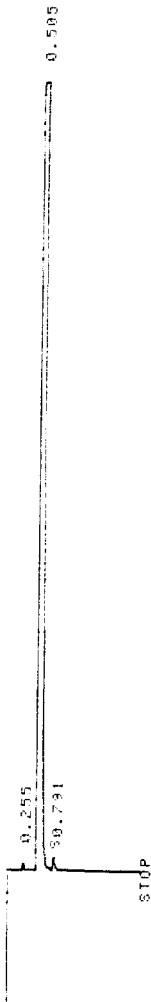
* RUN # 26
START

JUN 17, 1992

18154:42

CYC# 01051

METHANE@1490



RUN# 26 JUN 17, 1992 18154:42

AREA:

RT	AREA TYPE	WIDTH	AREA
.505	24739728	.048	99.91914
.791	20023	.038	.00087

TOTAL AREA=2.4760E+07
MUL FACTOR=1.0000E+00

METHANE@1490
FROM FLOW

* RUN # 27 JUN 17, 1992 11:01:05

START



RUN# 27 JUN 17, 1992 11:01:05

AREA:

RT	AREA TYPE	WIDTH	AREA
.395	55444	.259	.20024
.498	30956608	.060	99.27082
.777	164944	.039	.52894

TOTAL AREA=3.1184E+07
MUL FACTOR=1.0000E+00

THROUGH FLOW LINE

* RUN # 28 JUN 17, 1992 11:07:07

START



RUN# 28 JUN 17, 1992 11:07:07

AREA:

RT	AREA TYPE	WIDTH	AREA
.495	30956608	.060	99.27082

METHANE@1490
SYNTHESIS

TOTAL AREA=0.1100E+00
MUL FACTOR=1.0000E+00

* RUN # 29 JUN 17, 1992 11:16:09
START

MEMINE @ 200



PUN# 29 JUN 17, 1992 11:16:09

RT	AREA	TYPE	WIDTH	WREX
.274	11324	FB	.032	.03345
.496	33846624	SPB	.065	99.96656

TOTAL AREA=3.3858E+07
MUL FACTOR=1.0000E+00

* RUN # 30 JUN 17, 1992 11:25:48
START



PUN# 30 JUN 17, 1992 11:25:48

RT	AREA	TYPE	WIDTH	WREX
.508	2045384	SPB	.036	99.34403
.735	13506	BB	.039	.65598

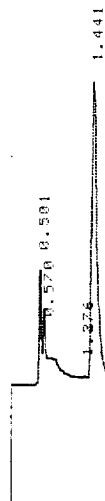
TOTAL AREA=2058890
MUL FACTOR=1.0000E+00

Complete / no further
Time

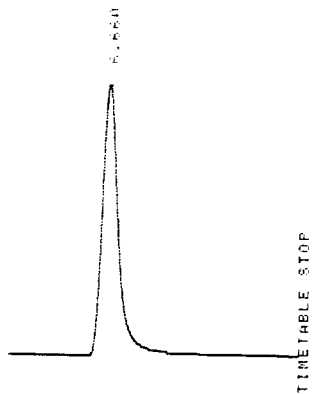
* TIME 11:31:50
JUN 17, 1992 11:31:50

* RUN # 31 JUN 17, 1992 11:33:25
START

FRONT



2.990
3.270

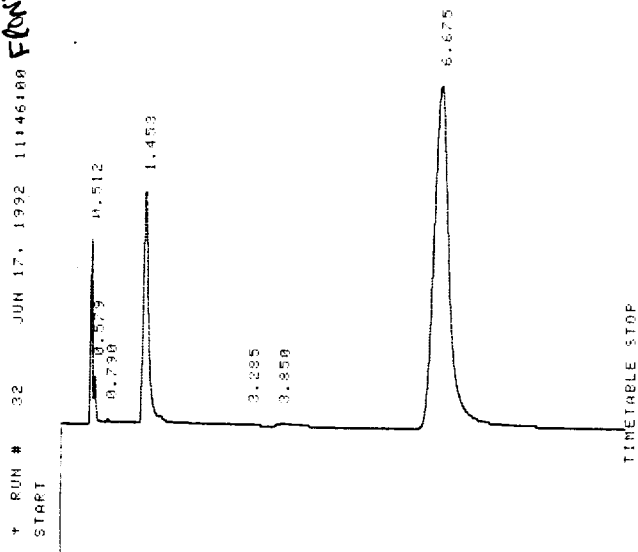


RUN# 31 JUN 17, 1992 11:33:25

AREA%	RT	AREA	TYPE	WIDTH	AREA2
1.901	109086	PV	.029	2.45204	
1.570	79691	VB	.037	1.79130	
1.441	1174986	VV	.105	26.40910	
2.990	19211	VV	.120	.43193	
3.270	20370	VB	.133	.45288	
6.660	3045549	PB	.302	68.45786	

TOTAL AREA=4448794
MUL FACTOR=1.0000E+00

FRONT



RUN# 32 JUN 17, 1992 11:46:00
START

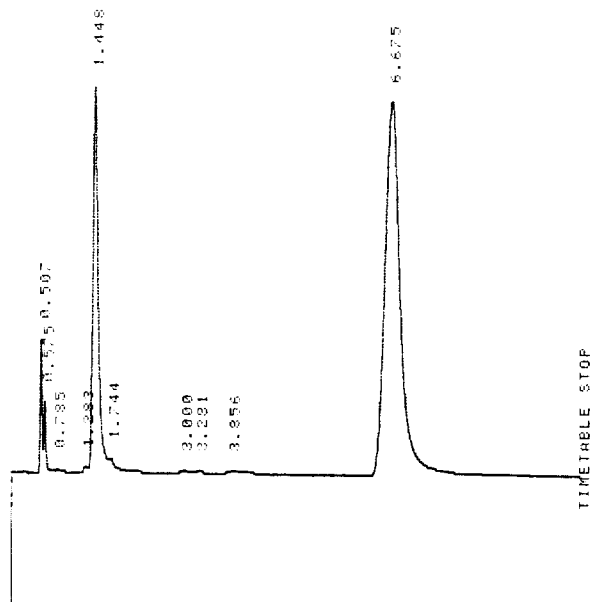
RUN# 32 JUN 17, 1992 11:46:00

AREA% RT AREA TYPE WIDTH AREA2

1.453	916261	FB	.106	17.7382
3.285	23010	VF	.146	.44550
3.850	56827	FB	.318	1.10043
6.675	3942554	FB	.302	74.94001

TOTAL AREA=5164998
MUL FACTOR=1.0000E+00

* RUN # 33 JUN 17, 1992 11:56:36 **Flow**
START



RUN# 33 JUN 17, 1992 11:56:36

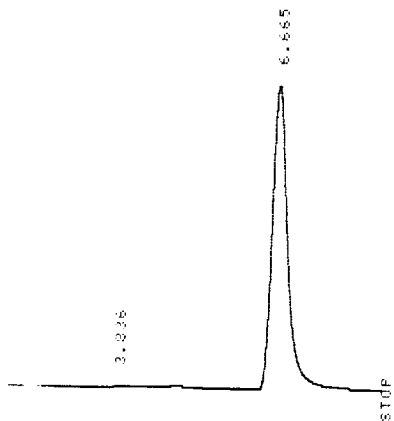
AREA%	RT	AREA	TYPE	WIDTH	AREA%
.507	205665	PV	.040	3.25320	
.575	107864	VB	.039	1.70619	
.785	17990	BP	.079	.28457	
1.283	49270	PV	.150	.77935	
1.448	150614	VV	.107	24.52758	
1.744	95580	VF	.159	1.51180	
3.000	26641	VV	.140	.42141	
3.281	29126	VF	.136	.46071	
3.856	44809	PV	.223	.70079	
6.675	4194362	FB	.303	66.34630	

TOTAL AREA=6321920
MUL FACTOR=1.0000E+00

* RUN # 34 JUN 17, 1992 12:07:13
START



Flow
0.502
0.254
0.780



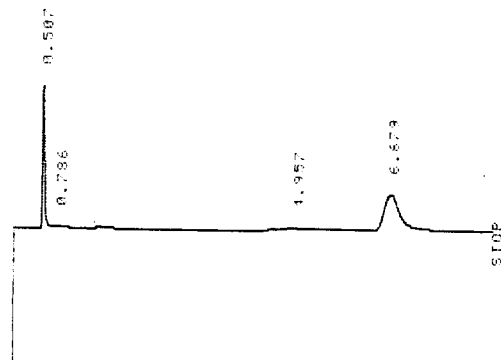
RUN# 34 JUN 17, 1992 12:07:13

AREA	RT	AREA	TYPE	WIDTH	AREA%
.254	1.2595	BV	.031		.30541
.502	3.7357	FB	.042		9.06318
.780	1.8300	BV	.040		.24976
1.446	2.36194	VV	.133		5.72743
3.836	4.2940	FV	.262		1.04125
6.665	3448120	FB	.303		83.61299

TOTAL AREA=4123906
MUL FACTOR=1.0000E+00

Handwritten note: 2000g sample

* RUN # 35 JUN 17, 1992 12:19:34



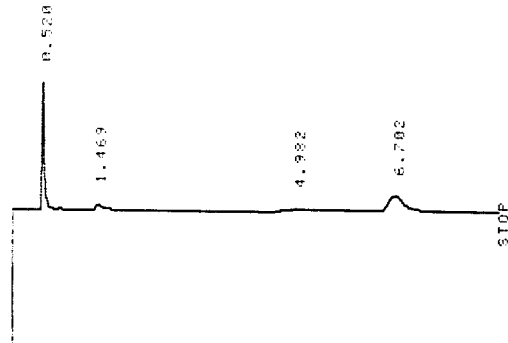
RUN# 35 JUN 17, 1992 12:19:34

AREA

4.950 1.5850 VB .318 10.34426
6.629 441633 PB .311 60.23306

TOTAL AREA= 733207
MUL FACTOR=1.0000E+00

* RUN # 36 JUN 17. 1992 12:29:55 *STRANGE REND*
START

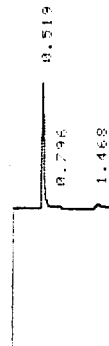


RUN# 36 JUN 17. 1992 12:29:55

RT	AREA	TYPE	WIDTH	AREA%
0.520	202810	PB	.042	41.31762
1.469	37769	PB	.136	7.69452
4.982	45421	PB	.296	9.25343
6.702	201856	PB	.318	41.73443

TOTAL AREA= 490856
MUL FACTOR=1.0000E+00

* RUN # 37 JUN 17. 1992 12:40:15
START



Handwritten notes:
NITTA MODEL
HARVARD
HARVARD

6.705

TIMEINBLE STOP

RUN# 37 JUN 17, 1992 12:40:15

AREA:

RT	AREA	TYPE	WIDTH	WPERC
.519	133807	FB	.041	24.93734
1.468	23937	BB	.122	3.08000
6.705	559432	FB	.358	71.98266

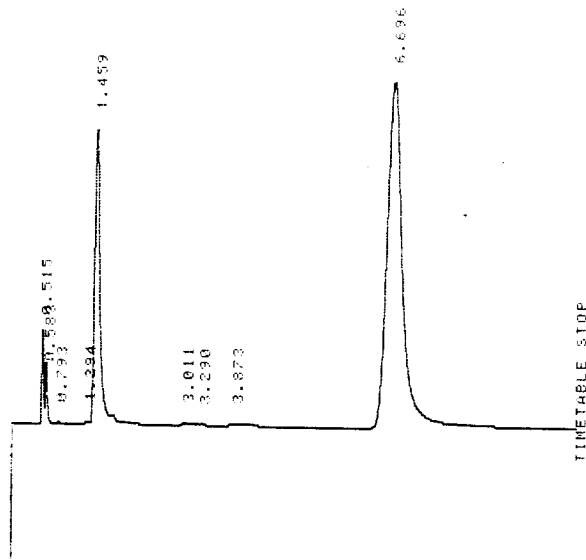
TOTAL WPERC=77.7176

MUL FACTOR=1.0000E+00

Handwritten: (last sample 1st lot)

* RUN # 38 JUN 17, 1992 12:51:50

START



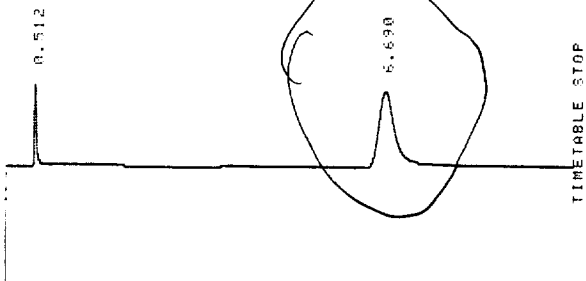
RUN# 38 JUN 17, 1992 12:51:50

AREA:

RT	AREA	TYPE	WIDTH	WPERC
.515	138531	PV	.038	2.56483
.593	91953	VB	.038	1.70193
1.294	11277	PV	.058	.20872
1.459	117528	WV	.106	21.75191
3.011	18831	PV	.119	.34835
3.290	22552	VF	.144	.41741
3.873	69465	FF	.365	1.35710

TOTAL AREA=5402870
MUL FACTOR=1.0000E+00

* RUN # 39 JUN 17, 1992 13:06:01 REAR 100% N₂ that long H₂ line
START



REAR DATA
Run 01
Suspect. This has long pulse & pump pulse d

RUN# 39 JUN 17, 1992 13:06:01

AREA#	PT	AREA TYPE	WIDTH	AREA#
	.512	129073 PB	.041	12.72390
	6.690	* 885349 PB	.312	87.27622

TOTAL AREA=1014422
MUL FACTOR=1.0000E+00

* RUN # 40 JUN 17, 1992 13:17:55 N₂ 100% N₂ 100% O₂
START



N₂ 100% O₂

TIME/ABLE STOP

RUN# 40 JUN 17. 1992 13:17:55

AREA	PT	AREA TYPE	WIDTH	AREA
.517	268329	BB	.038	28.82522
.795	72081	FB	.039	21.17476

TOTAL AREA= 340410
MUL FACTOR=1.0000E+00

* RUN # 41 JUN 17. 1992 13:28:49
START



TIME/ABLE STOP

RUN# 41 JUN 17. 1992 13:28:49

AREA	PT	AREA TYPE	WIDTH	AREA
.512	485121	BB	.038	96.40662
1.471	19092	FB	.171	3.59338

TOTAL AREA= 503203
MUL FACTOR=1.0000E+00

* RUN # 42 JUN 17. 1992 14:11:11
START

BUN LINE RUN 01

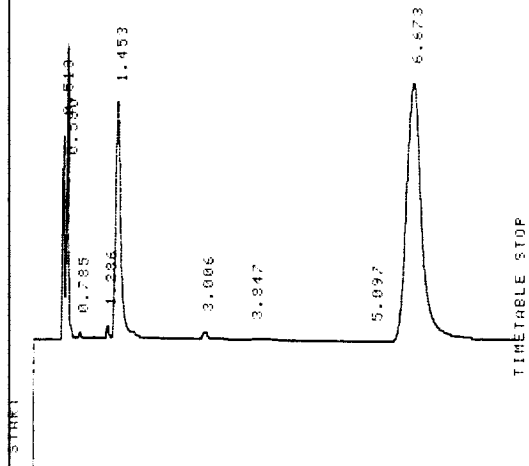


RUN# 42 JUN 17, 1992 14:11:11

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.515	1.14230	BY	.037	23.05510	
.584	88653	VB	.041	18.52430	
1.460	123641	PB	.110	14.67618	
6.680	435926	PB	.436	51.74442	

TOTAL AREA= 842460
MUL FACTOR=1.0000E+00

* TIME 8.5 STOP
* RUN # 43 JUN 17, 1992 14:21:15 **REAL**



RUN# 43 JUN 17, 1992 14:21:15

PT	AREA	TYPE	WIDTH	AREA1
.513	270407	PV	.026	5.71044
.530	422723	VB	.030	8.92703
.785	12423	PR	.010	.28235
1.286	30056	PV	.053	.63472
1.453	442276	VV	.106	14.84892
3.006	45278	PV	.113	.95618
3.947	42801	EV	.293	.90387
5.097	61194	PB	.624	1.23229
6.673	2908154	PB	.304	61.41421

TOTAL AREA=4735312
MUL FACTOR=1.0000E+00

* RUN # 44 JUN 17, 1992 14:33:00
START

0.515

S
STOP

RUN# 44 JUN 17, 1992 14:33:00

PT	AREA	TYPE	WIDTH	AREA1
.515	2076036	SPB	.036	100.00000

TOTAL AREA=2076036
MUL FACTOR=1.0000E+00

* RUN # 45 JUN 17, 1992 14:39:22
START

NETWAVE @ 80.2 ppm 1/4 JUMPED
BACK RUN OVER

0.210

0.513

S
STOP

RUN# 45 JUN 17, 1992 14:39:22

PT	AREA	TYPE	WIDTH	AREA1
.210	158796	BH	.251	4.77862
.513	3164253	SHB	.037	95.22139

TOTAL AREA=3323048
MUL FACTOR=1.0000E+00

* RUN # 46 JUN 17, 1992 14:42:25
START

NETWAVE @ 80.2 ppm 1/4 JUMPED (RUN 02)
BACK RUN OVER

0.510

S
STOP

PUN# 46 JUN 17, 1992 14:42:25

AREA:

PT	AREA TYPE	WIDTH	AREA%
.510	2233074	SFB	.037 100.00000

TOTAL AREA=3233074
MUL FACTOR=1.0000E+00

* RUN # 47 JUN 17, 1992 14:45:02 METHOD @ 80.2 HEAT TRACE 1006
START
STOP
1.040
0.513
(FLOOR - 10.10) NITE

PUN# 47 JUN 17, 1992 14:45:02

AREA:

PT	AREA TYPE	WIDTH	AREA%
.513	1822710	SFB	.037 92.05386
1.040	157337	BY	.346 7.94612

TOTAL AREA=1980047
MUL FACTOR=1.0000E+00

* RUN # 48 JUN 17, 1992 14:53:15 METHOD @ 80.2 ppm NITE 1006
START
STOP
0.514
HEAT TRACE

PUN# 48 JUN 17, 1992 14:53:15

AREA:

PT	AREA TYPE	WIDTH	AREA%
.514	2344405	SFB	.037 100.00000

TOTAL AREA=2344405
MUL FACTOR=1.0000E+00

* RUN # 49 JUN 17, 1992 14:56:00 METHOD @ 80.2 ppm NITE 1006
START
STOP
0.515
HEAT TRACE

RUN# 49 JUN 17, 1992 14:56:00

AREA:

PT	AREA	TYPE	WIDTH	AREA%
.515	3164478	SPB	.037	100.00000

TOTAL AREA=3164478
MUL FACTOR=1.0000E+00

NITTA MADE
HEAT TAPPE

80.2 99m
METRANE @

+ RUN # 50 JUN 17, 1992 14:58:50
START: not read.

0.520

STOP 1.111

RUN# 50 JUN 17, 1992 14:58:50

AREA:

PT	AREA	TYPE	WIDTH	AREA%
.520	3237374	SPB	.037	92.21821
1.111	273195	I BH	.272	7.78181

TOTAL AREA=3510558
MUL FACTOR=1.0000E+00

80.2 1/4" JUMPEL
METRANE @

+ RUN # 51 JUN 17, 1992 15:01:05
START

0.511

STOP

RUN# 51 JUN 17, 1992 15:01:05

AREA:

PT	AREA	TYPE	WIDTH	AREA%
.511	3231278	SPB	.037	100.00000

TOTAL AREA=3231278
MUL FACTOR=1.0000E+00

80.2 1/4" JUMPEL
METRANE @
NITTA MADE HEAT TAPPE

+ RUN # 52 JUN 17, 1992 15:11:30
START

0.515

STOP 1.211

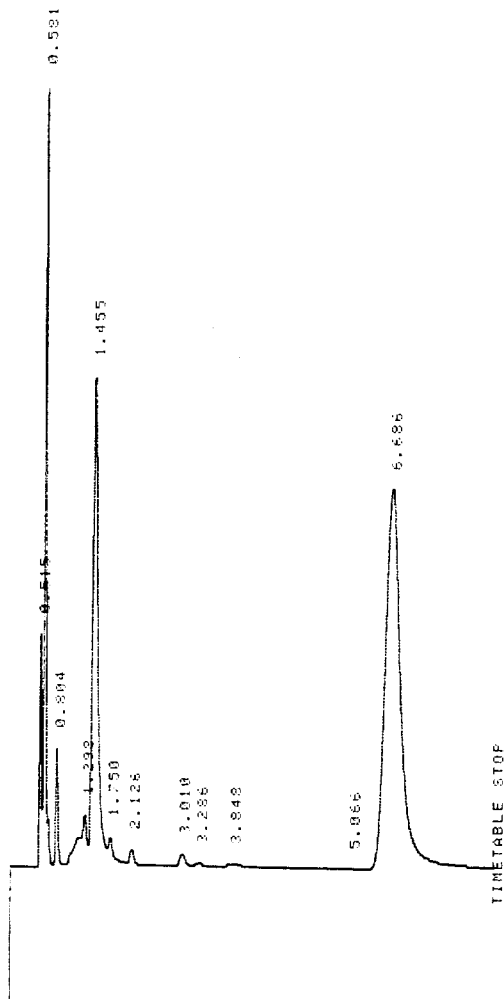
RUN# 52 JUN 17, 1992 15:11:30

AREA:

.805 6.7313 PB .039 2.02053
 1.311 15989 VV .056 .47294
 1.465 11575 VV .089 .34745

TOTAL AREA=2331453
 MUL FACTOR=1.0000E+00

* RUN # 53 JUN 17, 1992 15:16:59 FRONT
 START



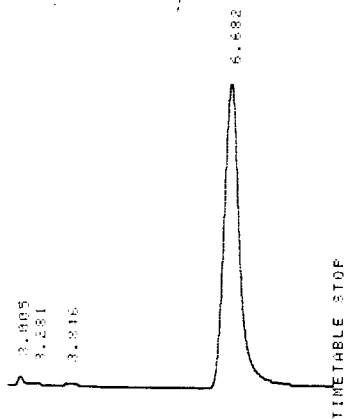
RUN# 53 JUN 17, 1992 15:16:59

RT	AREA	TYPE	WIDTH	AREA1
.515	305388	BV	.035	3.54587
.581	1139122	VB	.039	13.22637
.804	192982	BB	.041	2.12461
1.298	366819	BV	.199	4.25914
1.455	1948856	VV	.107	22.82821
1.750	129175	VV	.114	1.49985
2.126	59570	VB	.090	.69167
3.010	58111	BV	.113	.67473
3.286	38044	VP	.161	.44173
3.843	54573	FV	.233	.63365
5.066	59150	PB	.674	.68679
6.686	4270717	PB	.304	49.58739

TOTAL AREA=9.6125E+06
 MUL FACTOR=1.0000E+00

* RUN # 54 JUN 17, 1992 15:26:50 REAL
 START



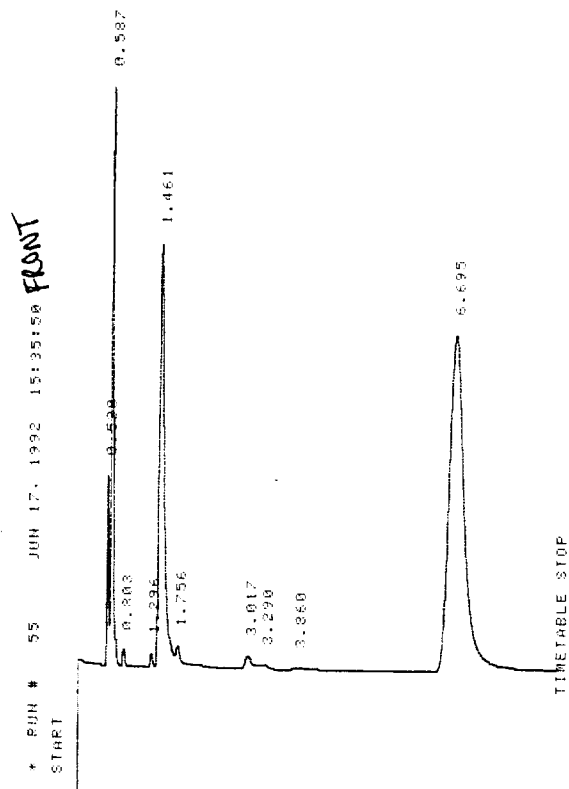


TIME/ABLE STOP

RUN# 54 JUN 17, 1992 15:26:150

AREA%	RT	AREA TYPE	WIDTH	AREA:
.310	263266	PV	.037	4.07020
.575	927232	VE	.039	14.36354
.730	19098	BB	.039	.29584
1.284	28978	PV	.053	.44889
1.450	155866	VV	.105	24.14804
1.745	77915	VV	.119	1.20636
3.005	51102	VV	.124	.79161
3.281	31700	VV	.163	.49106
3.846	65110	VP	.297	1.00860
6.682	3432199	PB	.305	53.16726

TOTAL AREA=6455456
MUL FACTOR=1.0000E+00



TIME/ABLE STOP

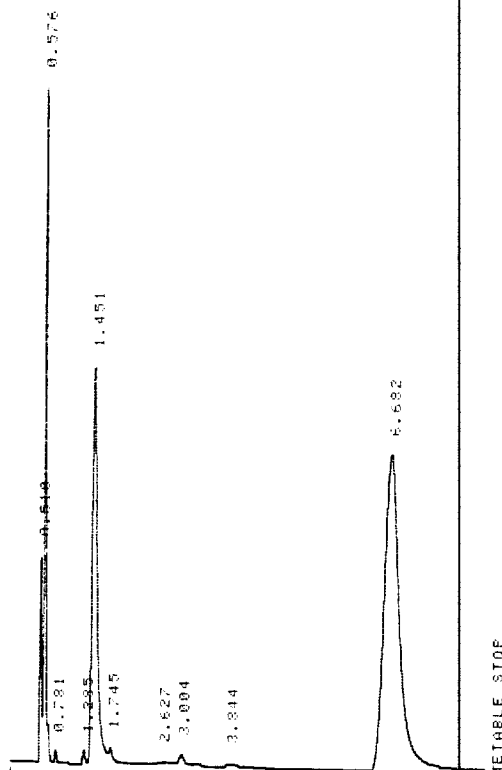
* RUN # 55 JUN 17, 1992 15:35:150 FRONT

RUN# 55 JUN 17, 1992 15:35:150

RT	AREA	TYPE	WIDTH	AREA
.520	54716	BV	.035	3.74318
.587	930736	VB	.038	12.20806
.803	34508	BB	.047	.58711
1.236	33009	FV	.054	.48508
1.461	1555915	VV	.104	24.34779
1.756	95538	VB	.101	1.27172
3.017	98298	BV	.149	1.29758
3.230	47478	VF	.175	.69721
3.860	40852	PV	.219	.68034
6.695	3731862	PB	.300	54.84152

TOTAL AREA=6804813
MUL FACTOR=1.0000E+00

* RUN # 56 JUN 17, 1992 15:45:10 **REAL**
START

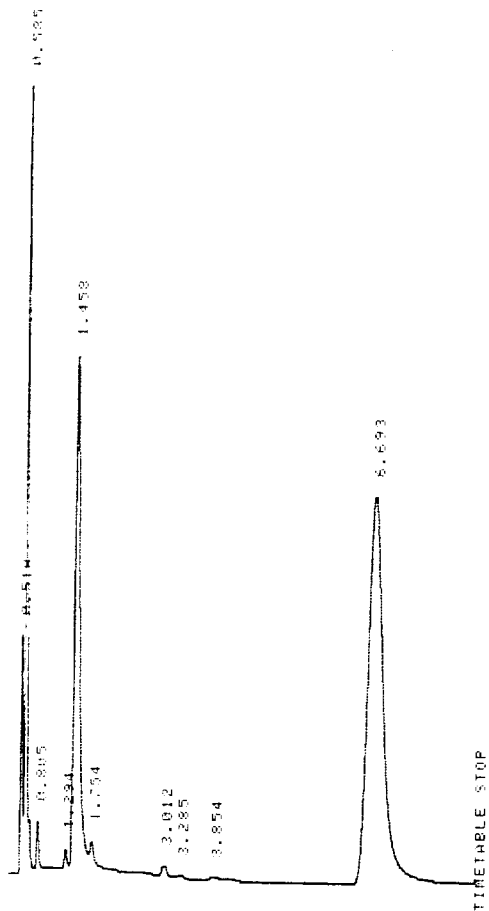


RUN# 56 JUN 17, 1992 15:45:10

RT	AREA	TYPE	WIDTH	AREA
.510	276721	BV	.035	4.14194
.576	990225	VB	.039	14.82127
.781	19245	BB	.038	.28805
1.235	29532	BV	.053	.44202
1.451	1594421	VV	.105	23.26592
1.745	71714	VB	.109	1.07339
2.627	46552	BV	.269	.69677
3.004	63211	VV	.135	.94612
3.844	50476	FV	.221	.75550
6.692	3579010	PB	.305	53.56912

TOTAL AREA=6681107
MUL FACTOR=1.0000E+00

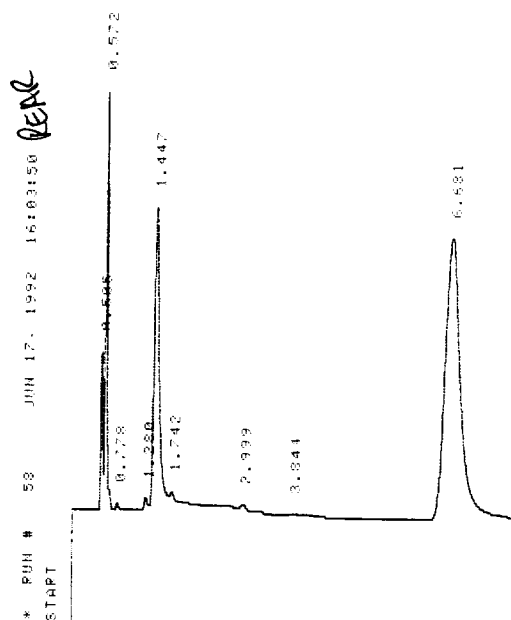
* RUN # 57 JUN 17, 1992 15:54:38 **100%**



RUN# 57 JUN 17. 1992 15:54:30

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.518	301298	PV	.034	3.59072	
.585	1263331	VB	.039	15.01434	
.805	80885	PB	.045	.96130	
1.294	58228	VV	.071	.69202	
1.458	2029330	VV	.106	24.11327	
1.754	150346	VV	.127	1.78682	
3.012	65288	VV	.119	.77593	
3.285	29770	VB	.129	.35381	
3.854	49474	BV	.215	.58798	
6.693	4386524	PB	.305	52.13382	

TOTAL AREA=8.4142E+06
MUL FACTOR=1.0000E+00



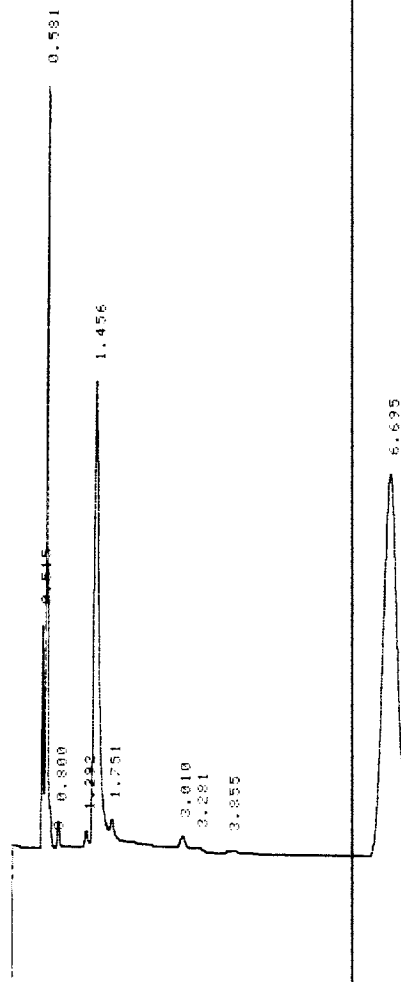
* RUN # 58 JUN 17. 1992 16:03:50
START

RUN# 59 JUN 17, 1992 16:03:50

AREA%	PT	AREA TYPE	WIDTH	AREA%
.505	216130	PV	.036	3.96726
.572	597619	VB	.038	10.97012
.778	13066	PB	.039	.23984
1.280	28559	BV	.063	.52424
1.447	1194742	VV	.106	21.93114
1.742	180236	VB	.156	1.93997
2.999	39569	VV	.116	.72634
3.844	54049	FP	.295	.99214
6.681	3203726	PR	.306	58.80893

TOTAL AREA=547596
MUL FACTOR=1.0000E+00

* RUN # 59 JUN 17, 1992 16:12:55 **FRONT**
START



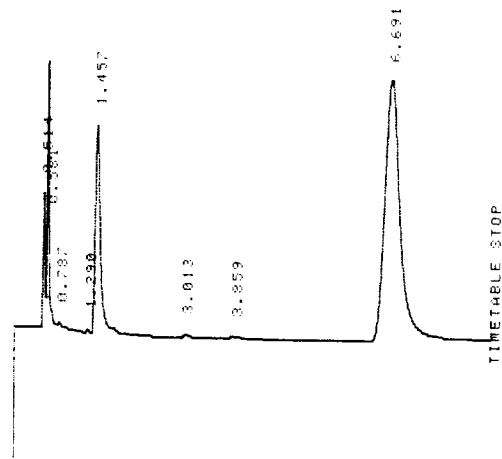
RUN# 59 JUN 17, 1992 16:12:55

AREA%	PT	AREA TYPE	WIDTH	AREA%
.515	302400	BH	.035	3.75463
.581	1121578	SHB	.039	13.92561
.800	52169	BB	.047	.64774
1.292	43437	BV	.063	.53932
1.456	1954566	VV	.106	23.02671
1.751	154367	VV	.137	1.91663
3.010	66569	VV	.120	.82653
3.281	26925	VP	.127	.33430
3.855	46654	PV	.216	.57926
6.695	4385379	PB	.305	54.44928

TOTAL AREA=8854064

* RUN # 60 JUN 17, 1992 16:24:15 CARFAX WAD LINE # 07

START



RUN# 60 JUN 17, 1992 16:24:15

AREA:			
PT	AREA	TYPE	WIDTH
0.737	185776	BV	.036
0.884	396132	VB	.039
1.290	18945	PV	.049
1.457	824338	VV	.105
3.013	24903	PV	.126
3.859	49943	PP	.294
6.691	2983765	FB	.306

TOTAL AREA=4475866

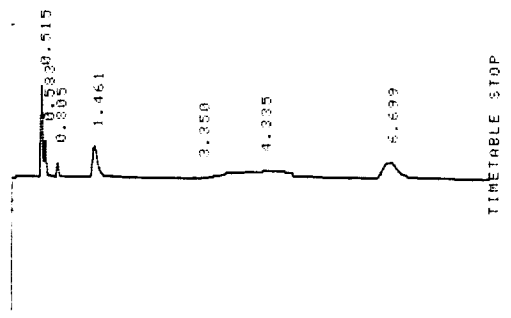
MUL FACTOR=1.0000E+00

1 READ 0.000

0.000000

+ RUN # 61 JUN 17, 1992 16:47:30 REAR

START



RUN# 61 JUN 17, 1992 16:47:30

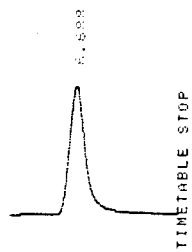
AREA#	PT	AREA	TYPE	WIDTH	AREA2
1.583	60293	V8	.041	5.51261	
1.805	25530	BB	.041	2.34009	
1.461	135340	VV	.108	12.37623	
3.350	29820	PV	.256	2.72630	
4.335	481704	V8	1.337	44.04365	
6.699	224729	FB	.319	20.55045	

TOTAL AREA=1093548
MUL FACTOR=1.0000E+00

* RUN # 62 JUN 17, 1992 16:56:30 REAR

START





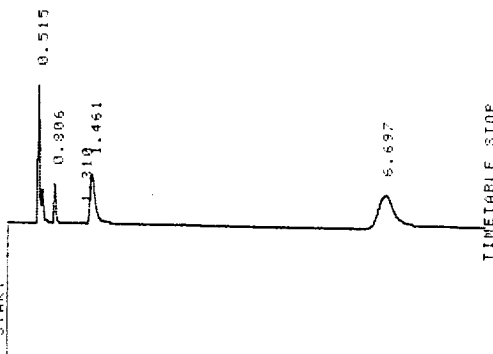
RUN# 62 JUN 17, 1992 16:56:30

AREA:

PT	AREA	TYPE	WIDTH	AREA%
.510	152995	VB	.038	6.69728
.579	39659	VB	.041	1.73617
1.455	524631	PB	.105	22.96695
6.693	1567812	PB	.322	68.59962

TOTAL AREA=2284286
MUL FACTOR=1.0000E+00

* RUN # 63 JUN 17, 1992 17:05:55 *Leak*



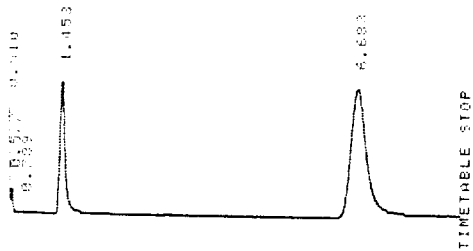
RUN# 63 JUN 17, 1992 17:05:55

AREA:

PT	AREA	TYPE	WIDTH	AREA%
.515	258943	VB	.048	24.00563
.806	61951	BB	.039	5.74324
1.461	216947	VB	.112	20.11234
6.697	540835	BB	.417	50.13880

TOTAL AREA=1078676
MUL FACTOR=1.0000E+00

* RUN # 64 JUN 17, 1992 17:14:55 *Leak*



RUN# 64 JUN 17. 1992 17:14:55

PT	AREA	TYPE	WIDTH	AREA%
.510	157163	PV	.039	7.04158
.577	39049	VB	.040	1.74956
1.453	522435	PB	.104	23.40735
6.693	1513290	PB	.315	67.80150

TOTAL AREA=2231926
MUL FACTOR=1.0000E+00

* RUN # 65 JUN 17. 1992 17:24:30 *lead*



RUN# 65 JUN 17. 1992 17:24:30

RT	AREA	TYPE	WIDTH	AREA%
.513	116836	VB	.037	17.13256
.530	63318	VB	.040	10.20740
.802	21790	FB	.040	10.59210
1.203	10224	VB	.065	1.50779
1.458	13431	VB	.111	12.81560
2.125	18556	VB	.110	2.44041
6.696	259520	FB	.451	88.25414

TOTAL AREA= 678410
MUL FACTOR=1.0000E+00

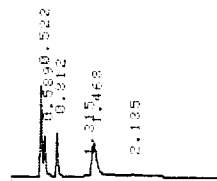
+ RUN # 66 JUN 17, 1992 17:33:51 *FRONT*
START



RT	AREA	TYPE	WIDTH	AREA%
.504	170653	VB	.045	9.16742
1.447	427778	FB	.105	22.98009
6.679	1263085	FB	.308	67.85251

TOTAL AREA=1861516
MUL FACTOR=1.0000E+00

+ RUN # 67 JUN 17, 1992 17:43:50 *REAL*
START





TIME/TABLE STOP

PUN# 67 JUN 17, 1992 17:43:50

AREA#	RT	AREA TYPE	WIDTH	AREA#
.522	131807	SV	.037	17.78563
.529	64200	VB	.040	9.66235
.912	66007	FB	.039	8.90678
1.468	145448	VV	.110	19.62630
2.135	23043	VB	.147	3.10935
6.717	310592	BB	.334	41.90898

TOTAL AREA=741087
MUL FACTOR=1.0000E+00

* PUN # 68 JUN 17, 1992 17:56:35 REAL METHOD# 2 30.2 AM

0.521

50.811

STOP

PUN# 69 JUN 17, 1992 17:56:35

AREA#	RT	AREA TYPE	WIDTH	AREA#
.521	2312408	SPB	.037	99.22346
.811	22793	BB	.040	.77654

TOTAL AREA=233202
MUL FACTOR=1.0000E+00

* PUN # 69 JUN 17, 1992 17:58:55

0.505

STOP

PUN# 69 JUN 17, 1992 17:58:55

AREA#	RT	AREA TYPE	WIDTH	AREA#
.506	1750460	SPB	.037	100.00000

* RUN # 70 JUN 17, 1992 18:01:35 FRONT METERED @ 179.88mm
 START
 STOP 0.505

RUN# 70 JUN 17, 1992 18:01:35

AREA:
 RT AREA TYPE WIDTH AREA
 .505 2389056 /588 .046 99.92150
 .739 18769 88 .038 .67851

TOTAL AREA=2.3908E+07
 MUL FACTOR=1.0000E+00

* RUN # 71 JUN 17, 1992 18:05:40 REAR METERED @ 199.16mm
 START: not ready

0.524
 STOP

RUN# 71 JUN 17, 1992 18:05:40

AREA:
 RT AREA TYPE WIDTH AREA
 .524 7620112 888 .036 99.41526
 .815 44821 88 .040 .58475

TOTAL AREA=7664934
 MUL FACTOR=1.0000E+00

* RUN # 72 JUN 17, 1992 18:07:55 FRONT METERED @ 199.16mm
 START

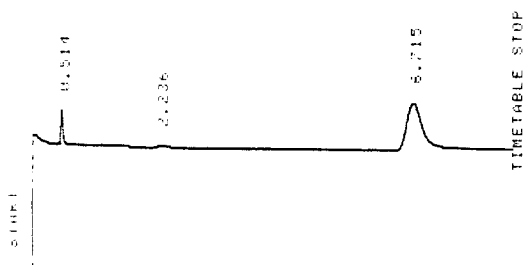
0.514
 STOP

RUN# 72 JUN 17, 1992 18:07:55

AREA:
 RT AREA TYPE WIDTH AREA
 .392 99128 88 .026 1.29415
 .514 7560547 1588 .037 98.74586

TOTAL AREA=7659677
 MUL FACTOR=1.0000E+00

FRONT



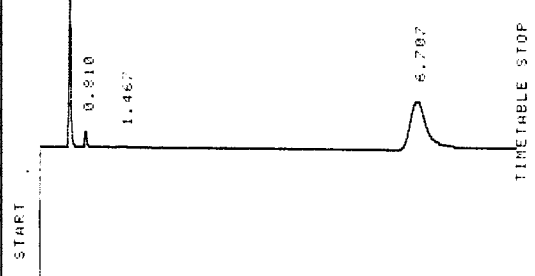
RUN# 73 JUN 17, 1992 18:12:26

AREA%	RT	AREA	TYPE	WIDTH	HEIGHT
	.514	33599	BB	.029	5.26622
	2.236	38608	FP	.259	6.06385
	6.715	565223	FB	.313	88.66932

TOTAL AREA= 638010
MUL FACTOR=1.0000E+00

018321
STAND @ 200 ppm
REAR 1/4" TAPER

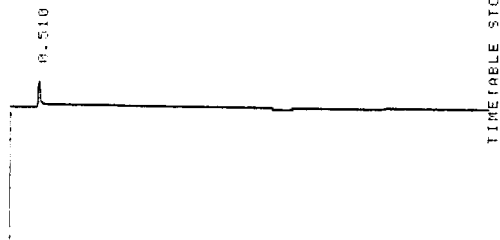
RUN# 74 JUN 17, 1992 18:22:10



RT	AREA	TYPE	WIDTH	AREA%
.520	325557	BB	.038	26.54474
.910	28742	BB	.041	3.38251
1.467	1459	VB	.102	1.2508
5.707	590767	BB	.317	88.34771

TOTAL AREA= 949724
MUL FACTOR=1.0000E+00

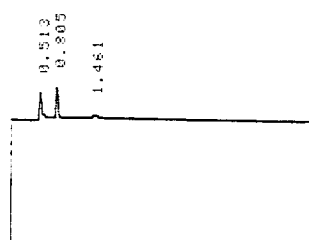
* RUN # 75 JUN 17, 1992 18:33:25 NITROGEN GLYPHIC FRONT HEPH TUBE (SUMMER)



RT	AREA	TYPE	WIDTH	AREA%
.510	42423	BB	.044	100.00000

TOTAL AREA= 42423
MUL FACTOR=1.0000E+00

* RUN # 76 JUN 17, 1992 18:45:50 NITROGEN GLYPHIC REAR SUMMER



6.715

TIME/TABLE STOP

RUN# 76 JUN 17, 1992 18:45:50

AREA#	PT	AREA	TYPE	WIDTH	AREA#
	.513	50329	BB	.049	9.04915
	.805	50817	BB	.040	8.14337
	1.461	22946	PB	.101	3.67207
	6.715	500037	I BH	2.187	89.13840

TOTAL AREA= 624029
MUL FACTOR=1.0000E+00

* RUN # 77 JUN 17, 1992 18:55:26

START

0.120

STOP

0.504

*CHL # 12-2046
METHANE @ 20.05 ppm*

RUN# 77 JUN 17, 1992 18:55:26

AREA#	PT	AREA	TYPE	WIDTH	AREA#
	.120	12525	BB	.036	1.31292
	.584	941459	SHB	.037	98.68710

TOTAL AREA= 953980
MUL FACTOR=1.0000E+00

*CHL # 12-2046
METHANE @ 14.1 ppm*

* RUN # 78 JUN 17, 1992 18:58:07

START

S

0.505

STOP

RUN# 78 JUN 17, 1992 18:58:07

AREA#	PT	AREA	TYPE	WIDTH	AREA#
	.505	1657964	SHB	.037	100.00000

TOTAL AREA=1657964
MUL FACTOR=1.0000E+00

* RUN # 79 JUN 17, 1992 19:01:24

NO DATA

*CHL # 12-2046
METHANE @ 20.0 ppm*

START

STOP

RUN# 79 JUN 17, 1992 19:01:24

AREA:

RT	AREA TYPE	WIDTH	AREA%
.507	3304614	ISBH .038	97.63488
.773	90079	ITB8 .205	2.36592

TOTAL AREA=3384693

MUL FACTOR=1.0000E+00

* RUN # 80 JUN 17, 1992 19:07:11

START
0.191
0.504
0.598
STOP
METANES @ 9.76ppm
ETHANE @ 10.01ppm

RUN# 80 JUN 17, 1992 19:07:11

AREA:

RT	AREA TYPE	WIDTH	AREA%
.504	475650	BV .037	41.28157
.598	676559	VB .036	58.71845

TOTAL AREA=1152209

MUL FACTOR=1.0000E+00

* RUN # 81 JUN 17, 1992 19:10:01

START

0.584
0.502
1.4
31441
2144
METANES @ 2144
ETHANE @ 215

METANES ~ 2.0ppm
ETHANE ~ 2.0ppm

RUN# 81 JUN 17, 1992 19:10:01

AREA:

RT	AREA TYPE	WIDTH	AREA%
.502	276248	PV .038	59.34565
.587	189242	VB .037	40.65435

TOTAL AREA= 465490

MUL FACTOR=1.0000E+00

* RUN # 82 JUN 17, 1992 19:13:26

START

0.584
0.502
1.2
21441
2144
METANES @ 2144
ETHANE @ 215

METANES ~ 2.0ppm
ETHANE ~ 2.0ppm

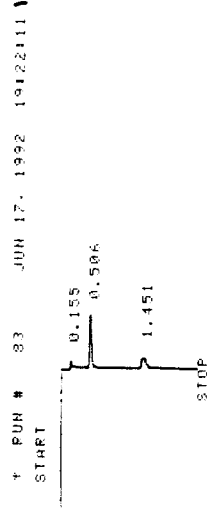
STOP

RUN# 82 JUN 17, 1992 19:13:26

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.500	328098	PV	.040	48.43776	
.595	349262	VB	.037	51.56226	

TOTAL AREA= 677360
MUL FACTOR=1.0000E+00

1:2 ON AAL 13774
ACETACONIDE 1.527mm



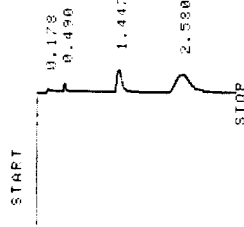
RUN# 83 JUN 17, 1992 19:22:11

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.155	11623	PB	.037	7.52366	
.506	87112	VB	.041	56.38827	
1.451	55751	PB	.112	36.08806	

TOTAL AREA= 154486
MUL FACTOR=1.0000E+00

ACETACONIDE 3.032mm

* RUN# 84 JUN 17, 1992 19:26:18

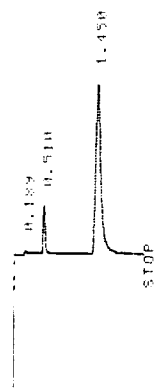


RUN# 84 JUN 17, 1992 19:26:18

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.490	13008	BB	.044	4.83666	
1.447	97849	PB	.105	26.28067	
2.580	256466	BB	.329	68.88266	

TOTAL AREA= 372323
MUL FACTOR=1.0000E+00

* RUN # 85 JUN 17, 1992 19:31:44 *1.2 Ombut*
 START *-1441 ACETALDEHYDE @ 92.9 ppm*

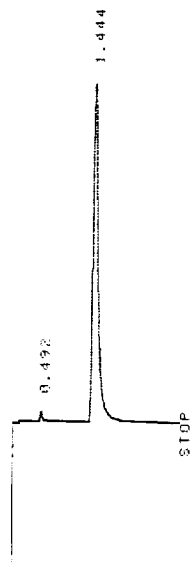


PUN# 85 JUN 17, 1992 19:31:44

AREA:				
PT	AREA	TYPE	WIDTH	AREA2
.510	70524	BB	.038	9.40715
1.450	679161	PB	.106	90.53283

TOTAL AREA=749685
 MUL FACTOR=1.0000E+00

* RUN # 86 JUN 17, 1992 19:35:05 *ANAL 1441 ACETALDEHYDE @ 94.3 ppm*
 START

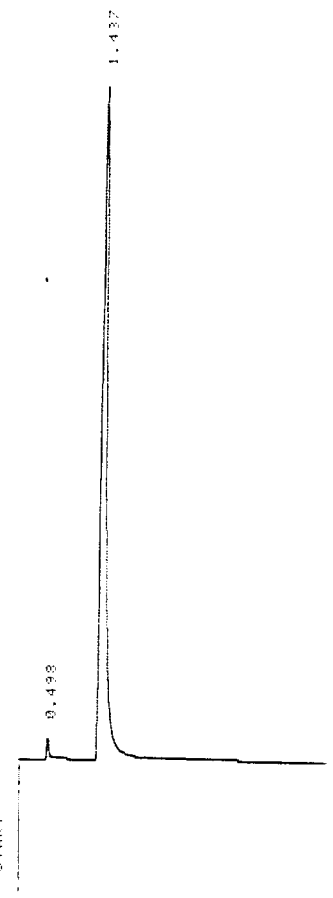


PUN# 86 JUN 17, 1992 19:35:05

AREA:				
PT	AREA	TYPE	WIDTH	AREA2
.432	18728	BB	.045	1.39540
1.444	1323395	PB	.104	98.60458

TOTAL AREA=1342123
 MUL FACTOR=1.0000E+00

* RUN # 87 JUN 17, 1992 19:39:03 *ANAL 207105 ACETALDEHYDE @ 82.5 ppm*
 START



RUN# 87 JUN 17. 1992 19:39:03

AREA:

PT	AREA TYPE	WIDTH	AREA
.498	33738	FB	.043
1.437	2604157	FB	.103

TOTAL AREA=2637894

MUL FACTOR=1.0000E+00

* RUN # 88

JUN 17. 1992

19:47:09

14 ON

ALM 018311 Ethanol @ 50 ppm

START

0.165 0.505

6.680

TIME/TABLE STOP

RUN# 88 JUN 17. 1992 19:47:09

AREA:

PT	AREA TYPE	WIDTH	AREA
.505	115632	VB	.042
6.560	273179	BB	.500

TOTAL AREA= 388670

MUL FACTOR=1.0000E+00

* RUN # 89

JUN 17. 1992

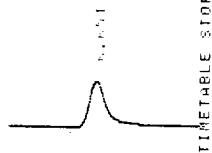
19:55:51

ALM 018311

with 100% Ethanol @ 200 ppm

START

0.491



RUN# 89 JUN 17, 1992 19:55:51

AREA%	RT	AREA	TYPE	WIDTH	HEIGHT
.491	18978	BB	.044	3.42751	
6.651	531901	VB	.313	96.57251	

TOTAL AREA= 550779
MUL FACTOR=1.0000E+00

* RUN# 90 JUN 17, 1992 20:05:31 ALM 024496 Ethanol @ 498 ppm

START



RUN# 90 JUN 17, 1992 20:05:31

AREA%	RT	AREA	TYPE	WIDTH	HEIGHT
.082	11956	BB	.034	.00439	
.493	21342	BB	.042	1.44798	
6.638	1440716	PB	.314	97.74762	

TOTAL AREA=1473314
MUL FACTOR=1.0000E+00

* RUN# 91 JUN 17, 1992 20:15:01 ALM 11908

Ethanol @ 498 ppm

0.145
1.680

6.659

TIMETABLE STOP

PUN# 91 JUN 17, 1992 20:15:01

AREA#	RT	AREA	TYPE	WIDTH	AREA%
1	0.495	23096	BV	0.043	1.1924
2	1.680	37106	PB	0.053	1.32018
3	6.659	11531848	PB	0.294	99.48864

TOTAL AREA=1.1592E+07
MUL FACTOR=1.0000E+00

+

Power failed
JUN 18, 1992 07:17:57

BREAK

* LIST: LIST
PEAK CAPACITY: 1244

ZERO = 5, 1093.306
ATT 2 = 6
CHT SP = 1.0
AP REJ = 10000
THRESH = 4
PK WD = 0.10

Power to breaker @ 12:10

*TIME 12:10:35
JUN 18, 1992 12:10:35

* TRANSFER
MOVED to 2nd location

Nitrogen @ 14 PSI ~ 1-22-1992
 Air @ 408 ml/min
 H₂ @ 30 ml/min

* LIST: LIST
 PENY CAPACITY: 1244
 ZERO = 5.47.163
 ATT 2 = 6
 CHT SP = 1.0
 AR PEJ = 10000
 THPSH = 4
 PK WD = 0.10

* ATT 2: BREAK

* RUN # 92 JUN 18, 1992 13:56:29
 START



Flow too low

RUN# 92 JUN 18, 1992 13:56:29

RT	AREA	TYPE	WIDTH	AREA2
.542	93914	VB	.053	17.70102
7.462	436643	PB	.483	82.29999

TOTAL AREA= 530557
 MUL FACTOR=1.0000E+00

Flow too low
 Adjust to 44 psi

0.136
 0.535

4.665

7.441

TIME/TABLE STOP

RUN# 93 JUN 18, 1992 14:06:09

AREA%	RT	AREA TYPE	WIDTH	AREA%
.136	15873	BB	.041	1.79258
.535	22782	VB	.048	3.13748
4.665	38849	BP	.189	3.48395
7.441	918982	PD	.516	91.58608

TOTAL AREA= 895486
 MUL FACTOR=1.0000E+00

* RUN # 94 JUN 18, 1992 14:21:13 1:1 Division Run 010001 signal @ 100psi

0.032
 0.433

6.649

TIME/TABLE STOP

RUN# 94 JUN 18, 1992 14:21:13

Flow too low

5043

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TOTAL AREA = 7,6731

MUL FACTOR=1.0000E+00

* RUN #	95	JUN 19, 1992	14:30:15
START			

3.139
3.488

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D
W
C
A

TIME TABLE STOP

FUN# 95 JUN 18, 1992 14:38:17

9938

PT	AREA	TYPE	WIDTH	AREA2
.139	11912	PB	.033	1.97308
.480	20731	VB	.042	3.43524
.634	57089	PB	.313	94.59080

TOTAL AREA= 603481
MUL FACTOR=1.00000E+00

* RUN # 36 JUN 18, 1992 14:40:55
STRT

0.139
0.429

2
3
4
5
6

TINETABLE STOP

RUN# 96 JUN 18, 1992 14:40:55

AREA#	PT	AREA TYPE	WIDTH	AREA#
	.180	13720	PV .034	.79396
	.488	21489	BB .045	1.24355
	6.620	1692831	PB .354	97.96250

TOTAL AREA=1.728040
MUL FACTOR=1.0000E+00

+ RUN # 97 JUN 19, 1992 14:50:25 ALM 011208 etand@ 1400 ppr

START	0.093	0.485
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5.105

6.634

TINETABLE STOP

RUN# 97 JUN 18, 1992 14:50:25

AREA#	PT	AREA TYPE	WIDTH	AREA#
	.093	10389	BB .031	.09277
	.485	30718	VV .045	.27483
	5.105	126380	PB .587	1.13072
	6.634	11009484	PB .294	98.50166

TOTAL AREA=1.1177E+07
MUL FACTOR=1.0000E+00

* RUN # 98 JUN 18, 1992 15:11:26 1:20:10 ppr 15:11:26 1:52:00 ppr

START



0.495

STOP

RUN# 98 JUN 18, 1992 15:11:26

AREA:

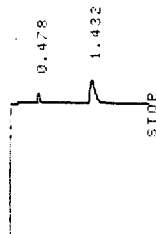
RT	AREA TYPE	WIDTH	AREA%
.495	BB	.042	66.39591
1.436	BB	.109	33.60419

TOTAL AREA= 163435

MUL FACTOR=1.0000E+00

* RUN # 99 JUN 18, 1992 15:11:34 AAL 13774 Actaldehyde @ 9.63 ppm

START



RUN# 99 JUN 18, 1992 15:11:34

AREA:

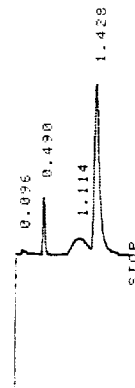
RT	AREA TYPE	WIDTH	AREA%
.478	BB	.042	15.06939
1.432	BB	.109	84.93059

TOTAL AREA= 122281

MUL FACTOR=1.0000E+00

* RUN # 100 JUN 18, 1992 15:20:06 1:2 Junior AAL 1441 Actaldehyde @ 22.2 ppm

START



RUN# 100 JUN 18, 1992 15:20:06

AREA:

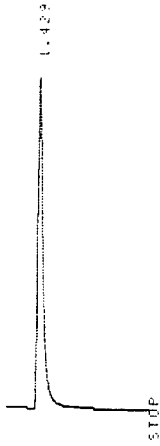
RT	AREA TYPE	WIDTH	AREA%
.490	BB	.041	9.47073
1.114	BB	.276	18.97114
1.428	BB	.109	71.55814

TOTAL AREA= 987347

MUL FACTOR=1.0000E+00

* RUN # 101 JUN 18, 1992 15:22:57 AAL 1441 Actaldehyde @ 44.3 ppm

START

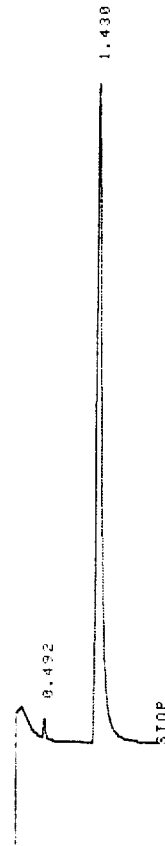


RUN# 101 JUN 18, 1992 15:22:57

AREA%
PT AREA TYPE WIDTH AREA%
.481 24718 VB .050 1.85859
1.429 1310965 BB .106 98.14941

TOTAL AREA=1335693
MUL FACTOR=1.0000E+00

* RUN # 102 JUN 18, 1992 15:26:40 ALM 003105 Act 11/10/92 @ 82.54pm



RUN# 102 JUN 18, 1992 15:26:40

AREA%
PT AREA TYPE WIDTH AREA%
.432 31834 BB .039 1.22308
1.430 2570938 BB .184 98.77692

TOTAL AREA=2682773
MUL FACTOR=1.0000E+00

* RUN # 103 JUN 18, 1992 15:31:45 14.51min
START
0.174
0.489578
STOP

Act 11/10/92 @ 82.54pm
Mettler 111488

RUN# 103 JUN 18, 1992 15:31:45

AREA%
PT AREA TYPE WIDTH AREA%
.494 312128 BV .038 47.79002
.578 340996 VB .036 52.20998

TOTAL AREA= 653124
MUL FACTOR=1.0000E+00

Act 11/10/92

519

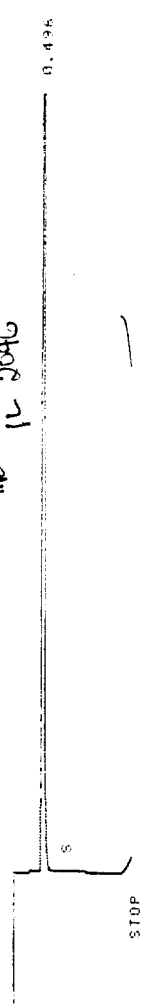
The infrared spectrum shows a broad absorption band centered around 3400 cm⁻¹, characteristic of N-H stretching in amides. There are sharp, intense peaks at approximately 1640 cm⁻¹ (C=O stretching), 1450 cm⁻¹ (C-N stretching), and 1050 cm⁻¹ (C-H stretching). The x-axis is labeled with wavenumbers in cm⁻¹, and the y-axis represents transmittance.

3015

PT	AREA	TYPE	WIDTH	AREA2
.493	1706462	SBB	.037	100.000000

Normal 2046 00.2
12 2046

* RUN # 107 JUN 18. 1992 15:43:19
START

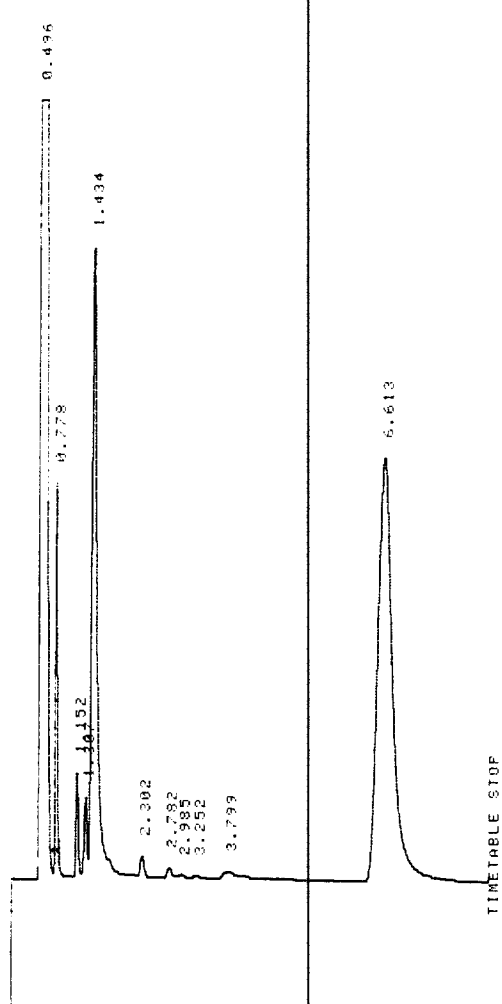


RUN# 107 JUN 18. 1992 15:43:19

AREA: PT AREA TYPE WIDTH AREA:
.496 3287250 SHB .036 100.00000

TOTAL AREA=3287250
MUL FACTOR=1.0000E+00

* RUN # 108 JUN 18. 1992 15:54:40
START

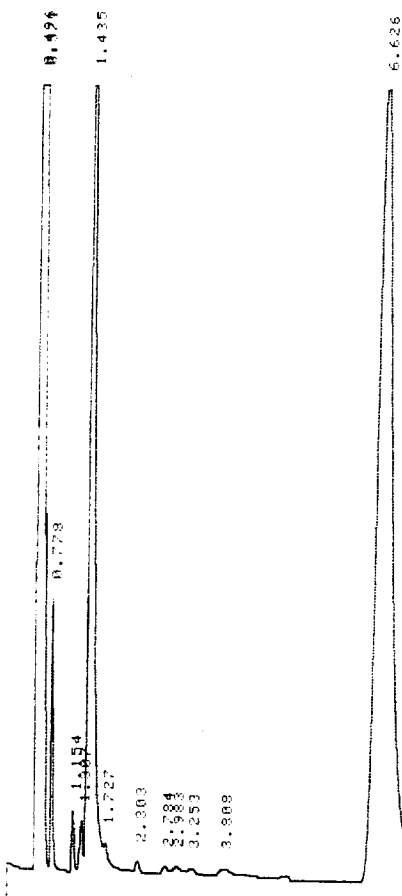


RUN# 108 JUN 18. 1992 15:54:40

AREA: PT AREA TYPE WIDTH AREA:
.496 33009636 >SPB .063 79.64006
.778 576021 BB .039 1.38372
1.152 181394 PV .046 .43764
1.207 160300 VV .055 .38674
1.434 2419359 VB .103 5.93679
2.302 66395 PB .078 .16016
2.782 44753 PV .097 .10797
2.985 26012 VV .121 .06276
3.252 29103 VP .146 .07821
3.799 119706 PV .310 .28891

TOTAL AREA=4.144E+01
 MUL FACTOR=1.0000E+00

* RUN # 109 JUN 18, 1992 16:03:35 *flow*
 START

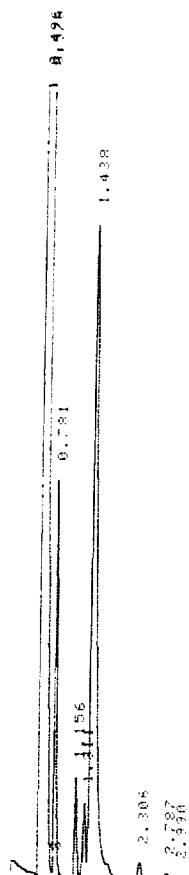


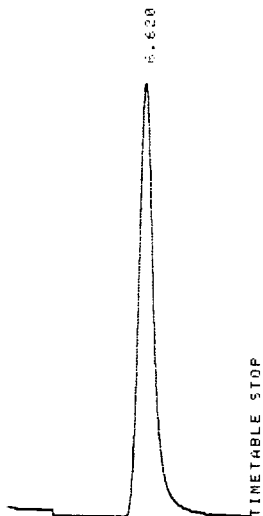
RUN# 109 JUN 18, 1992 16:03:35

RT	AREA	TYPE	WIDTH	AREA%
.496	25472032	SPB	.049	59.83581
.571	3072422	BB	.031	7.21736
.778	394949	BB	.039	.92777
1.154	112155	PV	.047	.26348
1.307	129005	VV	.055	.30304
1.435	3842582	VV	.104	9.02653
1.727	147703	VB	.130	.34537
2.303	39237	PP	.079	.09217
2.784	48951	PV	.125	.11499
2.933	64649	VV	.164	.15197
3.253	57038	VF	.163	.13399
3.808	84409	PV	.227	.19820
6.626	9104762	PB	.298	21.38779

TOTAL AREA=4.2570E+07
 MUL FACTOR=1.0000E+00

* RUN # 110 JUN 18, 1992 16:12:26 *flow*
 START





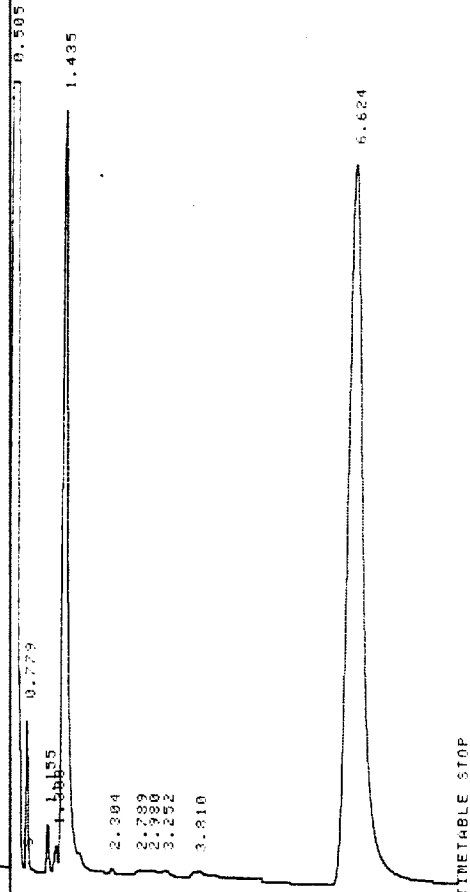
RUN# 110 JUN 18. 1992 16:12:26

AREA:

RT	APER	TYPE	WIDTH	AREA%
.496	31711728	>SBB	.061	74.58099
.576	2132760	TBB	.034	5.01591
.781	578753	BB	.038	1.36114
1.156	192045	PV	.046	.42814
1.311	161351	VV	.055	.37947
1.438	2529998	VB	.103	5.95016
2.386	65748	PF	.081	.16404
2.787	53816	BV	.106	.12657
2.998	63426	VV	.176	.14917
3.808	113904	VV	.255	.26788
6.620	4922352	PB	.302	11.57660

TOTAL AREA=4.2520E+07
MUL FACTOR=1.0000E+00

RUN # 111 JUN 18. 1992 16:21:25 FIRST
START



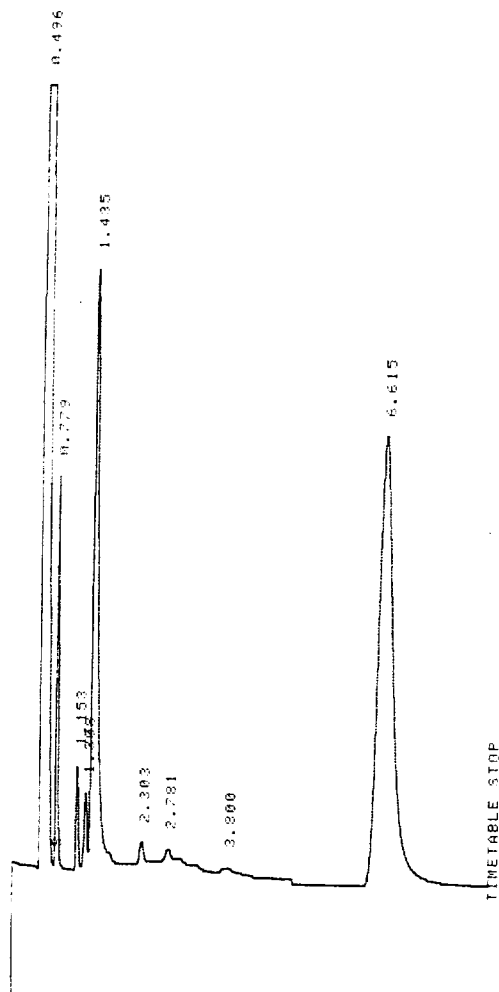
RUN# 111 JUN 18. 1992 16:21:25

AREA:

RT	AREA	TYPE	WIDTH	AREA1
1.151	88567	PV	.047	.71429
1.308	44428	VV	.065	.28845
1.435	3014845	VV	.105	.24240
2.304	25529	VB	.084	9.81896
2.789	48736	SV	.160	.08314
2.980	64775	VV	.190	.15873
3.252	68482	VV	.191	.21096
3.810	171459	VV	.441	.22304
6.624	8038707	PB	.399	.55842
				26.18103

TOTAL AREA=3.0704E+07
MUL FACTOR=1.0000E+00

* RUN # 112 JUN 18, 1992 16:30:35
START

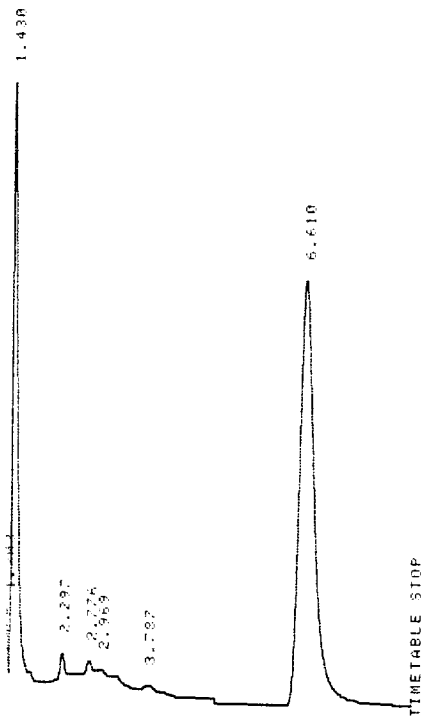


RUN# 112 JUN 18, 1992 16:30:35

RT	AREA	TYPE	WIDTH	AREA1
1.151	32819556	VB	.063	77.92291
1.308	569890	VB	.039	1.35307
1.435	190894	PV	.047	.45321
2.303	179026	VV	.059	.42505
2.781	241274	VV	.106	5.72856
3.252	245416	VV	.187	.58268
3.800	335073	VV	.303	.79555
6.615	254364	VV	.462	.60535
	5110506	PB	.302	12.13367

TOTAL AREA=4.2118E+07
MUL FACTOR=1.0000E+00

* RUN # 113 JUN 18, 1992 16:39:30
START



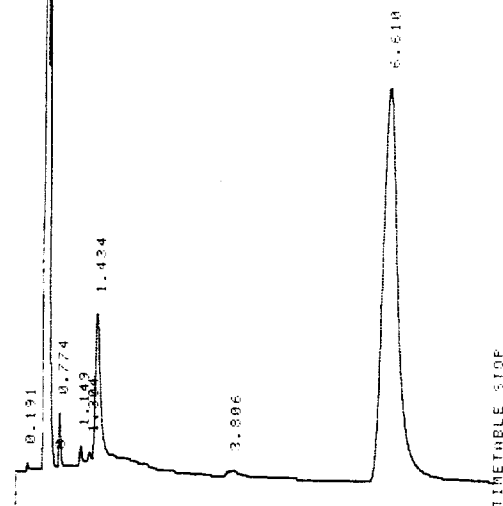
RUN# 113 JUN 18, 1992 16:39:30

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.488	33955168	SBB	.065	77.63885	
.773	607215	B0	.039	1.38840	
1.148	204059	BV	.049	.46659	
1.303	193628	VV	.059	.44845	
1.438	2462762	VV	.107	5.63113	
2.297	419204	VV	.247	.95851	
2.776	482775	VV	.332	1.10387	
2.969	271742	VV	.233	.62134	
3.787	327053	VV	.481	.74781	
6.610	4812195	P0	.301	11.00314	

TOTAL AREA=4.3735E+07
NUL FACTOR=1.0000E+00

Real

* RUN # 114 JUN 18, 1992 16:49:28
STRT 0.191 0.774 1.434 3.906 5.610 9.499

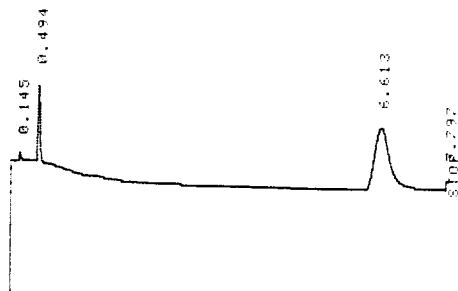


PUN# 111 JUN 18, 1992 16:49:28

AREA:	RT	AREA	TYPE	WIDTH	AREA:
	.191	11857	BB	.033	.09570
	.499	711914	SHB	.039	57.46502
	.274	79959	BB	.038	.64535
	1.149	30607	PV	.044	.24703
	1.304	21944	VV	.055	.17711
	1.434	589026	VB	.105	4.75405
	3.906	74972	FB	.238	.60510
	6.610	4461712	FB	.302	36.01062

TOTAL AREA=1.2390E+07
MUL FACTOR=1.0000E+00

* RUN # 115 JUN 18, 1992 16:59:47
START



PUN# 115 JUN 18, 1992 16:59:47

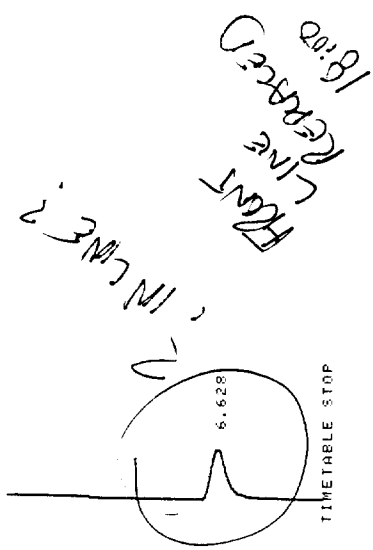
AREA:	RT	AREA	TYPE	WIDTH	AREA:
	.145	11328	BB	.033	1.24999
	.494	123607	VB	.041	13.63942
	6.613	750719	FB	.311	82.83814
	7.797	20594	FB	.048	2.27245

TOTAL AREA= 906248
MUL FACTOR=1.0000E+00

* RUN # 116 JUN 18, 1992 17:08:10
START



WENTHAW@2000 8/15/92

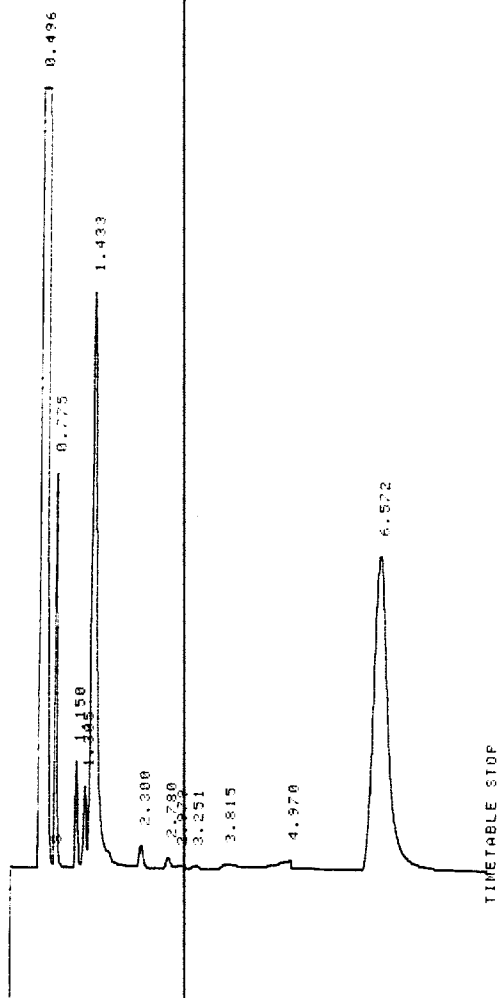


PUN# 116 JUN 18. 1992 17:08:30

AREA%	RT	AREA TYPE	WIDTH	AREA%
	.496	31632192 >SBB	.061	98.18269
	6.628	593506 PB	.311	1.91734

TOTAL AREA=3.2210E+07
MUL FACTOR=1.0000E+00

* PUN# 117 JUN 18. 1992 17:22:56
START



PUN# 117 JUN 18. 1992 17:22:56

AREA%	RT	AREA TYPE	WIDTH	AREA%
	.496	33276128 >SBB	.064	92.38867
	.775	592001 BB	.039	1.46574
	1.150	189893 PV	.046	.47013
	1.305	166375 VV	.055	.41193
	1.433	2230545 VB	.104	5.52297

TIME/ABLE STOP

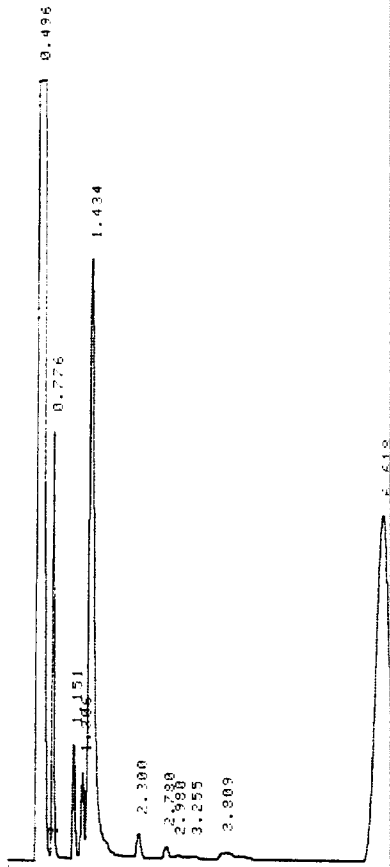
RUN# 119 JUN 18, 1992 17:43:59

AREA% RT AREA TYPE WIDTH AREA%
 .479 70087 PB .033 100.00000

TOTAL AREA= 70087
 MUL FACTOR=1.0000E+00

DEA

* RUN # 120 JUN 18, 1992 17:53:15
 START



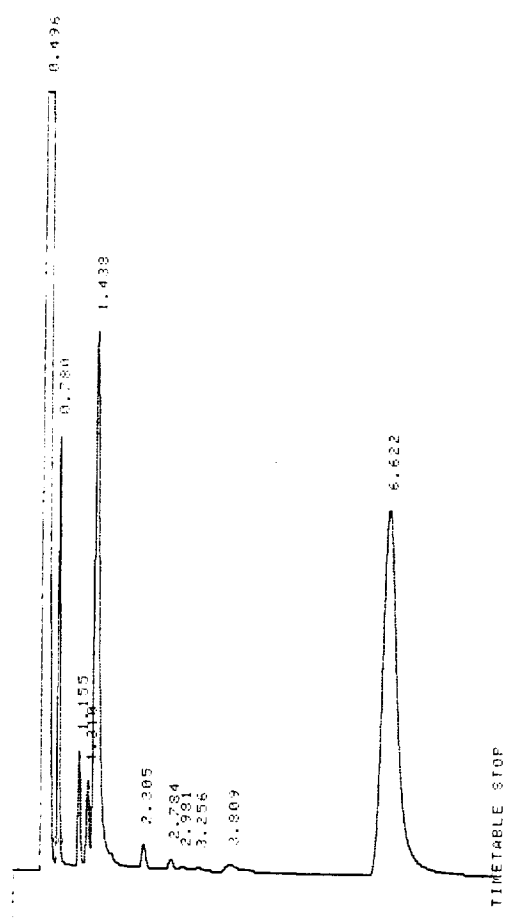
TIME/ABLE STOP

RUN# 120 JUN 18, 1992 17:53:15

AREA% RT AREA TYPE WIDTH AREA%
 .496 34161344 SPB .066 81.92771
 .776 630921 BB .033 1.51311
 1.151 201429 PV .046 .48308
 1.306 172079 VV .054 .41269
 1.434 2286022 VB .102 5.48247
 2.300 77565 BP .081 .18602
 2.780 49316 BV .098 .11827
 2.990 27933 VV .125 .06699
 3.255 30145 VP .150 .07230
 3.809 105802 PP .294 .25374
 6.618 3954415 PB .304 9.48371

TOTAL AREA=4.1637E+07
 MUL FACTOR=1.0000E+00

* RUN # 121 JUN 18, 1992 18:04:20 *Peak*
 STOP

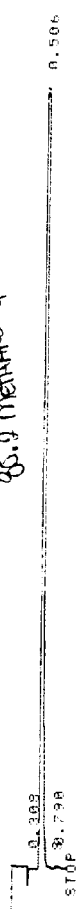


RUN# 121 JUN 18, 1992 18:04:20

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.496	33956192	SPB	.065	81.84685	
.780	626630	BB	.039	1.51041	
1.155	202648	PV	.046	.48946	
1.310	173679	VV	.055	.41863	
1.439	2057213	VB	.103	4.95864	
2.305	79981	VF	.083	.19259	
2.784	49465	PV	.098	.11682	
2.981	25752	VV	.122	.06287	
3.256	32103	VP	.154	.07738	
3.809	182847	PV	.239	.24790	
6.622	4182096	PB	.304	10.00039	

TOTAL AREA=4.1482E+07
 MUL FACTOR=1.0000E+00

* RUN # 122 JUN 18, 1992 18:17:45 *Front Peak Trace*
 STOP *95.9 Methane QC Check*



RUN# 122 JUN 18, 1992 18:17:45

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.308	33227	PB	.059	1.02849	
.506	3197429	SPB	.036	98.97149	

TOTAL AREA=3230654

20020608
JUN 18 1992
THERM 123

* RUN # 123 JUN 18, 1992 18:19:50

START

0.505

00.790

STOP

RUN# 123 JUN 18, 1992 18:19:50

AREA:

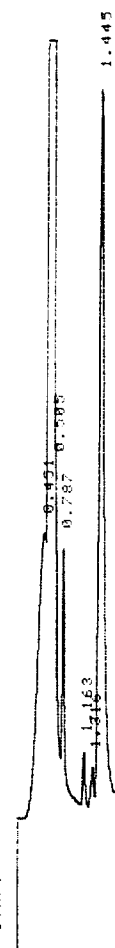
RT	AREA	TYPE	WIDTH	AREA%
.505	3242742	SB	.036	99.59981
.790	13030	BB	.040	.40021

TOTAL AREA=3255773

MUL FACTOR=1.0000E+00

* RUN # 124 JUN 18, 1992 18:23:55

START



TIME/TABLE STOP

RUN# 124 JUN 18, 1992 18:23:55

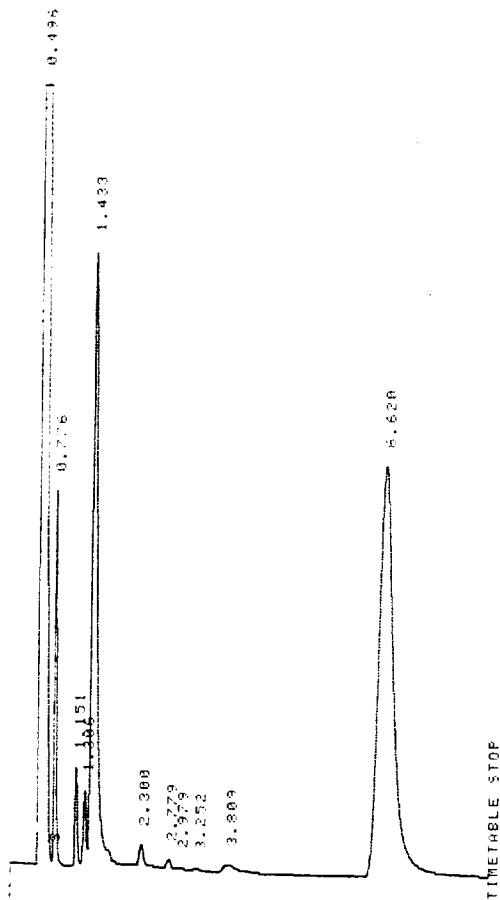
AREA:

RT	AREA	TYPE	WIDTH	AREA%
.451	1562939	BB	.154	3.96852
.505	28875520	SB	.056	68.90742
.787	313730	TBB	.038	.74882
1.163	93668	TBF	.046	.22353
1.316	94346	TFV	.059	.22514
1.445	2820514	TVV	.104	6.73076
2.321	42932	TFV	.080	.10245
2.561	677739	TFV	.314	1.61733
3.266	44167	TVB	.162	.10540
3.810	91114	BF	.274	.21743
5.640	7189048	FB	.300	17.15327

REAL

* RUN # 125 JUN 18, 1992 18:33:35

START



RUN# 125 JUN 18, 1992 18:33:35

AREA%

RT	AREA	TYPE	WIDTH	AREA%
.496	32699328	>SBB	.063	79.91069
.776	552866	BB	.039	1.36333
1.151	175104	PV	.046	.42792
1.306	153913	VV	.056	.37589
1.433	2372341	VB	.103	5.79760
2.300	83628	BB	.095	.20437
2.779	39686	BV	.093	.09699
2.979	18069	VV	.106	.04416
3.252	20089	VF	.122	.05105
3.809	118987	PV	.301	.29054
6.628	4680170	PB	.303	11.43754

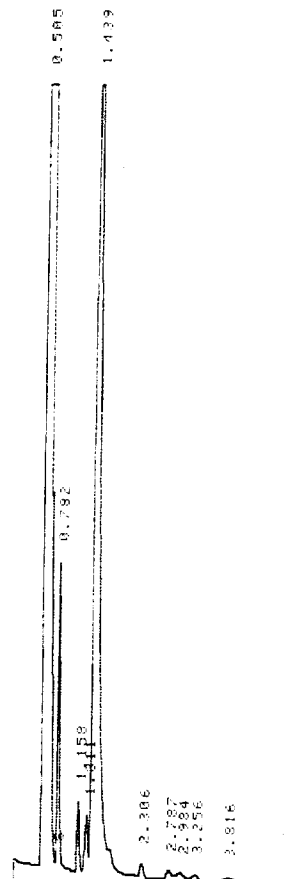
TOTAL AREA=4.0919E+07

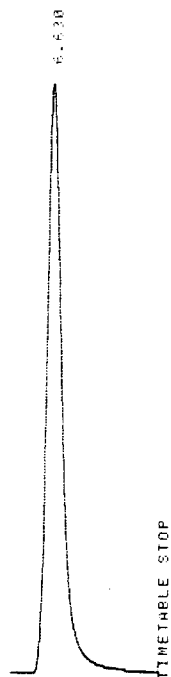
MUL FACTOR=1.0000E+00

FRONT

* RUN # 126 JUN 18, 1992 18:42:35

START



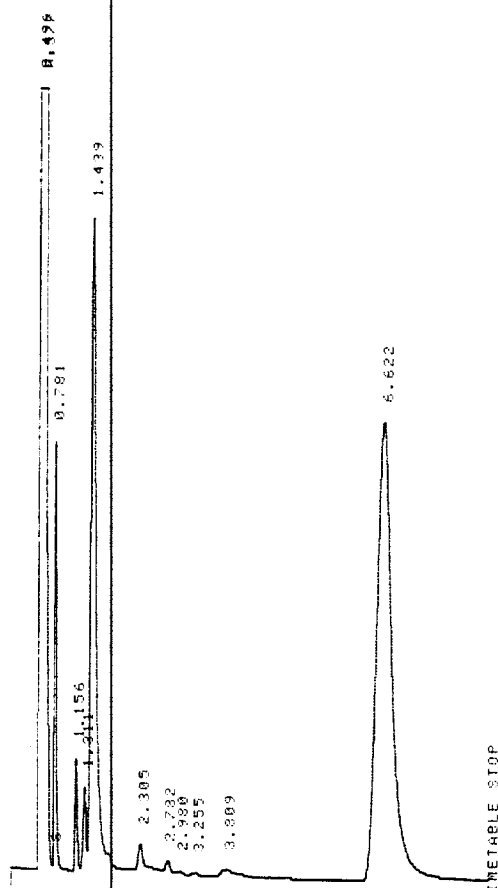


RUN# 126 JUN 18, 1992 18:42:35

AREA%	PT	AREA	TYPE	WIDTH	AREA%
.505	31509840	>SB		.061	72.82195
.792	459797	BB		.039	1.05339
1.159	131918	PV		.047	.30487
1.311	142348	VV		.063	.32898
1.439	4842120	VV		.104	9.34168
2.306	48949	VB		.080	.11313
2.787	52270	VV		.116	.12080
2.994	63816	VV		.161	.14564
3.256	55968	VP		.152	.12935
3.816	68994	PV		.223	.15920
4.899	58428	BB		.210	.11654
6.630	6648192	PB		.302	15.36454

TOTAL AREA=4.3270E+07
MUL FACTOR=1.0000E+00

* RUN # 127 JUN 18, 1992 18:52:08
START



RUN# 127 JUN 18, 1992 18:52:08

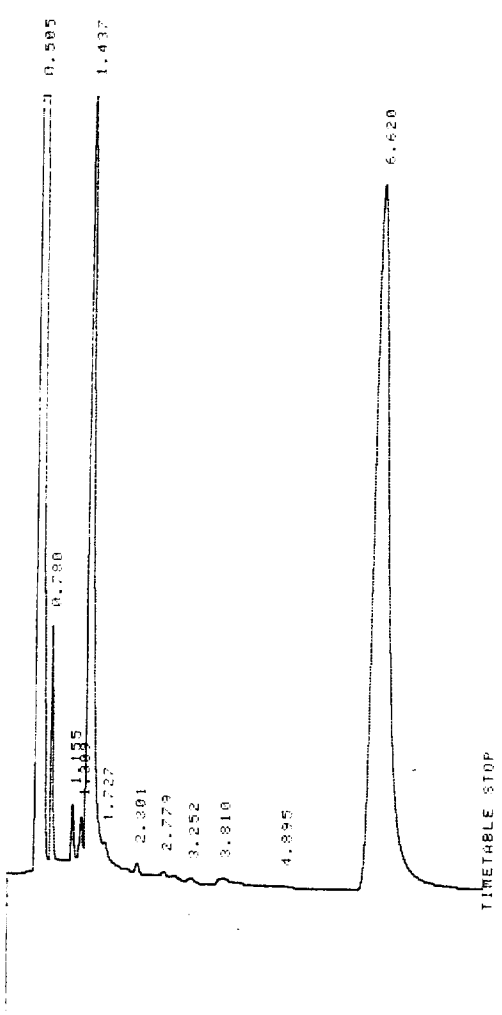
AREA%	PT	AREA	TYPE	WIDTH	AREA%
.496	32361392	>SB		.062	24.11434
.577	2218250	TBB		.034	5.09025

1.433 2523670 VV .105 5.89424
 2.305 33048 PB .093 .21310
 2.792 41450 BV .090 .09493
 2.990 17112 VP .099 .03919
 3.255 21567 PP .115 .04952
 3.809 114606 PV .301 .26265
 6.622 5302461 PB .302 11.91472

TOTAL AREA=4.3654E+07
 MUL FACTOR=1.0000E+00

7/10/87

* RUN # 129 JUN 19. 1992 19:01:20
 START



TINETABLE STOP

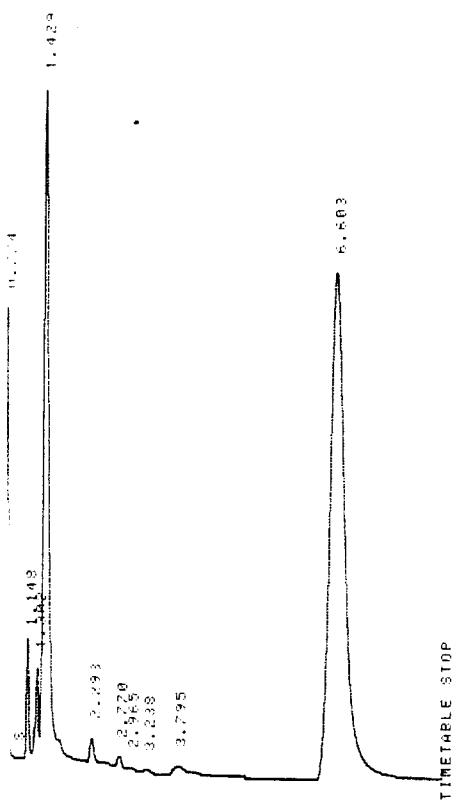
RUN# 129 JUN 19. 1992 19:01:20

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.505	27168160	3580		.052	59.41459
.780	348147	1839		.039	.09951
1.155	113637	TVV		.051	.29034
1.309	121783	TVV		.066	.31116
1.437	3148768	TVV		.105	8.04509
1.727	113751	TVR		.116	.29063
2.301	33521	BP		.077	.08565
2.779	35923	VV		.111	.09196
3.252	25514	VP		.110	.08519
3.810	114473	PV		.318	.29248
4.895	32431	VB		.217	.08286
6.620	5982832	PB		.299	20.14061

TOTAL AREA=3.9139E+07
 MUL FACTOR=1.0000E+00

* RUN # 129 JUN 19. 1992 19:10:45
 START

ARC



RUN# 129 JUN 18, 1992 19:10:45

AREA%	RT	AREA	TYPE	WIDTH	WPEAK
.499	35295024	>SB8		.069	79.31165
.774	662360	TBB		.039	1.48559
1.148	221579	BV		.049	.49177
1.382	208135	VV		.059	.46194
1.429	2655690	VV		.105	5.91624
2.293	79826	BB		.091	.17717
2.778	44050	BV		.090	.09776
2.965	15219	VF		.096	.03378
3.238	19765	FF		.110	.04387
3.795	115911	FF		.284	.25725
5.803	5732653	PB		.302	12.72308

TOTAL AREA=4.58575E+02
MUL FACTOR=1.0000E+00

dc check
800 ppm Methanol-EtOH

* RUN # 130 JUN 18, 1992 19:20:25
START



RUN# 130 JUN 18, 1992 19:20:25

AREA%	RT	AREA	TYPE	WIDTH	WPEAK
.496	23985994	>SB8		.046	99.87626
.779	29717	TBB		.042	.12374

TOTAL AREA=2.4015E+07
MUL FACTOR=1.0000E+00

dc check Methanol-EtOH
800 ppm

* RUN # 131 JUN 18, 1992 19:22:25

80.779
STOP

PUN# 131 JUN 18, 1992 19122125

AREA:

RT	AREA	TYPE	WIDTH	AREA
.496	24029280	>SBB	.046	99.90010
.779	22105	BB	.030	.09191

TOTAL AREA=2.4051E+07
MUL FACTOR=1.0000E+00

1996 November 26 12:02 PM

* PUN # 132 JUN 18, 1992 19124145
START

0.780

STOP

0.496

PUN# 132 JUN 18, 1992 19124145

AREA:

RT	AREA	TYPE	WIDTH	AREA
.496	30487504	>SBB	.059	99.47021
.790	153922	BB	.030	.52181

TOTAL AREA=3.0647E+07
MUL FACTOR=1.0000E+00

*

Power failed

JUN 18, 1992 19126107

BREAK

* PUN # 133 JUN 18, 1992 19126130
START

1996 November 26 12:02 PM

0.774 STOP

0.194

PUN# 133 JUN 18, 1992 19126130

AREA:

RT	AREA	TYPE	WIDTH	AREA
.184	20605776	BB	.237	41.01874
.498	29654448	>VB	.059	58.80310
.774	89948	BB	.022	.17816

134 # 134
134 # 134

JUN 19. 1992 19129144

292.0

9.439

PUHH 134 JUN 18. 1992 19129144

4334

PT	AREA	TYPE	WIDTH	AREA:
.480	30570240	>SBB	.059	99.45565
.767	167324	BB	.039	54.436

TOTAL AREA=3.0739E+07
MUL FACTOR=1.0000E+00

```
* RUN # 135 JUN 18, 1992 19132140
START
```

STOP

19. 4. 9. 19

135 JUN 18. 1992 19:32:48

REAR

RT	AREA	TYPE	WIDTH	AREA%
4.88	35030752	SPB	.967	100.00000

TOTAL AREA=3.5031E+07
MUL FACTOR=1.0000E+00

RUN # 136 JUN 18, 1992 13:35:13
TAPT

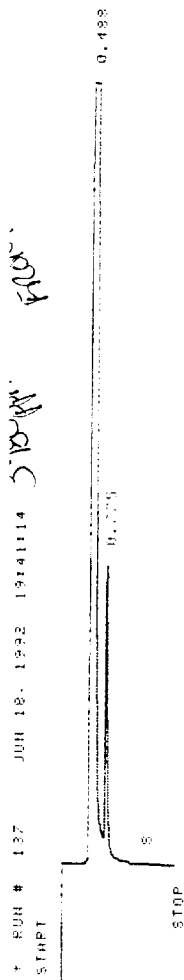
483

UIN #	136	JUN 12, 1992	12135113
UIN #	136	JUN 12, 1992	12135113

23

RT	AREA	TYPE	WIDTH	AREA
1.488	33581376	5888	.065	98.82160
1.736	10114	88	.037	.03123
1.134	389841	188	.329	1.14730

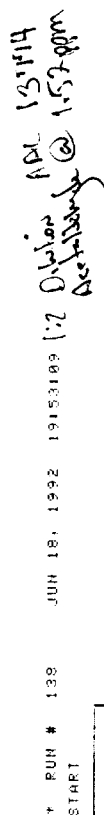
OTOL WREA=3.3982E+07
UL FACTOR=1.0000E+00



RUN# 137 JUN 18, 1992 19:41:14

AREA%	RT	WPEA	TYPE	WIDTH	WPEA%
.488	394.8880	.868		.076	98.96499
.775	412.79	TBB		.038	1.03581

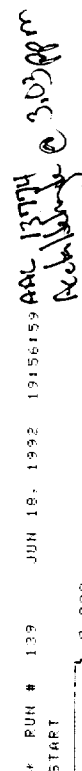
TOTAL AREA=3.9892E+07
MUL FACTOR=1.0000E+00



RUN# 138 JUN 18, 1992 19:53:09

AREA%	RT	WPEA	TYPE	WIDTH	WPEA%
.492	92756	BB		.046	64.65493
1.425	58685	BP		.110	35.33509

TOTAL AREA= 143441
MUL FACTOR=1.0000E+00

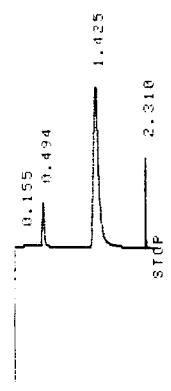


RUN# 139 JUN 18, 1992 19:56:59

AREA%	RT	WPEA	TYPE	WIDTH	WPEA%
.481	17247	BP		.039	14.29637
1.429	103392	FB		.112	85.70362

TOTAL AREA= 120639

* PUN # 140 JUN 18, 1992 20100127 1:2 Major and 7441
 Detailing @ 22.7 ppm

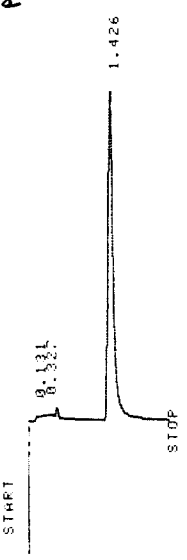


PUN# 140 JUN 18, 1992 20100127

AREA	PT	AREA	TYPE	WIDTH	AREA
.494	71165	BB	.040	9.50710	
1.425	643299	PB	.105	85.93981	
2.310	34092	BB	.017	4.55309	

TOTAL AREA=748546
 MUL FACTOR=1.0000E+00

* PUN # 141 JUN 18, 1992 20103120 441
 Detailing @ 14.3 ppm

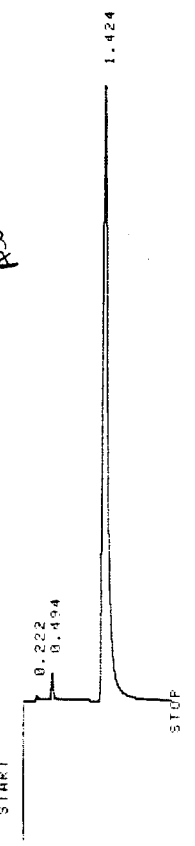


PUN# 141 JUN 18, 1992 20103120

AREA	PT	AREA	TYPE	WIDTH	AREA
.131	11917	PV	.054	.84807	
.327	111740	VV	.360	7.94414	
1.426	1283107	PB	.103	91.21578	

TOTAL AREA=1406672
 MUL FACTOR=1.0000E+00

* PUN # 142 JUN 18, 1992 20110149 007115
 Detailing @ 22.5 ppm



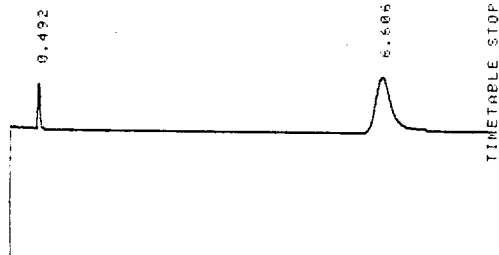
PUN# 142 JUN 18, 1992 20110149

.494 49437 PB .844 2.01924
 1.424 239956 PB .103 97.98077

TOTAL AREA=249302
 MUL FACTOR=1.0000E+00

*ALM 03:44:46
 1:2 Nitro
 2/24/92 @ 2:44 PM
 2/24/92*

* RUN # 143 JUN 18, 1992 20:17:32
 START



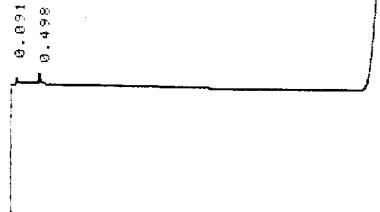
RUN# 143 JUN 18, 1992 20:17:32

AREA%	RT	AREA	TYPE	WIDTH	AREA%
.492	73590	BB	.842	9.48611	
6.606	702080	PB	.345	98.51389	

TOTAL AREA= 775660
 MUL FACTOR=1.0000E+00

*ALM 03:44:46
 2/24/92 @ 1:48 PM*

* RUN # 144 JUN 18, 1992 20:26:31
 START



TIMETABLE STOP

RUN# 144 JUN 18. 1992 20125131

AREA: RT AREA TYPE WIDTH AREA
 .498 17729 VB .839 1.23803
 6.625 1414394 PB .307 98.76195

TOTAL AREA=1432033
 MUL FACTOR=1.0000E+00

* RUN # 145 JUN 18. 1992 20135159 ACN 011203 4000 f
 START

0.939
 0.486

6.625

TIMETABLE STOP

RUN# 145 JUN 18. 1992 20135159

AREA: RT AREA TYPE WIDTH AREA
 .039 10686 BB .834 .09794
 .486 26266 VB .849 .24073
 6.625 10074024 PB .292 99.66131

TOTAL AREA=1.0911E+07
 MUL FACTOR=1.0000E+00

* RUN # 145 JUN 18. 1992 20147125 ACN 21441
 START

0.487

0.580

STOP

RUN# 146 JUN 18, 1992 20147125

AREA:

PT	AREA TYPE	WIDTH	AREA
.495	441687 BV	.036	39.17835
.500	685689 VB	.035	60.82165

TOTAL AREA=1127375

MUL FACTOR=1.0000E+00

* RUN # 147 JUN 18, 1992 20150128 11-2046
START
METHANE @ 40.1

0.495

STOP

RUN# 147 JUN 18, 1992 20150128

AREA:

PT	AREA TYPE	WIDTH	AREA
.495	1699663 SBB	.036	100.00000

TOTAL AREA=1699663

MUL FACTOR=1.0000E+00

* RUN # 148 JUN 18, 1992 20152132 11-2046
START

METHANE @ 30.2 ppm

0.494

1.521

STOP

RUN# 148 JUN 18, 1992 20152132

AREA:

PT	AREA TYPE	WIDTH	AREA
.494	3241046 SFB	.036	92.39174
1.521	266893 BV	.416	7.60826

TOTAL AREA=3507939

MUL FACTOR=1.0000E+00

* RUN # 149 JUN 18, 1992 20156120 AC-402
START
METHANE @ 1771 ppm

0.130

0.775

STOP

0.499

AREA%
PT AREA TYPE WIDTH AREA%
.498 7103085 ISBP .036 98.64880
.775 97292 TBF .207 1.35121

TOTAL AREA=7200378
MUL FACTOR=1.0000E+00

* RUN # 150 JUN 18, 1992 21:00:38 1/2 DL ALM-011031
START METHANE @ 397 ppm

0.169
30.770
STOP

0.495

RUN# 150 JUN 18, 1992 21:00:38

AREA%
PT AREA TYPE WIDTH AREA%
.495 15605400 SBB .036 100.00000

TOTAL AREA=1.5605E+07
MUL FACTOR=1.0000E+00

* RUN # 151 JUN 18, 1992 21:02:54 ALM-511031
START METHANE @ 798 ppm

30.770

0.499

STOP

RUN# 151 JUN 18, 1992 21:02:54

AREA%
PT AREA TYPE WIDTH AREA%
.498 24621344 >SPB .047 99.92410
.770 19706 BB .037 .07592

TOTAL AREA=2.4640E+07
MUL FACTOR=1.0000E+00

* RUN # 152 JUN 18, 1992 21:06:01 ALM-511031
START METHANE @ 800 ppm

30.771
1.252
STOP

0.499

PUN# 153 JUN 18, 1992 21:03:18

AREA:

PT	AREA TYPE	WIDTH	AREA
.488	33275424	.064	99.67600
1.252	108491	.025	.32401

TOTAL AREA=3.3484E+07
MUL FACTOR=1.0000E+00

*Wentworth @ 240000
MAY 1992*

* PUN# 153 JUN 18, 1992 21:03:18

START

0.773 0.488

STOP

PUN# 153 JUN 18, 1992 21:03:18

AREA:

PT	AREA TYPE	WIDTH	AREA
.488	39522436	.076	98.95218
.773	416500	.038	1.04284

TOTAL AREA=3.9939E+07
MUL FACTOR=1.0000E+00

* LIST: LIST

PEAK CAPACITY: 1244

ZERO = 5.0341

ATT 2 = 6

CHT SP = 1.0

AR PEJ = 10000

THRESH = 4

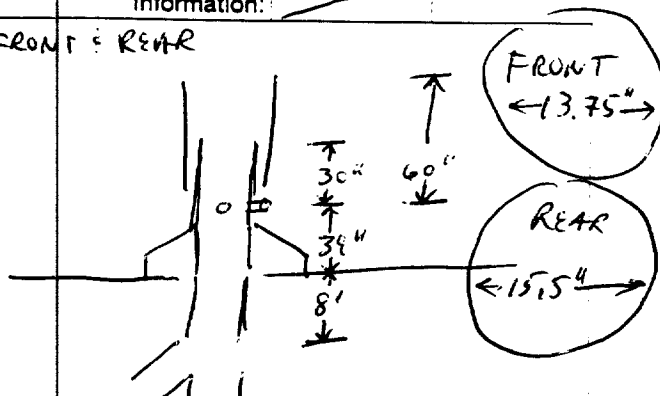
PK WD = 0.10

Appendix B.5

Field Flow Measurements Data Sheets

Traverse Point Location Form

Plant	SIREZ	Sample Ports	Number	I.D. (in)
Date	6/17	Information:		
Sampling Location	LINE 3 BREAD	FRONT - REAR		
Total Duct Depth (Distance A)				
(Inside Far Wall to Outside of Nipple/Port)				
Nipple/Port Length (Distance B)				
(Inside Near Wall to Outside End of Nipple/Port)				
Stack Depth (Dist A - Dist B)				
Stack Width (If rectangular)				
Nearest Upstream Disturbance	2.5'			
Nearest Downstream Disturbance	11.25'			
Calculator	8	CAP		



**Schematic of Sampling Location
(Cross Section of Duct)**

[illegible]

FRONT

Traverse Point Location Form

Plant	SITE 2	Sample Ports	Number	I.D. (in)
Date	6/16	Information:		
Sampling Location	L/NE 2 BRIDG REAR			
Total Duct Depth (Distance A)				
(Inside Far Wall to Outside of Nipple/Port)				
Nipple/Port Length (Distance B)				
(Inside Near Wall to Outside End of Nipple/Port)				
Stack Depth (Dist A - Dist B)				
Stack Width (If rectangular)				
Nearest Upstream Disturbance	28" (1.4 diam)			
Nearest Downstream Disturbance	24' (3 diam)			
Calculator				

From
From

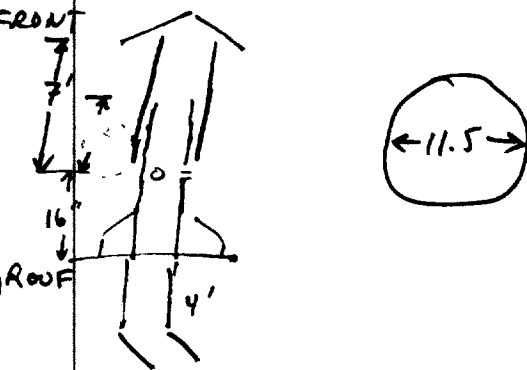
**Schematic of Sampling Location
(Cross Section of Duct)**

[illegible]

Traverse Point Location Form

Plant	SITE 2	Sample Ports	Number	I.D. (in)
Date	6/16	Information:		
Sampling Location	LINE 2 BREAD - FRONT			
Total Duct Depth (Distance A)				
(Inside Far Wall to Outside of Nipple/Port)				
Nipple/Port Length (Distance B)				
(Inside Near Wall to Outside End of Nipple/Port)				
Stack Depth (Dist A - Dist B)				
Stack Width (If rectangular)				
Nearest Upstream Disturbance	11' (0.96 diam)			
Nearest Downstream Disturbance	6.5' (5.6 diam)			
Calculator				

From
From



**Schematic of Sampling Location
(Cross Section of Duct)**

[illegible]

Traverse Point Location Form

Plant	Site 2	Sample Ports	Number	I.D. (in)
Date	6/16	Information:		
Sampling Location	LIVE 1 (BUN) FRONT			
Total Duct Depth (Distance A)				
(Inside Far Wall to Outside of Nipple/Port)				
Nipple/Port Length (Distance B)				
(Inside Near Wall to Outside End of Nipple/Port)				
Stack Depth (Dist A - Dist B)				
Stack Width (If rectangular)				
Nearest Upstream Disturbance	2' (2 diam)			
Nearest Downstream Disturbance	9' (9 diam)			
Calculator				

**Schematic of Sampling Location
(Cross Section of Duct)**

[illegible]

PRELIMINARY VELOCITY TRAVERSE

PLANT Stoehmanns
DATE 6/19
LOCATION LINE 1 FRONT
INSIDE STACK DIMENSIONS 12
BAROMETRIC PRESSURE in. Hg _____
STACK GAUGE PRESSURE in. H₂O - 0.10
OPERATOR _____

~ 1630 km

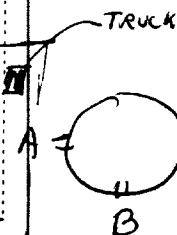
Fyrate 19 oz
2.0 CO₂

TRAVERSE POINT NUMBER	VELOCITY HEAD (ΔP_s), in. H_2O	STACK TEMPERATURE ($^{\circ}F$)
A1	0.15	266
2	0.14	273
3	0.12	269
4	0.11	267
At 1, all the way in.		

St. I, all the way in

AVERAGE

Revisión: 3/90



SCHEMATIC OF TRAVERSE POINT LAYOUT

[illegible]

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

PRELIMINARY VELOCITY TRAVERSE

A hand-drawn diagram showing a truck on the left and a car on the right, both on a road. The truck is labeled 'TRUCK' and has a rectangular body and a curved roof. The car is labeled 'A' and has a rounded body and a curved roof. A dashed vertical line is drawn between the truck and the car.

Fyrite 18.5 O₂
1 CO₂

[illegible][illegible]

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

AVERAGE

TRUCK

14.50
b240h

SCHEMATIC OF TRAVERSE POINT LAYOUT

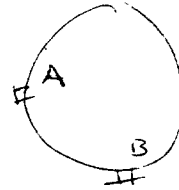
[illegible]

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

AVERAGE

PRELIMINARY VELOCITY TRAVERSE

TRUCK



18:40 hrs

AVERAGE

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

6-16

PRELIMINARY VELOCITY TRAVERSE

PLANT Strochmanns
DATE 6/19
LOCATION LINE 3 - FRONT
INSIDE STACK DIMENSIONS 13.75"
BAROMETRIC PRESSURE in. Hg _____
STACK GAUGE PRESSURE in. H₂O -0.25
OPERATOR CBP

17:00 hrs

Fyrite 19.5 O₂
0.5 CO₂

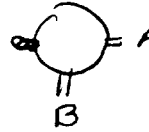
[illegible]

AVERAGE

Revision: 3/90

6-16

TRUCK



SCHEMATIC OF TRAVERSE POINT LAYOUT

[illegible]

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

PRELIMINARY VELOCITY TRAVERSE

PLANT Strochmanns
DATE 6/19
LOCATION LINE 3 REAR
INSIDE STACK DIMENSIONS 15.5
BAROMETRIC PRESSURE in. Hg _____
STACK GAUGE PRESSURE in. H₂O -0.15
OPERATOR CRP

1800 hrs

SCHEMATIC OF TRAVERSE POINT LAYOUT

[illegible][illegible]

Figure 6-6. Preliminary Velocity and Cyclonic Flow Sheet.

Appendix B.6
Field H2O Data Sheets

SITE 2
LINE 3 - FRONT
N-34
BOX Y = 0.8947
14.8 wds entrance

Plant Stoehrmanns
 Location LINE 3 FRONT
 Operator CAP
 Date 6/19/4
 Run No. _____
 Ambient temperature 88 F0
 Barometric pressure _____
 Probe length in (ft) 3

Traverse point number	Sampling time (t), min.	Stack temperature °C (°F)	Pressure differential across orifice meter ΔH mm (in.) H ₂ O	Meter reading gas sample volume m³ (ft³)	ΔV _m m³ (ft³)	Gas Sample temperature at dry gas meter		Temperature of gas leaving condenser or last impinger °C (°F)
						Inlet (T _{m,i}). °C (°F)	Outlet (T _{m,o}). °C (°F)	
	1725	220	1.5	570.790		80	79	
	1730	-	1.6	574.1		80	84	
	1738	-	1.6	579.		82	89	
	1745	-	-	584.471		-	-	
Total					Avg.			
Average						Avg.	Avg.	

SITE 2
LINE 2 - FRONT
Box N-39
Y = 0.9947

SCHEMATIC OF STACK CROSS SECTION

Traverse point number	Sampling time (9), min.	Stack temperature °C (°F)	Pressure differential across orifice meter ΔH mm (in.) H ₂ O	Meter reading gas sample volume m ³ (ft ³)	ΔV_m m ³ (ft ³)	Gas Sample temperature at dry gas meter		Temperature of gas leaving condenser or last impinger °C (°F)
						Inlet (T _{inlet}), °C (°F)	Outlet (T _{outlet}), °C (°F)	
	1607	238	1.5	479.616		86	86	
	1612	240	1.5	482.7		87	87	
	1620	243	0.8	486.9		90	88	
	1622	-	1.2	488.15		88	87	
	1622	-	-	493.972		-	-	
Total								
Average								

FIELD MOISTURE DETERMINATION REFERENCE METHOD

SITE 2

Plant Strochmums

Location LINE 2 REAR

Operator GP

Date 6/18

Run No. 2

Ambient temperature 80

Barometric pressure

Probe length in (ft) 3

INITIAL LEAK $\checkmark = 0.004 @ 10'$

FINAL LEAK $\checkmark = 0.004 @ 5'$



SCHEMATIC OF STACK CROSS SECTION

24.2 mls entrans

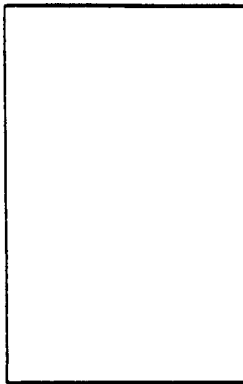
Traverse point number	Sampling time (H), min.	Stack temperature °C (°F)	Pressure differential across orifice meter ΔH mm (in.) H ₂ O	Meter reading gas sample volume m ³ (ft ³)	ΔV_m m ³ (ft ³)	Gas Sample temperature at dry gas meter		Temperature of gas leaving condenser or last impinger °C (°F)
						Inlet (T _{inlet}), °C (°F)	Outlet (T _{outlet}), °C (°F)	
	1659	300	1.7	494.110		87	87	
	1704	304	1.7	497.65		88	87	
	1728	365	1.4	512.5		90	88	
	1730	-	-	513.737		-	-	
Total								
Average						Avg.	Avg.	

Figure 6-9. Method 4 Field Data Sheet.

FIELD MOISTURE DETERMINATION REFERENCE METHOD

SIDE 2
LINE 1 - FRONT
N-39
Y = 0.9947

31.0 wds entrained



Plant Strohm, W. M. S.
Location LINE 1 - FRONT
Operator cap
Date 6/18
Run No. 3
Ambient temperature 80
Barometric pressure 30
Probe length in (ft) 3

INITIAL LEAK ✓ = 0.004 G10'
FINAL " " = 0.012 017"

SCHEMATIC OF STACK CROSS SECTION

Traverse point number	Sampling time (θ), min.	Stack temperature °C (°F)	Pressure differential across orifice meter ΔH mm (in.) H ₂ O	Meter reading gas sample volume m ³ (ft ³)	ΔV_m m ³ (ft ³)	Gas Sample temperature at dry gas meter		Temperature of gas leaving condenser or last impinger °C (°F)
						Inlet ($T_{m,i}$), °C (°F)	Outlet ($T_{m,o}$), °C (°F)	
	1924	250	1.6	574.160		81	82	
	1948	-	0.65	524.1		82	80	
	2005	-	-	531.355		-	-	
Total								
Average						Avg.	Avg.	

Figure 6-9. Method 4 Field Data Sheet.

MOISTURE RECOVERY FORM FOR METHOD 4

PLANT Stochmans
 DATE _____
 RUN NUMBER _____
 SAMPLING LOCATION LINE 1 - Run
 SAMPLING TYPE _____
 SAMPLING BOX NUMBER _____
 CLEAN-UP PERSON _____
 SOLVENT RINSES _____
 SAMPLE IDENTIFICATION CODE _____
 XAD TRAP NUMBER _____

IMPINGER NUMBER	IMPINGER SOLUTION	AMOUNT OF SOLUTION (g)	IMPINGER TIP CONFIGURATION	IMPINGER WEIGHT (grams)		
				FINAL	INITIAL	WEIGHT GAIN
					609.0	
					603.2	
					474.0	
					729.0	

Revision: 3/80

TOTAL WEIGHT GAIN (grams) _____

Figure 6-8. Method 4 Train Preparation and Recovery Sheet.

$$V_{LC} \times .04707 = R_{0.5}$$

$$(V_{LC} \times .04707) + V_m$$

MOISTURE RECOVERY FORM FOR METHOD 4

Run 1 4.7% $\times 20$ $\div 3$

Run 2 12.5% $\times 20$ $\div 3$

Run 3
 $31 \times .04707 = 8.976$
 $31 \times .04707 + 15$

PLANT Strochmann's Bakery
 DATE 6/18/92
 RUN NUMBER 01
 SAMPLING LOCATION Line 2 Run 1 = FRONT
 SAMPLING TYPE H₂O Run 2 = REAR
 SAMPLING BOX NUMBER 1
 CLEAN-UP PERSON CRP
 SOLVENT RINSES None
 SAMPLE IDENTIFICATION CODE ---
 XAD TRAP NUMBER ---

IMPINGER NUMBER	IMPINGER SOLUTION	AMOUNT OF SOLUTION (g)	IMPINGER TIP CONFIGURATION	IMPINGER WEIGHT (grams)			WEIGHT GAIN (g)
				FINAL	INITIAL	WEIGHT GAIN	
1	H ₂ O	100	MOD <u>FLARE</u>	<u>669.4</u>	<u>592.4</u>	<u>77.0</u>	<u>17.1</u>
2	H ₂ O	100	<u>600.0</u>	<u>598.0</u>	<u>589.9</u>	<u>8.1</u>	<u>2.0</u>
3	MT	0	<u>473.0</u>	<u>472.2</u>	<u>470.4</u>	<u>1.8</u>	<u>0.8</u>
4	Sol Gel	200	<u>720.3</u>	<u>716.0</u>	<u>711.6</u>	<u>4.4</u>	<u>4.3</u>
						<u>Run 1</u>	<u>Run 2</u>

Revision: 3/80

TOTAL WEIGHT GAIN (grams)

91.3

24.2
 Total
 Run
 02

Figure 6-8. Method 4 Train Preparation and Recovery Sheet.

MOISTURE RECOVERY FORM FOR METHOD 4

PLANT 51R2
 DATE 6/18
 RUN NUMBER 3
 SAMPLING LOCATION LIN 1 FRONT
 SAMPLING TYPE 1R2
 SAMPLING BOX NUMBER _____
 CLEAN-UP PERSON _____
 SOLVENT RINSES _____
 SAMPLE IDENTIFICATION CODE _____
 XAD TRAP NUMBER _____

CAP

6/18/92

Run 03

2m

~~6/18/92~~

MPINGER NUMBER	MPINGER SOLUTION	AMOUNT OF SOLUTION (g)	MPINGER TIP CONFIGURATION	MPINGER WEIGHT (grams)		
				T _S ≈ 350° FINAL	≈ 15 ft° INITIAL	WEIGHT GAIN
4	SG			723.7	720.3 686.5	3.4
3				473.2	473	0.2
2				601.7	600	1.7
1				712.2	686.5	25.7
						Run 3

Revision: 3/80

TOTAL WEIGHT GAIN (grams)

31.46

Figure 6-8. Method 4 Train Preparation and Recovery Sheet.

Appendix B.7
Flow Calculations

PLANT	SITE 2	STD METERED VOLUME (scf).....	16.78
DATE	6/18/92	MOISTURE COLLECTED (g).....	24.20
SAMPLING LOCATION	LINE 1 FRONT	% O2.....	19.00
RUN	LINE 1F - RUN 1	% CO2.....	2.00
AMBIENT TEMPERATUR	72.00	%N2.....	79.00
BAROMETRIC PRESSUR	30.01	PERCENT MOISTURE IN STACK....	6.37
STATIC PRESSURE (in H2	-0.10	MOLE FRAC. of DRY STACK GAS...	0.94
OPERATOR	CRP	DRY MOLECULAR	29.08
METER TEMP (deg. F)....	81.25	WET MOLECULAR	28.37
METER ORIFICE dH (" H2	1.13	STACK DIAMETER (I	12.00
METERED VOLUME (cu.f	17.20	STACK AREA (sq ft)	0.79
METER Y.....	0.9947		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.150	266	0.39	25.68	1540.73
A2	0.140	273	0.37	24.93	1495.65
A3	0.120	269	0.35	23.02	1380.91
A4	0.110	267	0.33	22.01	1320.31
B1	0.130	266	0.36	23.91	1434.34
B2	0.130	270	0.36	23.97	1438.29
B3	0.120	269	0.35	23.02	1380.91
B4	0.120	269.00	0.35	23.02	1380.91
Averages		268.63	0.36	23.69	1421.50

STACK GAS ACTUAL VOL FLOW (acfm)	1116.44
STACK GAS STANDARD VOL FLOW (scfm)	811.26
STACK GAS STANDARD DRY VOL FLOW (ds	759.61

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/18/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	LINE 1 REAR	% O2.....	18.50
RUN	LINE 1R - RUN 1	% CO2.....	1.00
AMBIENT TEMPERATURE	72.00	%N2.....	80.50
BAROMETRIC PRESSURE	30.01	PERCENT MOISTURE IN STACK.....	6.37 *
STATIC PRESSURE (in H2	-0.20	MOLE FRAC. of DRY STACK GAS.....	0.94
OPERATOR	CRP	DRY MOLECULAR W	28.90
METER TEMP (deg. F)....	NC	WET MOLECULAR W	28.21
METER ORIFICE dH (" H2	NC	STACK DIAMETER (I	12.00
METERED VOLUME (cu.ft.	NC	STACK AREA (sq ft)	0.79
METER Y.....	NC		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.330	312	0.57	39.40	2363.90
A2	0.320	297	0.57	38.42	2305.08
A3	0.310	298	0.56	37.84	2270.27
A4	0.280	298	0.53	35.96	2157.63
B1	0.350	315	0.59	40.65	2439.21
B2	0.340	318	0.58	40.15	2408.76
B3	0.310	316	0.56	38.28	2297.08
B4	0.300	314.00	0.55	37.61	2256.81
<hr/>					
Averages		308.50	0.56	38.54	2312.15

STACK GAS ACTUAL VOL FLOW (acfm)	1815.96
STACK GAS STANDARD VOL FLOW (scfm)	1250.78
STACK GAS STANDARD DRY VOL FLOW (dscf)	1171.15

* ASSUMED FROM A PREVIOUS RUN

PLANT	SITE 2	STD METERED VOLUME (scf).....	13.95
DATE	6/17/92	MOISTURE COLLECTED (g).....	91.30
SAMPLING LOCATION	LINE 2 FRONT	% O2.....	19.00 *
RUN	LINE 2F - RUN 1	% CO2.....	0.05 *
AMBIENT TEMPERATURE	72.00	%N2.....	80.95
BAROMETRIC PRESSURE	30.21	PERCENT MOISTURE IN STACK.....	23.58
STATIC PRESSURE (in H2	-0.10	MOLE FRAC. of DRY STACK GAS.....	0.76
OPERATOR	CRP	DRY MOLECULAR W	28.77
METER TEMP (deg. F)....	87.38	WET MOLECULAR W	26.23
METER ORIFICE dH (" H2	1.25	STACK DIAMETER (I	11.50
METERED VOLUME (cu.ft.	14.36	STACK AREA (sq ft)	0.72
METER Y.....	0.9947		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.18	224	0.42	28.30	1698.26
A2	0.18	222	0.42	28.26	1695.78
A3	0.19	223	0.44	29.06	1743.52
A4	0.19	224	0.44	29.08	1744.80
A5	0.19	221	0.44	29.02	1740.96
A6	0.20	220	0.45	29.75	1784.88
A7	0.19	230	0.44	29.21	1752.44
A8	0.18	235.00	0.42	28.53	1711.87
B1	0.15	240.00	0.39	26.14	1568.33
B2	0.15	238.00	0.39	26.10	1566.09
B3	0.19	240.00	0.44	29.42	1765.10
B4	0.18	236.00	0.42	28.55	1713.10
B5	0.18	234.00	0.42	28.51	1710.64
B6	0.16	231.00	0.40	26.82	1609.31
B7	0.15	230.00	0.39	25.95	1557.08
B8	0.16	230.00	0.40	26.80	1608.15
<hr/>					
Averages		229.88	0.42	28.10	1685.86

STACK GAS ACTUAL VOL FLOW (acfm)	1216.03
STACK GAS STANDARD VOL FLOW (scfm)	939.47
STACK GAS STANDARD DRY VOL FLOW (dscf)	717.93

* ESTIMATED

PLANT	SITE 2	STD METERED VOLUME (scf).....	19.07
DATE	6/17/92	MOISTURE COLLECTED (g).....	24.20
SAMPLING LOCATION	LINE 2 REAR	% O2.....	19.00 *
RUN	LINE 2R - RUN 1	% CO2.....	0.05 *
AMBIENT TEMPERATURE	72.00	%N2.....	80.95
BAROMETRIC PRESSURE	30.21	PERCENT MOISTURE IN STACK.....	5.64
STATIC PRESSURE (in H2	-0.05	MOLE FRAC. of DRY STACK GAS.....	0.94
OPERATOR	CRP	DRY MOLECULAR W	28.77
METER TEMP (deg. F)....	87.83	WET MOLECULAR W	28.16
METER ORIFICE dH (" H2	1.60	STACK DIAMETER (I	16.00
METERED VOLUME (cu.ft.	19.63	STACK AREA (sq ft)	1.40
METER Y.....	0.9947		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.020	286	0.14	9.51	570.53
A2	0.020	293	0.14	9.55	573.20
A3	0.025	292	0.16	10.67	640.43
A4	0.025	294	0.16	10.69	641.28
A5	0.025	300	0.16	10.73	643.83
A6	0.045	355	0.21	14.91	894.51
A7	0.045	346	0.21	14.83	889.56
A8	0.035	300.00	0.19	12.70	761.79
B1	0.045	330.00	0.21	14.68	880.68
B2	0.045	333.00	0.21	14.71	882.35
B3	0.050	332.00	0.22	15.49	929.49
B4	0.045	336.00	0.21	14.73	884.02
B5	0.045	338.00	0.21	14.75	885.13
B6	0.040	300.00	0.20	13.57	814.39
B7	0.035	323.00	0.19	12.89	773.24
B8	0.035	300.00	0.19	12.70	761.79
<hr/>					
Averages		316.13	0.19	12.92	775.36

STACK GAS ACTUAL VOL FLOW (acfm)	1082.61
STACK GAS STANDARD VOL FLOW (scfm)	743.54
STACK GAS STANDARD DRY VOL FLOW (dscf)	701.57

* ESTIMATED

PLANT	SITE 2	STD METERED VOLUME (scf).....	13.23
DATE	6/19/92	MOISTURE COLLECTED (g).....	14.80
SAMPLING LOCATION	LINE 3 FRONT	% O2.....	19.50
RUN	LINE 3F - RUN 1	% CO2.....	0.50
AMBIENT TEMPERATURE	72.00	%N2.....	80.00
BAROMETRIC PRESSURE	29.77	PERCENT MOISTURE IN STACK.....	5.01
STATIC PRESSURE (in H2	-0.25	MOLE FRAC. of DRY STACK GAS....	0.95
OPERATOR	CRP	DRY MOLECULAR W	28.86
METER TEMP (deg. F)....	82.33	WET MOLECULAR W	28.32
METER ORIFICE dH (" H2	1.57	STACK DIAMETER (I	13.75
METERED VOLUME (cu.ft.	13.68	STACK AREA (sq ft)	1.03
METER Y.....	0.9947		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.550	217	0.74	47.73	2863.87
A2	0.520	218	0.72	46.45	2786.73
A3	0.340	213	0.58	37.42	2245.04
A4	0.290	208	0.54	34.43	2065.68
B1	0.440	219	0.66	42.76	2565.31
B2	0.460	218	0.68	43.68	2621.03
B3	0.460	219	0.68	43.72	2622.96
B4	0.370	217.00	0.61	39.15	2348.95
Averages		216.13	0.65	41.91	2514.43
STACK GAS ACTUAL VOL FLOW (acfm)					2592.82
STACK GAS STANDARD VOL FLOW (scfm)					2013.37
STACK GAS STANDARD DRY VOL FLOW (dscf)					1912.52

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/19/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	LINE 3 REAR	% O2.....	19.50 *
RUN	LINE 3R - RUN 1	% CO2.....	0.50 *
AMBIENT TEMPERATURE	72.00	%N2.....	80.00
BAROMETRIC PRESSURE	29.77	PERCENT MOISTURE IN STACK.....	4.97
STATIC PRESSURE (in H2	-0.15	MOLE FRAC. of DRY STACK GAS.....	0.95
OPERATOR	CRP	DRY MOLECULAR W	28.86
METER TEMP (deg. F)....	NC	WET MOLECULAR W	28.32
METER ORIFICE dH (" H2	NC	STACK DIAMETER (I	15.50
METERED VOLUME (cu.ft.	NC	STACK AREA (sq ft)	1.31
METER Y.....	NC		

Traverse Point Number	Velocity Head P (in H2O)	Stack Ts (F)	Square Root of P	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.290	226	0.54	34.88	2092.93
A2	0.300	227	0.55	35.50	2130.26
A3	0.250	225	0.50	32.36	1941.82
A4	0.190	201	0.44	27.72	1662.91
B1	0.220	208	0.47	29.98	1798.83
B2	0.250	209	0.50	31.98	1919.00
B3	0.260	210	0.51	32.64	1958.46
B4	0.230	208.00	0.48	30.65	1839.26
<hr/>					
Averages		214.25	0.50	31.95	1917.20
<hr/>					
STACK GAS ACTUAL VOL FLOW (acfm)					2512.22
STACK GAS STANDARD VOL FLOW (scfm)					1956.69
STACK GAS STANDARD DRY VOL FLOW (dscf)					1859.42

* ESTIMATED

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/18/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	COMFORT HOOD	% O2.....	20.90 *
RUN	C.H.-LINE#1-RUN1	% CO2.....	0.00 *
AMBIENT TEMPERATURE ...	70.00	%N2.....	79.00
BAROMETRIC PRESSURE ...	30.01	PERCENT MOISTURE IN STACK.....	2.00 *
STATIC PRESSURE (in H2O)	0.00	MOLE FRAC. of DRY STACK GAS.....	0.98
OPERATOR	CRP	DRY MOLECULAR WEIGHT.....	28.81
METER TEMP (deg. F)....	NC	WET MOLECULAR WEIGHT.....	28.59
METER ORIFICE dH (" H2O)	NC	STACK DIAMETER (IN)	NA
METERED VOLUME (cu.ft.).	NC	STACK AREA (sq ft)	3.30
METER Y.....	NC		

Traverse Point Number	Velocity Head DP (in H2O)	Stack Ts (°F)	Square Root of DP	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1		207			200.00
A2		207			100.00
A3		207			50.00
B1		207			200.00
B2		207			200.00
B3		207			100.00
<hr/>					
Averages		207.00			141.67
STACK GAS ACTUAL VOL FLOW (acfm)					467.47
STACK GAS STANDARD VOL FLOW (scfm)					371.16
STACK GAS STANDARD DRY VOL FLOW (dscfm)					363.73

* ESTIMATED

** VELOCITY AND FLOW MEASUREMENTS NOT MADE ACCORDING TO EPA REFERENCE METHODS 1 & 2. COMFORT HOODS EXHAUSTS VENTED DIRECTLY TO ATMOSPHERE FOLLOWING THE FAN. VELOCITY MEASUREMENTS MADE AT 3 POINTS ALONG 2 RADII OF A ANNULAR TYPE AREA. FLOW MEASUREMENTS MADE WITH A HOT WIRE ANEMOMETER (see below).

NOTE: FAN OFF

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/18/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	COMFORT HOOD	% O2.....	20.90 *
RUN	C.H.-LINE#3-RUN1	% CO2.....	0.00 *
AMBIENT TEMPERATURE ...	70.00	%N2.....	79.00
BAROMETRIC PRESSURE ...	30.01	PERCENT MOISTURE IN STACK.....	2.00 *
STATIC PRESSURE (in H2O)	0.00	MOLE FRAC. of DRY STACK GAS.....	0.98
OPERATOR	CRP	DRY MOLECULAR WEIGHT.....	28.81
METER TEMP (deg. F)....	NC	WET MOLECULAR WEIGHT.....	28.59
METER ORIFICE dH (" H2O)	NC	STACK DIAMETER (IN)	NA
METERED VOLUME (cu.ft.).	NC	STACK AREA (sq ft)	3.30
METER Y.....	NC		

Traverse Point Number	Velocity Head DP (in H2O)	Stack Ts (*F)	Square Root of DP	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1		100			400.00
A2		100			200.00
A3		100			50.00
B1		100			400.00
B2		100			200.00
B3		100			100.00

Averages		100.00			225.00

STACK GAS ACTUAL VOL FLOW (acfm)	742.45
STACK GAS STANDARD VOL FLOW (scfm)	702.12
STACK GAS STANDARD DRY VOL FLOW (dscfm)	688.07

* ESTIMATED

** VELOCITY AND FLOW MEASUREMENTS NOT MADE ACCORDING TO EPA REFERENCE METHODS 1 & 2. COMFORT HOODS EXHAUSTS VENTED DIRECTLY TO ATMOSPHERE FOLLOWING THE FAN. VELOCITY MEASUREMENTS MADE AT 3 POINTS ALONG 2 RADII OF A ANNULAR TYPE AREA. FLOW MEASUREMENTS MADE WITH A HOT WIRE ANEMOMETER (see below).

NOTE: FAN OFF

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/18/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	COMFORT HOOD	% O2.....	20.90 *
RUN	C.H.-LINE#2-RUN1	% CO2.....	0.00 *
AMBIENT TEMPERATURE ...	70.00	%N2.....	79.00
BAROMETRIC PRESSURE ...	30.01	PERCENT MOISTURE IN STACK.....	2.00 *
STATIC PRESSURE (in H2O)	0.00	MOLE FRAC. of DRY STACK GAS.....	0.98
OPERATOR	CRP	DRY MOLECULAR WEIGHT.....	28.81
METER TEMP (deg. F)....	NC	WET MOLECULAR WEIGHT.....	28.59
METER ORIFICE dH (" H2O)	NC	STACK DIAMETER (IN)	NA
METERED VOLUME (cu.ft.).	NC	STACK AREA (sq ft)	3.30
METER Y.....	NC		

Traverse Point Number	Velocity Head DP (in H2O)	Stack Ts (*F)	Square Root of DP	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1		106			2500.00
A2		106			1500.00
A3		106			500.00
B1		106			3500.00
B2		106			2500.00
B3		106			1000.00

Averages	105.50	1916.67
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STACK GAS ACTUAL VOL FLOW (acfm)	6324.56
STACK GAS STANDARD VOL FLOW (scfm)	5922.82
STACK GAS STANDARD DRY VOL FLOW (dscfm)	5804.37

* ESTIMATED

** VELOCITY AND FLOW MEASUREMENTS NOT MADE ACCORDING TO EPA REFERENCE METHODS 1 & 2. COMFORT HOODS EXHAUSTS VENTED DIRECTLY TO ATMOSPHERE FOLLOWING THE FAN. VELOCITY MEASUREMENTS MADE AT 3 POINTS ALONG 2 RADII OF A ANNULAR TYPE AREA. FLOW MEASUREMENTS MADE WITH A HOT WIRE ANEMOMETER (see below).

PLANT	SITE 2	STD METERED VOLUME (scf).....	NC
DATE	6/17/92	MOISTURE COLLECTED (g).....	NC
SAMPLING LOCATION	COMFORT HOOD	% O2.....	20.90 *
RUN	C.H.-LINE#2-RUN2	% CO2.....	0.00 *
AMBIENT TEMPERATURE ...	70.00	%N2.....	79.00
BAROMETRIC PRESSURE ...	30.21	PERCENT MOISTURE IN STACK.....	2.00 *
STATIC PRESSURE (in H2O)	0.00	MOLE FRAC. of DRY STACK GAS.....	0.98
OPERATOR	CRP	DRY MOLECULAR WEIGHT.....	28.81
METER TEMP (deg. F)....	NC	WET MOLECULAR WEIGHT.....	28.59
METER ORIFICE dH (" H2O)	NC	STACK DIAMETER (IN)	NA
METERED VOLUME (cu.ft.).	NC	STACK AREA (sq ft)	3.30
METER Y.....	NC		

Traverse Point Number	Velocity Head DP (in H2O)	Stack Ts (°F)	Square Root of DP	Stack Gas Velocity (fps)	Stack Gas Velocity (fpm)
A1	0.470	110	0.69	39.98	2398.95
A2	0.270	106	0.52	30.20	1811.86
A3	0.080	110	0.28	16.50	989.73
B1	0.420	107	0.65	37.70	2261.78
B2	0.300	107	0.55	31.86	1911.56
B3	0.050	108	0.22	13.02	781.08
<hr/>					
Averages	0.27	108.00	0.48	28.2108	1692.65

STACK GAS ACTUAL VOL FLOW (acfm)	5585.35
STACK GAS STANDARD VOL FLOW (scfm)	5242.24
STACK GAS STANDARD DRY VOL FLOW (dscfm)	5137.40

* ESTIMATED

** VELOCITY AND FLOW MEASUREMENTS NOT MADE ACCORDING TO
EPA REFERENCE METHODS 1 & 2. COMFORT HOODS EXHAUSTS
VENTED DIRECTLY TO ATMOSPHERE FOLLOWING THE FAN. VELOCITY
MEASUREMENTS MADE AT 3 POINTS ALONG 2 RADII OF A
ANNULAR TYPE AREA (see below).

Appendix B.8

Test Log

Monday 6/15 - Site 2

0900 Flew up to Philly. Picked up CBM truck/trailer in Economy Lot

1200 Arrived at Streckmanns after getting a little lost in Norristown. Couldn't find Stue-Kmetz (lunch) so we parked truck at line 1/2 location and broke for lunch

1330 Came back. Repacked vehicle.

Sitting heat trace
unmarked ports. Line 2 over had 3
stocks. At front, a mid, and
a stock coming off the burner. (didn't
friction over). The mid stock does
not appear to have any flow.

1400 Plant employee worked on setting up power.
Source was 220 trip phase - so wouldn't
work. Finally, after working on this all day
got power up at 1930 hrs

While waiting for power, plumbed support
guels to GC, Cal bases for the - reset
the rack w/ pumps on it. (Had to
have machine shop cut the pump base plate
so it would fit.)

we were hoping to get 80-80%. Set up
to day heat because of the lack of
power - not so (Both lines 1 and 2 are
running on two day)

Begin

Left Site

6/16 Tues

0845

On Site

Left Mike & Geoff to work while I drove around getting a few things.

1200 - 1330

Went to Hardware store & broke for lunch.

14:00

Checked Flow of mid oven 2 stack w/ Hot wire. Reading was 24-30 fpm over the top of the stack. This was same reading as ambient verifying no flow at this location.

* LINE 2 mid stack - no flow

* LINE 2 top ~ 225°F at front stack

* LINE 2 mid stack top = 80°F same as ambient

1700

Mike all set - off site

~1900

Asl. holocaust in parts stacks

1900

Had some major bugs w/ DTC monitor. Calc. both real bad - very inconsistent

~2100

Discovered problem was having both rate monitors so close together. The sample pump of one was severely interfering with the other. 1) lower the response ~ 2000 ppm 2) - cause flame out 3) product noisy trace. Moved instruments apart and problem was rectified.

2130

I drove out to get whoppers while Geoff started to replace system.

2200

Performed leak checks. Slight leak in one system & replaced pump bypass w/ new one. Front is about 0.2% $V \Rightarrow O_2$. Will track down leaks tomorrow.

2330

Off Site

6/17 Wed

0835

On site (Gaff got here at 0800)

Everything went smooth, until right before we started we got a phantom voltage again on the DAS.

Voltmeter on the lenses would read 3.7 V for a ~3900 Cal gas and computer would see 3.2-4.6 V

Very hectic - Delayed starting till 11:30

1130-1300

Ran Line 2 Burn over stacks. As usual, the data was excellent. GC data on front stack was good but rear had heat trace jumper problems (GC). It's amazing the CH_4 can be so biased by loss of heat. If we think we have a bias problem, we really don't need to work with ethanol (RT = 8 min), we can use CH_4 (@ 1.5 min)

Rear stack data is questionable (GC) but values are very low (<100) as expected (its the burner exhaust)

1400-1515

Started on the burn over. Changed product ~1430 so really didn't want to use that data. Had GC problems afterwards - so didn't start till ~1515. Ran till 16:15

1630

On the way to pulling the heat trace from the oven stacks, was hit in the face by high ethanol concentrations from the comfort hood. Decided to test it and it was ~1000 ppm. There's no way to really get a good test on it as its an annulus type geometry but got some good #'s on it and some mediocre flows on it.

2030

off site

6/18 Thur

0700

0800

CP On Site

Geoff / Mike On Site

Switching to Truck Location
#2 → for over 3 tests

As usual, power problems - finally fired
up ~ 1200 hrs

Everything looks good. Geoff showed me
step by step CEM operation. I changed
Mike B's Helium pressure (by mistake)
previous night - so his RT changed slightly.
Was shooting for startups at 1500 hrs.
but didn't really get started till ~ 1545

~1600

Front oven showed very consistent
oscillation (strip chart pen noise)

Ran for ~ $\frac{1}{4}$ - $\frac{1}{2}$ hour. Geoff
lost the flame (due to too short
a warm up period) and wind oscillation
continued. Ran stuck gas intermittently,
while continuing to shoot RCs, ok, to
determine why the oscillation occurred.
All RC's show no oscillation - Geoff
checked signal output, electronics &
source problems & they are ok.

Finally, at the end of the day,
~~put the probes~~ put the probes together (same)
and both ~~the~~ monitors showed
the oscillation.

Ran moisture on Line 2 at
Line 1 (Front Only)

2130

off site

6/19 Friday

~ 1030

On Site

Mike took Goff to airport, while I started line 1-rear, moisture run. Started raining cats & dogs. I had a tarp over me but T/C readout shorted, - but I kept going. Left train for ~10 minutes and probe fell out of stack & train was plugged somehow. Very frustrated & wet. Decided to bag moisture

~ 1200

Raining too hard to work. Drove to get foul weather gear

~ 1300 - 1400

broke for lunch

Drove to granger to try and get new T/C readout - no dice. Bought multimeter.

~ 1500

Got back to bakery. Did flour on line 1-rear, Line 3 both stacks. Ran a moisture on line 3 front

~ 2000

off site - ~~Left~~ Left for Mainer's @ Easton

~ 2200

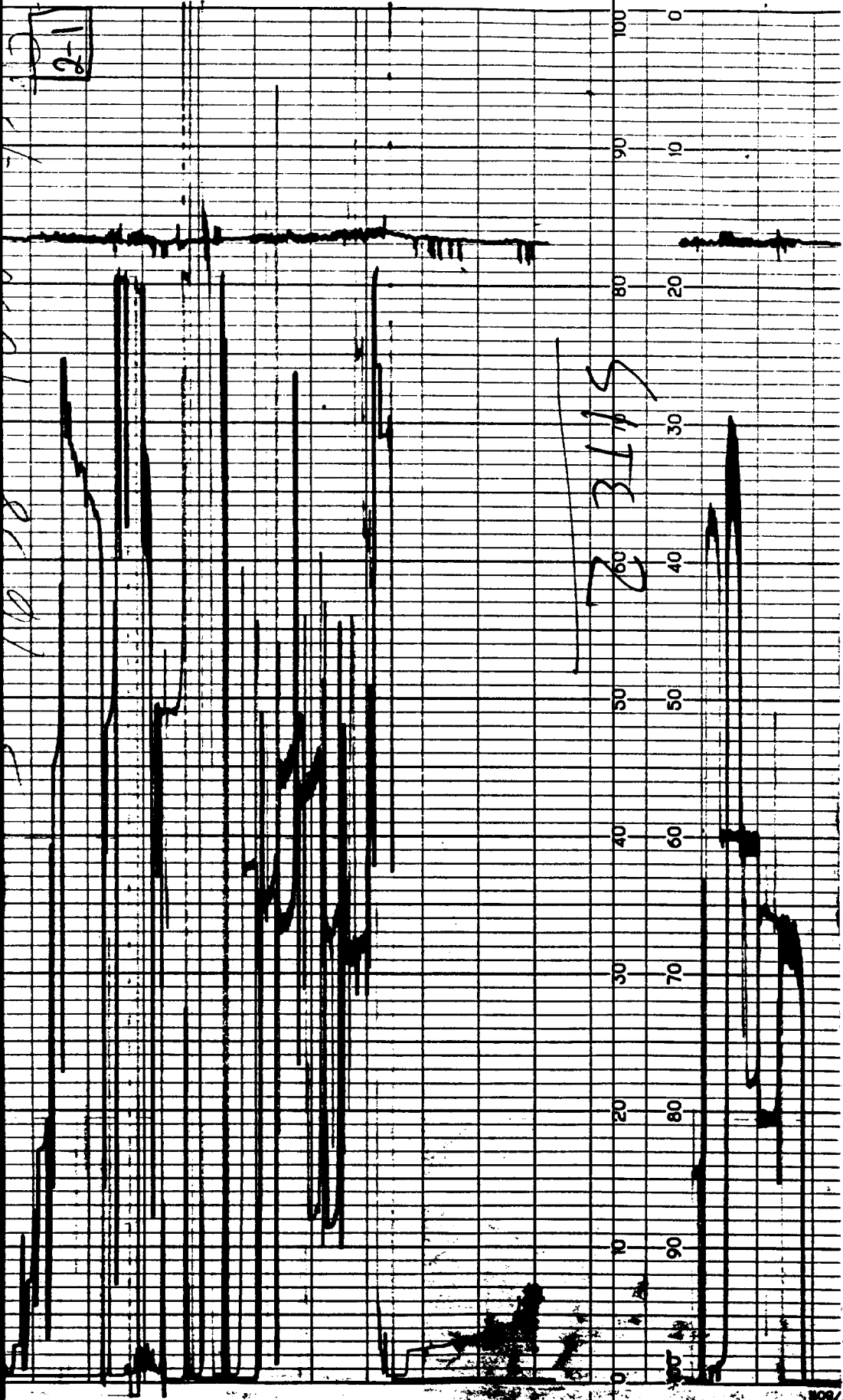
Arrived at Days Inn - Easton

Appendix B.9
Method 25A SCR Copies

SITE 02
STRECHMAN'S BAKERY
NORRISTOWN, PA.

PAGE 1 OF 25

SITE 02 - PAGE 01



11N3E15

22

100 90 80 70 60 50 40 30 20 10 0
90 80 70 60 50 40 30 20 10 0

7/18

1070

234 872

4/1031

2-3

100 0
90 10
80 20
70 30
60 40
50 50
40 60
30 70
20 80
10 90
0 100

100/

2-11

LINE 11

100 90 80 70 60 50 40 30 20 10 0
0 10 20 30 40 50 60 70 80 90 100

2-5

Back C

23.14 hrs
4/16

Front (pressure)

11/25

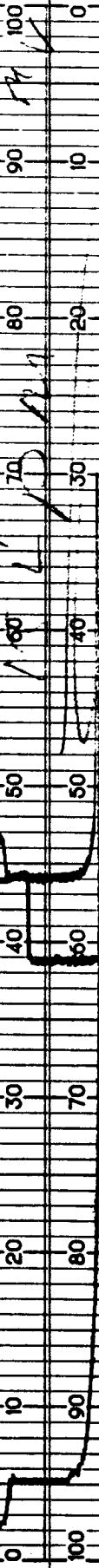
Pressure

50 PSI N₂ (20 rpm)

O₂ - Table

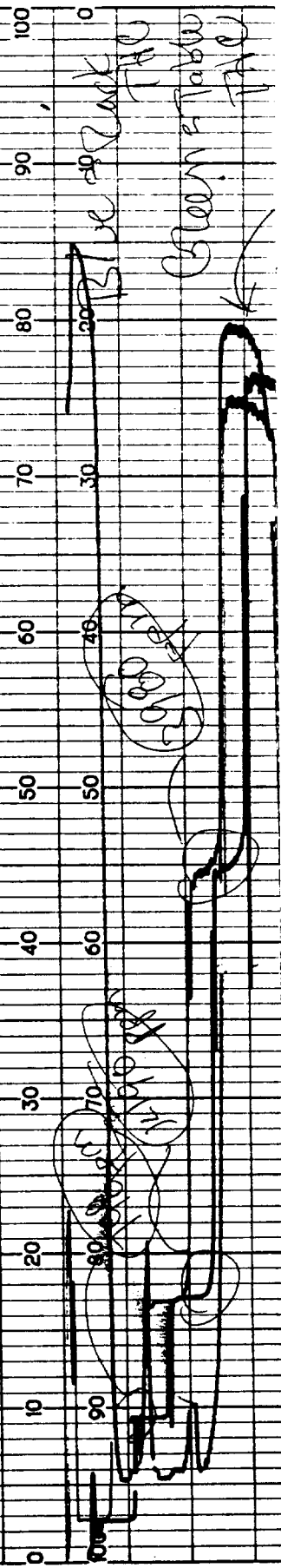
30 PSI N₂ (20 rpm)

Blow + R₂ (20 rpm)



26

Rack THC
= Rear Stack
Table THC
= Front Stack



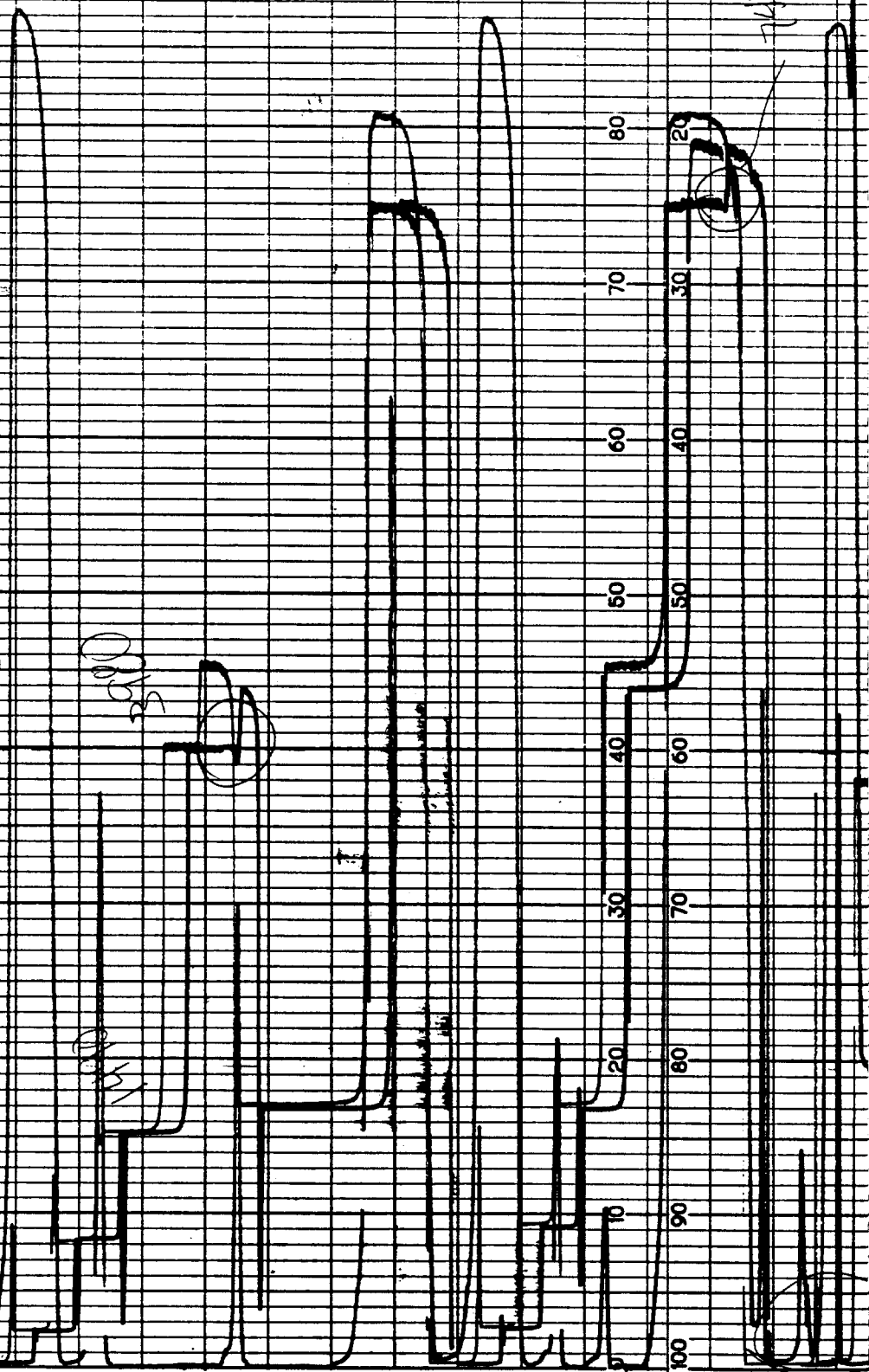
27

27
3080

27
3080

27
3080

27
3080



27
3080

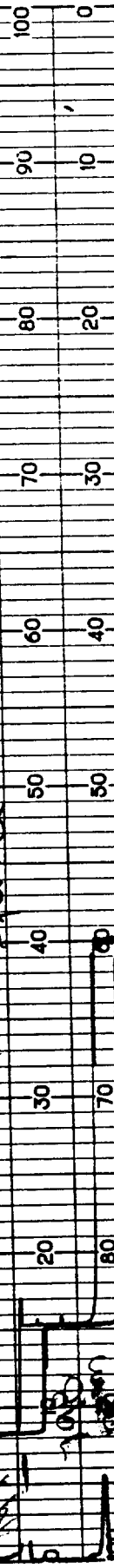
27
3080

2-8

IN E I S

3480
Span 20 ✓

21100 GND



DUPLICATE Run 01

11:30 A.M. 6/17/92

↓ repeat 10 cm

29



2-10

1300 END Run of

LINE 15

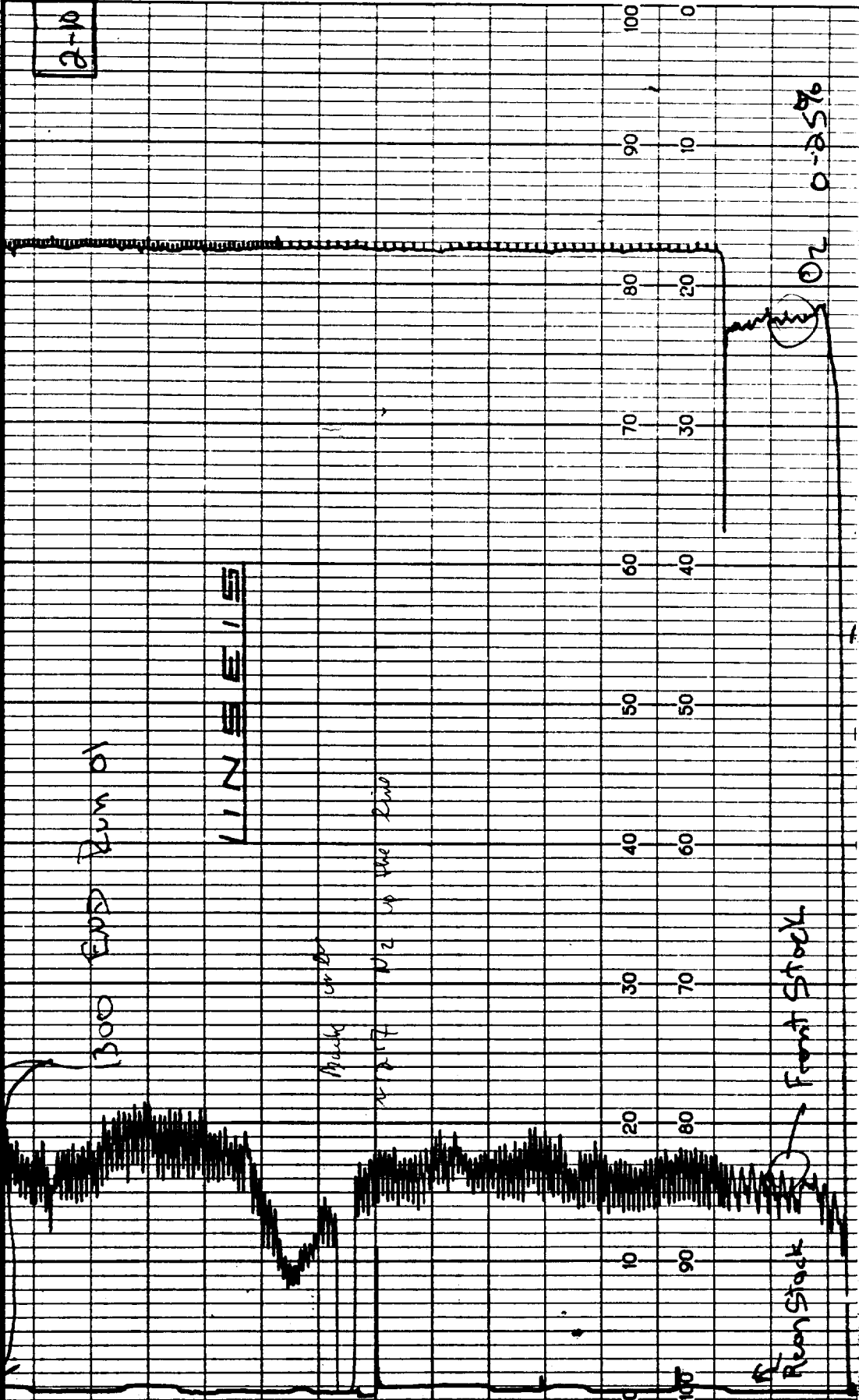
Back

at 17 W2 is the End

Front Stock

Back Stock

0-25%



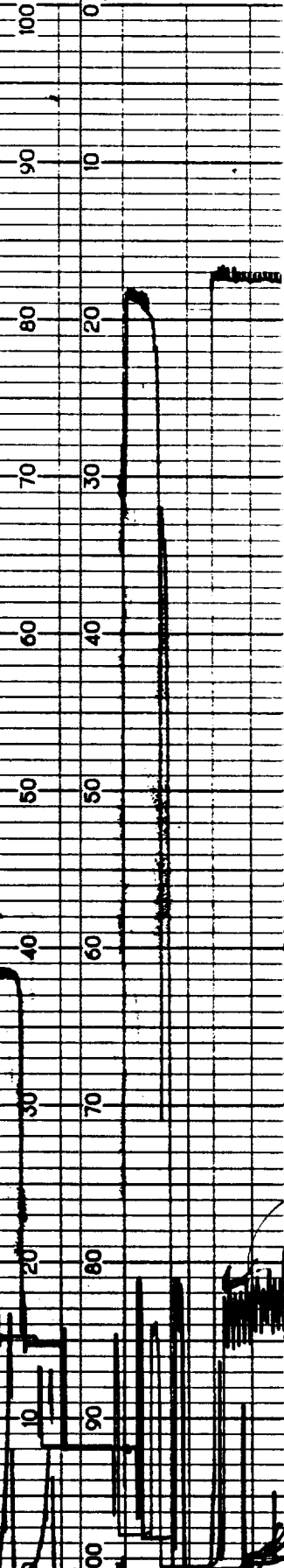
2-11

Dam & Dam

act 13-15-10
13-15-10
13-15-10

TIME 1341

13-15-10 → 13-15-10



60 pm 30

2020 4073

11445
11435 02-17-16
R.S.C. News

Rubber

25

e

1	2	3
4	5	6
7	8	9
10	11	12

4

•

2-13

Start
Broad Line

16:40

Correct
City
16:40

16:50

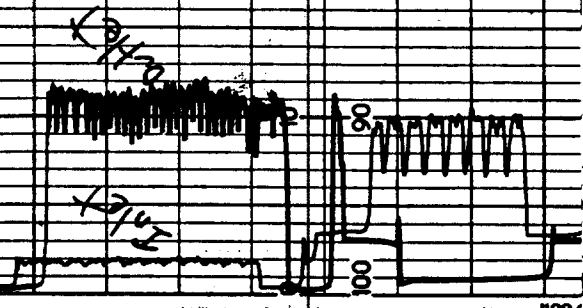
16:15 END RUN RUN

100

8-16

TIME 1945

CONFIDENTIAL

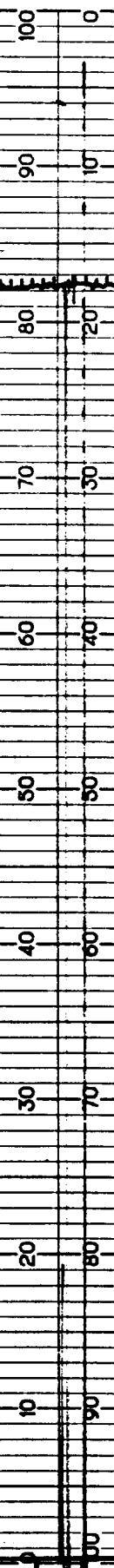


100 90 80 70 60 50 40 30 20 10 0



2.1

1123456789



R-1742

$T = 6\frac{1}{2}$ psi (12 psi)

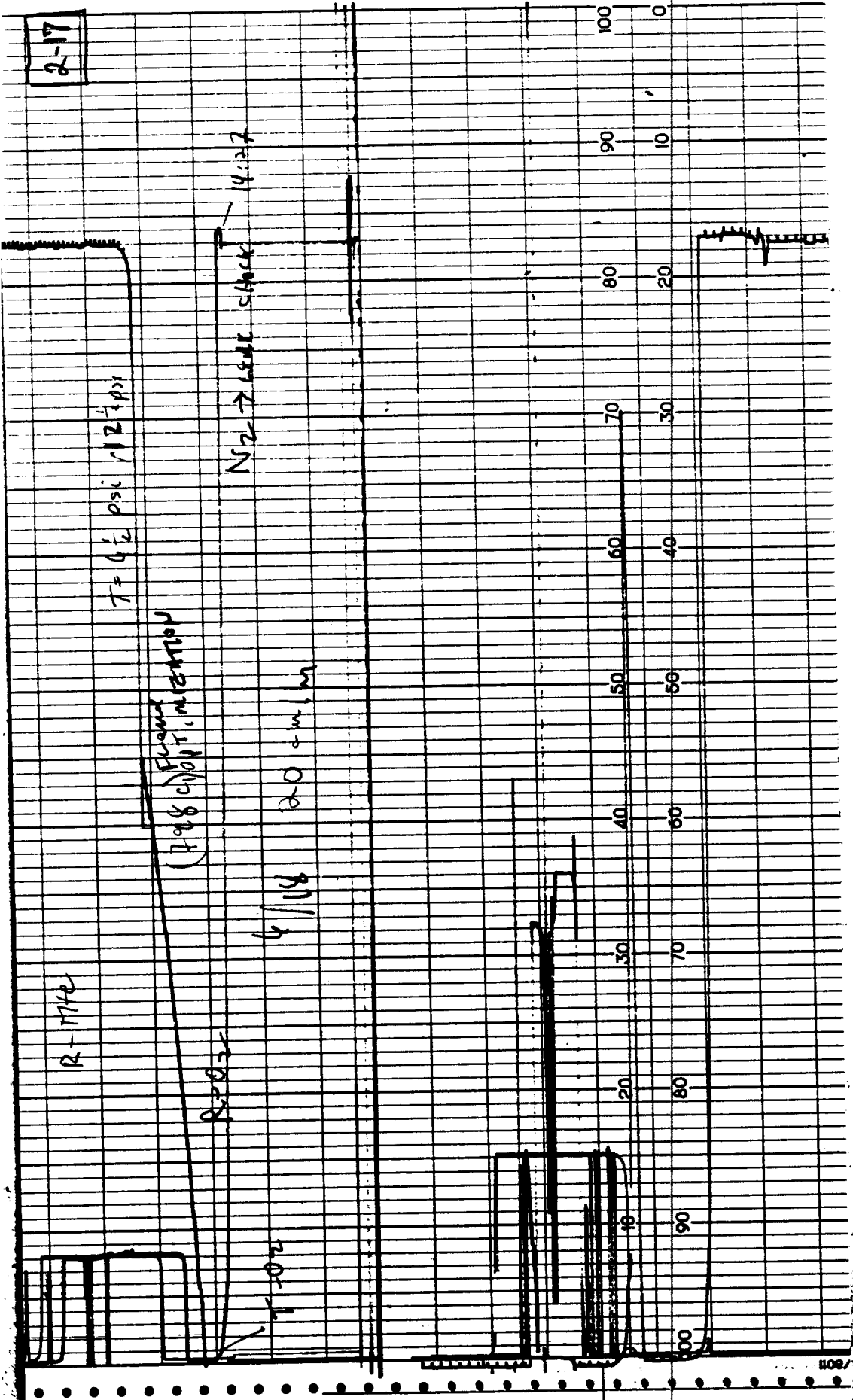
(798) Front
cylinder, mixture

R-1742

4 // 118 20 cm/m

N₂ → 14.27 stock

2-17



2-18

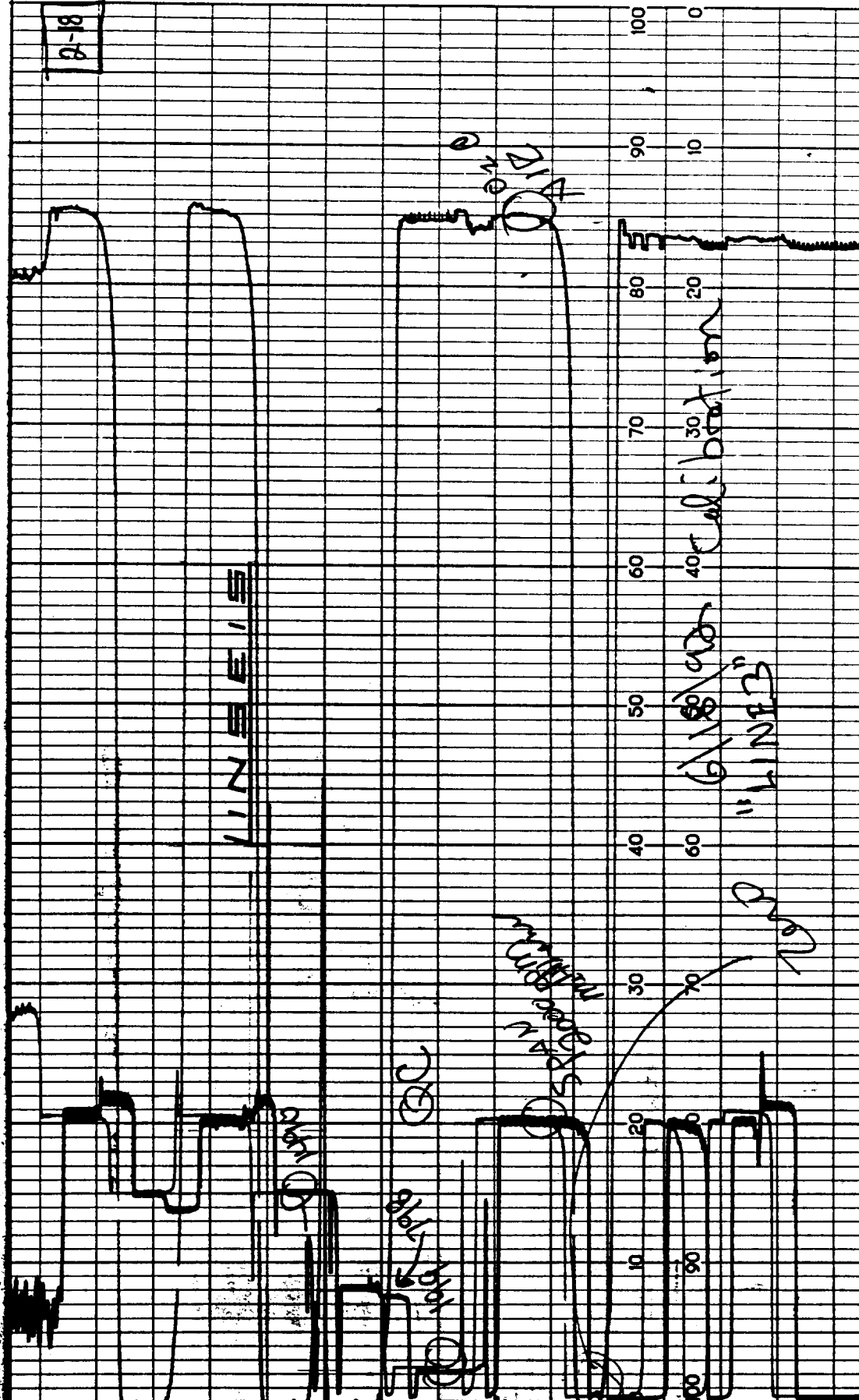
LINE 15

100 90 80 70 60 50 40 30 20 10 0

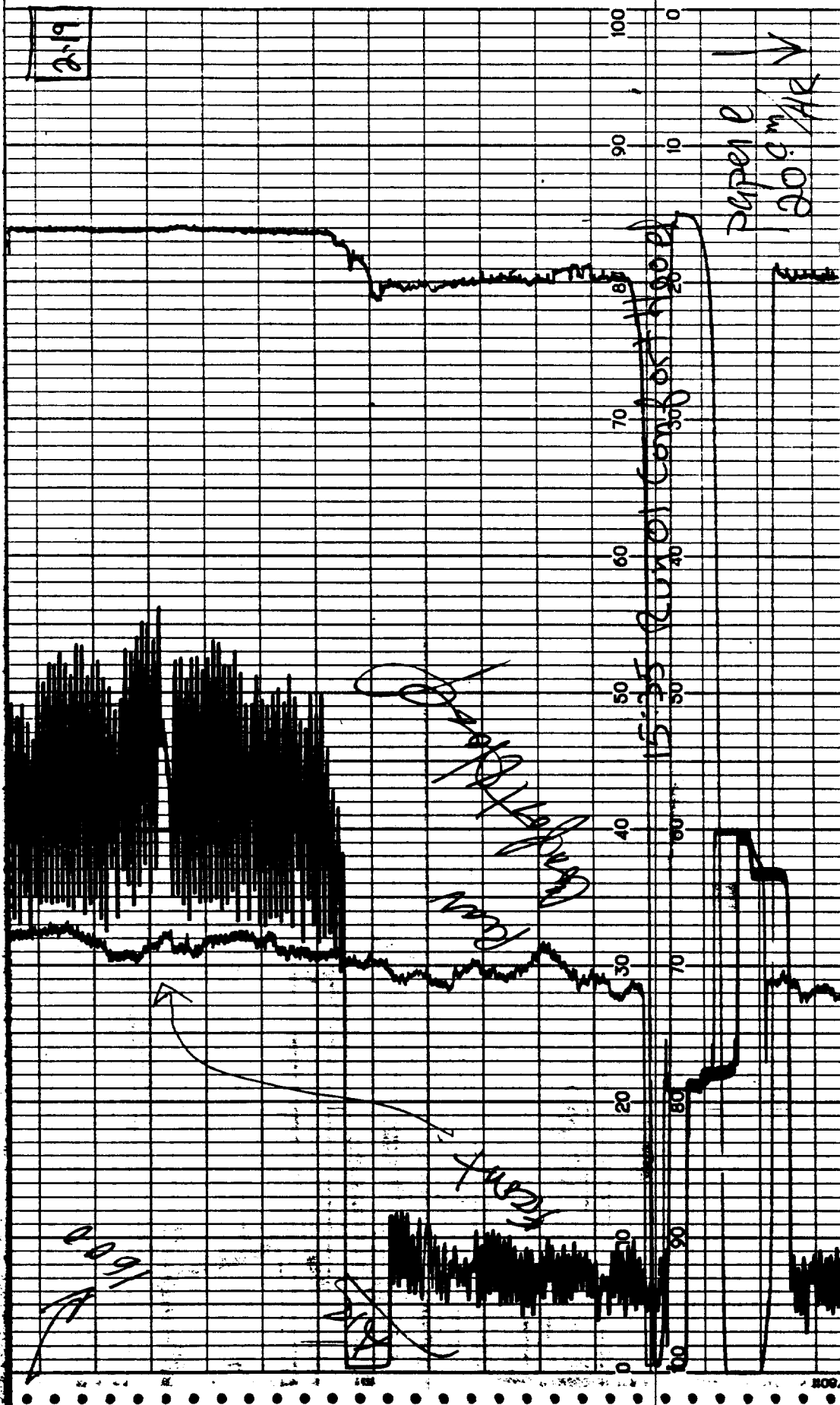
6/18/92 Calibration

"LINE 3"

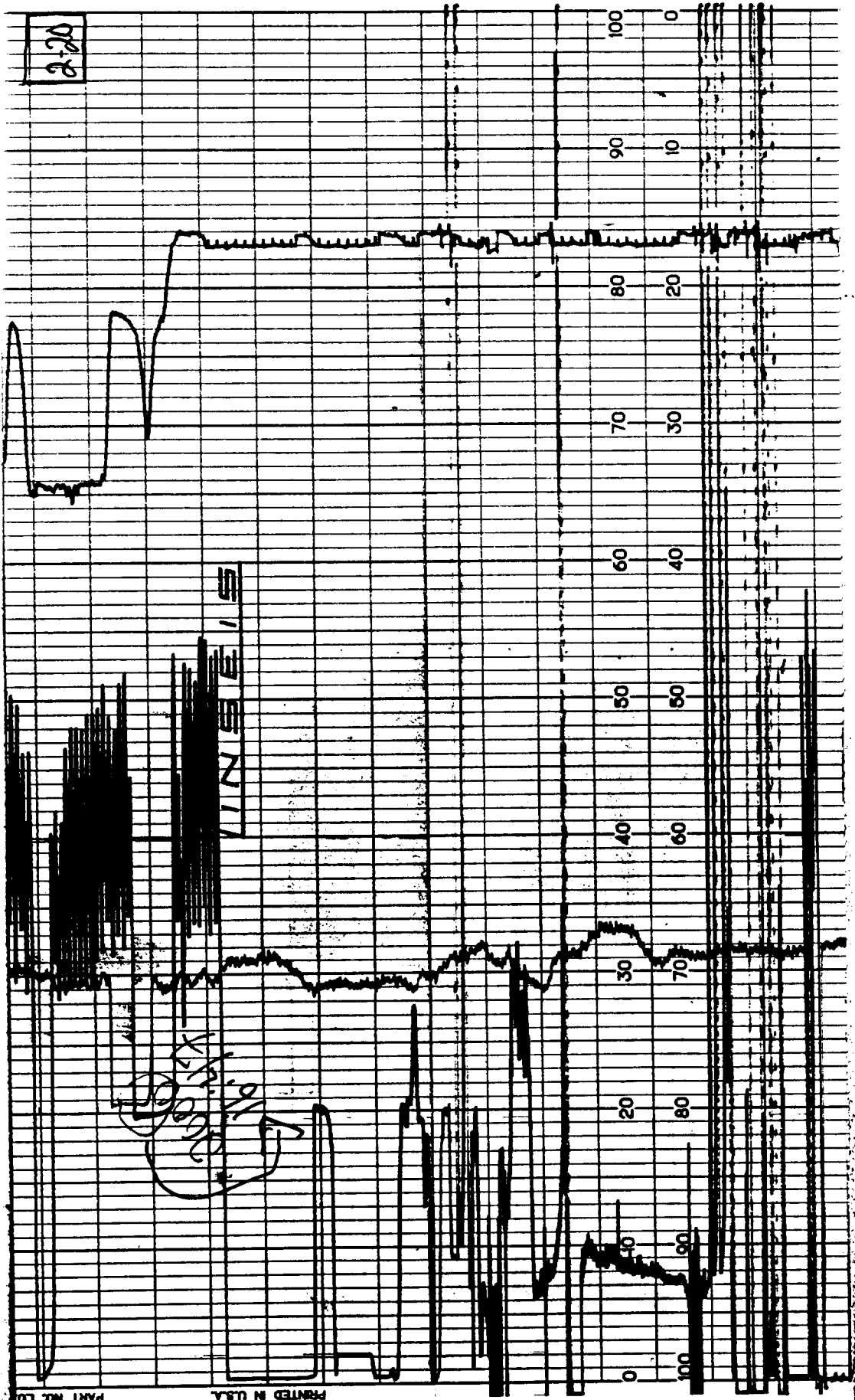
100



219



2-20



VINCE / S

6/19
2002
X

2-21

ambient

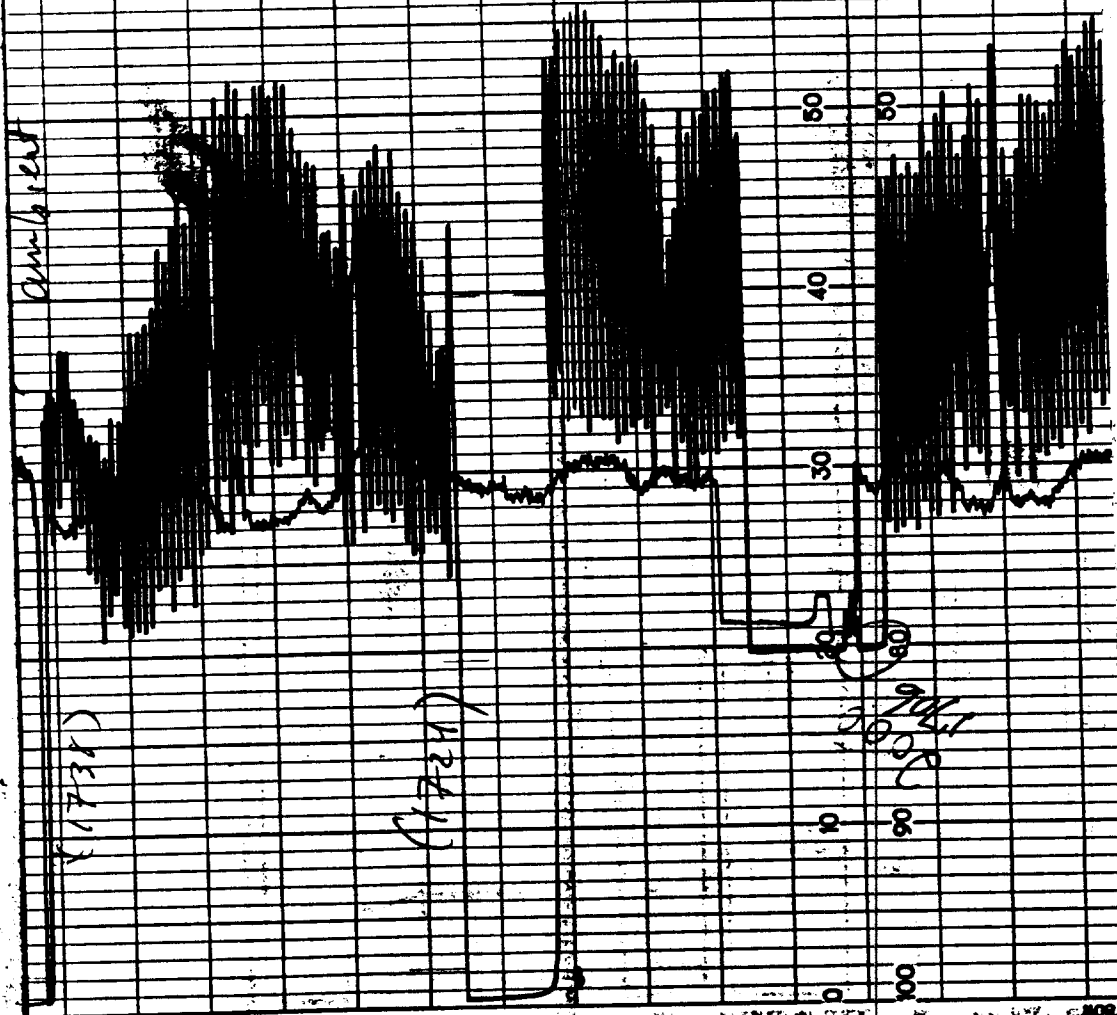
(1541)

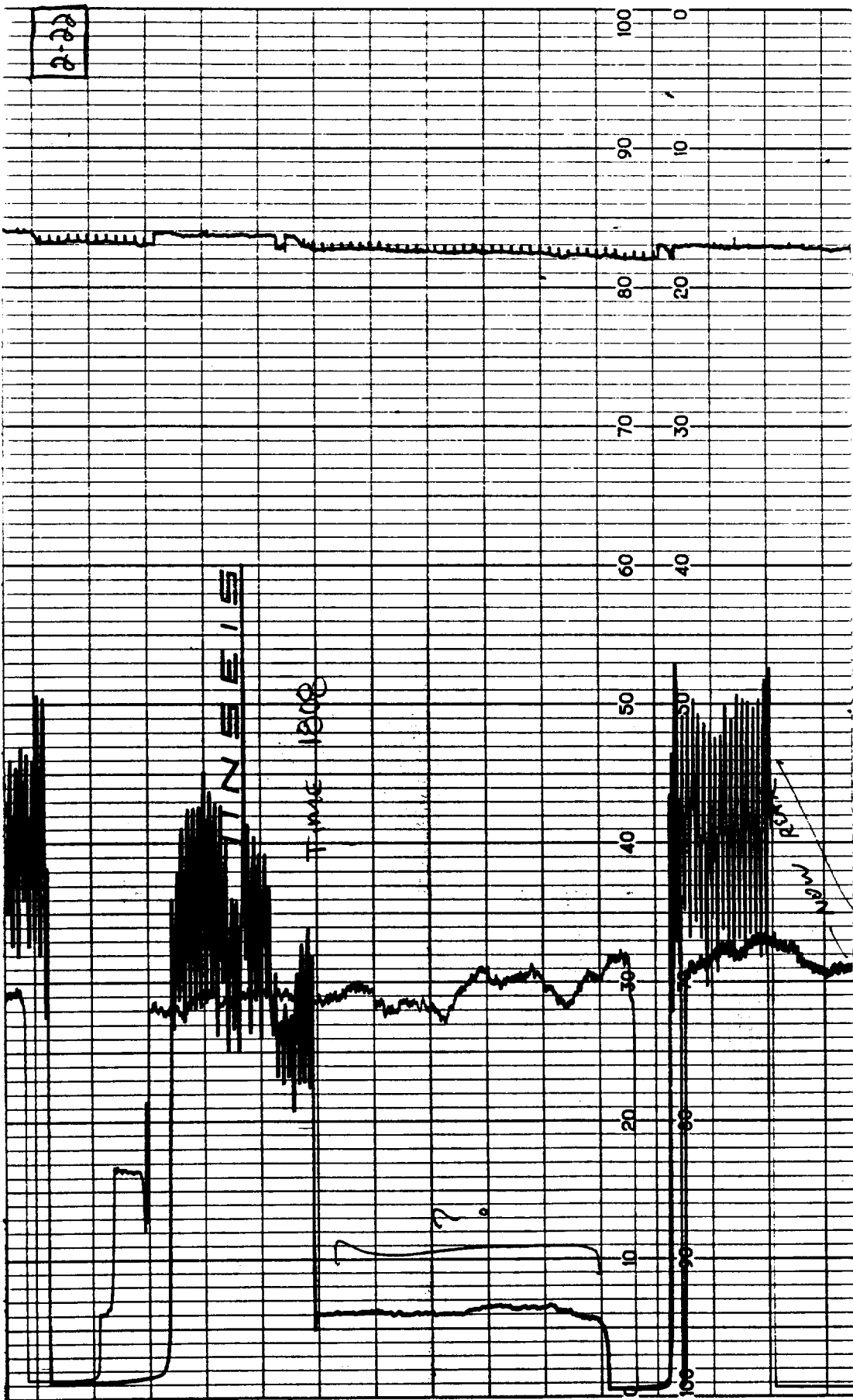
(1721)

100
90
80
70
60

50
40
30
20
10
0

904.1
1000
1100





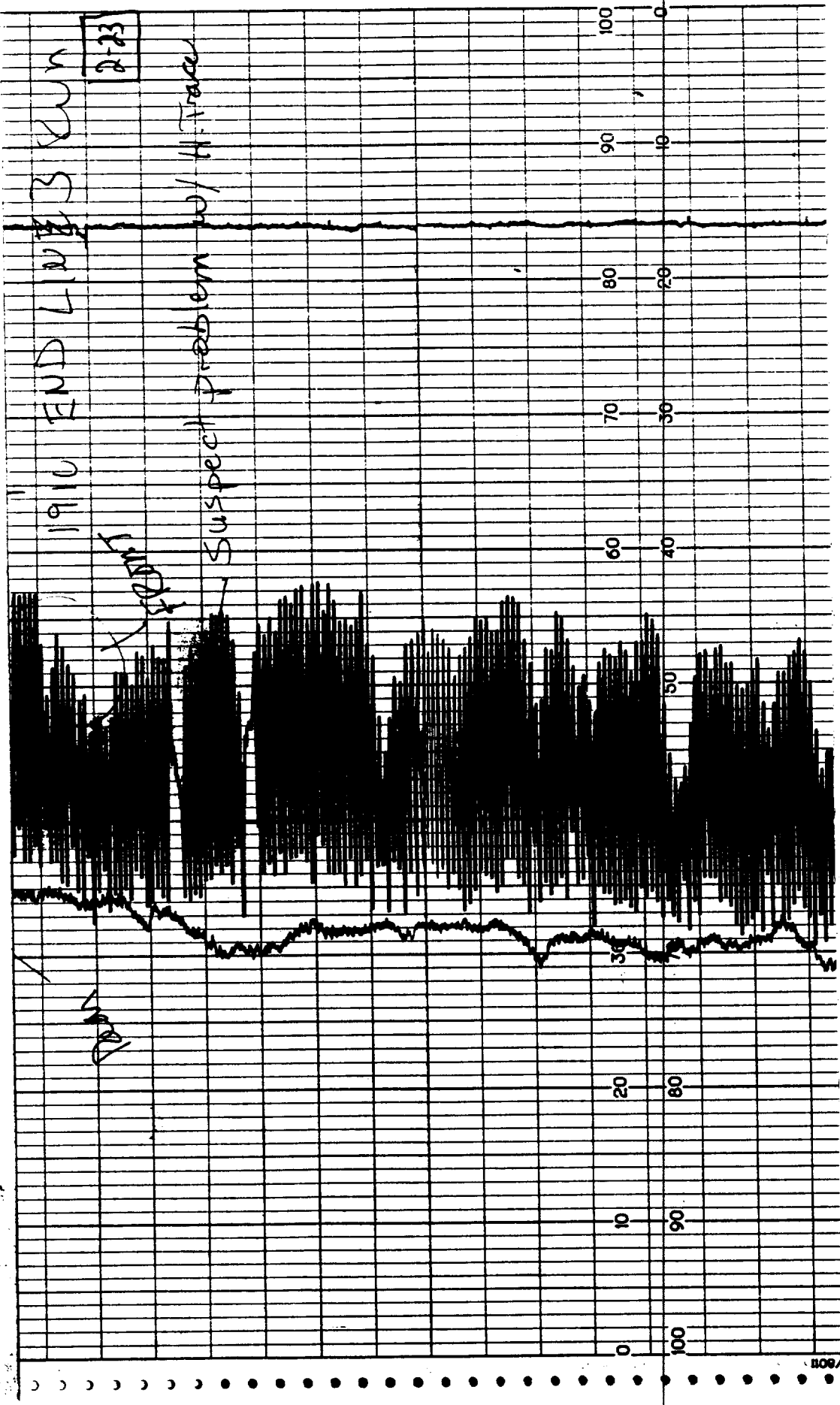
1910 END LINE 3 RUN

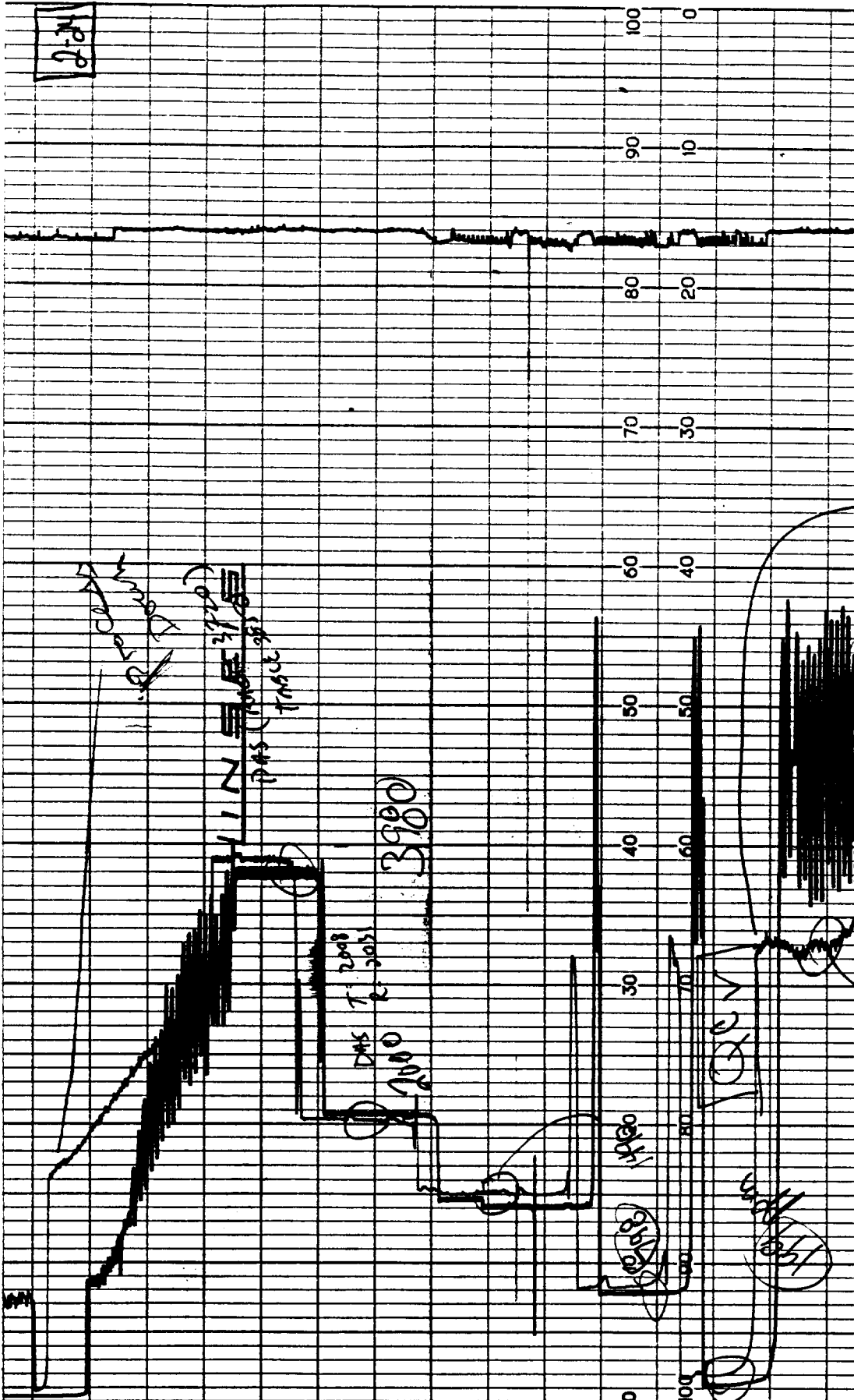
2-23

Left

Suspect problem w/ H-Trace

Run





225

